Street Emissions Celing exercise

Phase 2 report



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ETC/ACC Street Emission Ceiling (SEC) exercise

Phase 2 report

Final Report, July 2005

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Foreword

This report has been prepared by the task team of the Street Emission Ceilings exercise of the European Topic Centre on Air and Climate Change (ETC/ACC). It is based on the work performed by the Aristotle University Thessaloniki (AUT), the Norwegian Institute for Air Research (NILU), the National Institute for Public Health and the Environment (RIVM) and the Institute of Environmental Sciences Energy Research and Process Innovation (TNO). It is the phase 2 final report.

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Executive Summary

Traffic related air pollution is still one of the most pressing problems in urban areas. Evidence of the adverse health effects of fine particulate matter is continuously emerging and the fact that most of the traffic related emissions are in the fine particulates range (<PM_{2.5}) is of particular concern. Population exposure to increased pollutant concentrations in densely populated urban areas is high and thus the improvement of air quality is imperative since most air quality limit values under the new air quality directives pertain to health and apply everywhere except at workplaces, hence also in streets as the most typical example for urban hotspots. The SEC project analyses the excess concentrations observed at urban hotspots and attempts to formulate a generalised approach that can be used by local authorities in their efforts to reduce local air pollution. At the same time, SEC aims to support the CAFE program and provide a basis for the inclusion of the local scale into the full Integrated Assessment Modelling chain currently applied at European scale to study present and future air quality and air emission reductions.

As a first step and in order to study the excess concentrations observed at street/road side (traffic) stations and test the appropriateness of the overall approach and the specific models and tools against measurements, it was necessary to determine a number of cases where the data available would enable such a test basis and would be representative in order to allow for a generalisation of the results. Detailed quality controlled hourly traffic and meteorological data as well as street and urban background level concentrations (ideally PM_{2.5}, PM₁₀, NO₂, NO_x, CO and background O₃ were required) and appropriate street geometries were not readily available. Often enough the location of the stations was a limiting factor for the analysis. Furthermore, the lack of detailed traffic data as well as incomplete datasets was also a problem often encountered. Nevertheless, three case studies were singled out as most appropriate and for which an hourly data analysis for a full year was performed: Marylebone Rd. (London), Hornsgatan street (Stockholm) and Frankfurter Allee (Berlin). The data analysis considered annual and monthly averages and average diurnal variations separately for weekdays-weekends and summer-winter periods. This detailed analysis allowed for an evaluation of the emission factors for heavy and light duty vehicles and also elucidated the effect of re-suspension PM with respect to vehicle PM emissions.

Comparison of the delta (street minus background) concentration ratios (PM/NO_x and CO/NO_x) with the corresponding emission ratios enabled the site specific characteristics to emerge (e.g. importance of re-suspension PM) and provided a basis of assessment for the air quality model applications that followed. Furthermore, the appropriateness of the emissions factors could be directly compared against the concentrations observed and for PM the importance of non-tail pipe PM emissions (tyre and brake abrasion, road wear and dust re-suspension) was particularly noted. Moreover, as the streets in the cities considered had different characteristics the

influence of parameters such as height/width ratio, traffic speed and composition (different HDV percentages), wind and dispersion parameters, could be also evaluated.

Further to the concentration and emission ratio comparisons performed with data from individual sites, a "global" analysis was also performed using a number of stations across 5 European countries. The comparison showed a fair agreement between the concentration and emission ratio of CO/NO_x at a country level, suggesting that the measured concentrations originate from traffic-related emissions. The NO_x/PM and PM/CO emission ratios estimated by the TRENDS model were over- and underestimated respectively. This work highlighted once again the importance of PM emissions from gasoline-fuelled vehicles and non-exhaust sources.

The data collected and studied for Marylebone Rd. (London), Hornsgatan street (Stockholm) and Frankfurter Allee (Berlin), were further processed and the datasets were made available to interested institutes for performing a model intercomparison exercise. This exercise provided an insight in the level of uncertainty that is inherent in the various model calculations and a first estimate of the uncertainty that enters from the street level, into a complete regional-urban-street scale model application. Moreover, the large number of models that participated (13) and the variety of cases available enabled an evaluation of model performance, bearing in mind the restrictions of the input data. Finally, as the OSPM model was applied by three different institutes a different "modeller" intercomparison emerged with interesting results related to user-sensitivity analysis.

In parallel to the above data analysis and modelling activities, the theoretical basis for the classification of street types was developed. This "street typology" should allow for a generalised methodology to determine the local emission reductions needed to reach certain air quality thresholds. In the development of the typology methodology, the balance had to be maintained between model accuracy, requiring many explicit and continuous parameters, and simplicity, which demands giving preference to classified parameters. A first selection of the key parameters sufficiently characterising the various street classes resulted in the distinction of twelve street types. The classified parameters (represented by ranges of values) consisted of geometry (street canyon or not), fraction of HDVs, traffic behaviour (speed), distance of the receptor from the road axis. The only parameter retained as an explicit continuous one was daily traffic intensity. The candidate parameters were assessed in terms of their importance to air pollution, their suitability for air quality modelling and the availability of data (on specific streets and statistics across Europe). A further criterion was whether the particular parameter could be altered by specific measures, as for example the percentage of HDVs is important since it is a vehicle category with significant air emissions but technological improvements related to emission reduction for HDVs and private cars follow different tracks in time.

As an application of the typology, annual mean concentrations were calculated with the simplified air quality model CAR and then empirical relationships were used to compute exceedance days. The region chosen for the application was an arbitrary location in Flanders (Belgium). However, the methodology needs to be further applied to different types of streets in a reasonable number of countries before it is revised for the possible inclusion of new parameters and the parameter ranges are confidently defined.

Chapter 1: Report on data analysis and comparison with emissions estimates

1.1 Introduction

This report presents the work carried out, as part of the "Street Emission Ceilings" (SEC) project, to use existing monitoring data from selected quality monitoring stations as a basis for testing street scale models as well as COPERT 3 emission factors for road vehicles.

The primary objective of the Street Emission Ceilings (SEC) project is to develop a method for determining what local emission reductions in streets are needed to reach certain air quality thresholds, e.g. limit values. In particular, SEC has two purposes namely (a) Use by local authorities and (b) Use in Integrated Assessment Methodology (IAM) for CAFE.

Purpose 1: Use by local authorities

Most of the limit values under the new air quality directives pertain to health and they apply everywhere except at workplaces, so also in streets. Hence city authorities have to identify streets where limit values may be exceeded. Some countries use models for making surveys of levels in busy streets throughout the country, but most countries do not have such models. The first objective of the SEC project is to make easy-to-use model assessment systems available to local authorities for estimating air pollution levels in streets, with the purpose of identifying potential problem situations.

Purpose 2: Use in IAM for CAFE

In the developments of EU legislation prior to CAFE, Integrated Assessment Modelling has been carried out with RAINS. It focused on the regional scale concentrations in Europe, in line with the analyses needed for CLTRAP, which dealt primarily with long-range transport and the impact on vegetation and ecosystems. In CAFE, population exposure and compliance with limit values are of prime importance, hence urban levels and hotspots should be included in the assessment. For this purpose, JRC has set up the City-Delta study, targeted at modelling the urban background levels in Europe in order to provide an urban module for use in IAM. Analogously, SEC aims to provide robust street modelling techniques that can be used in IAM.

Chapter 1 summarises the work done under the subtasks 3 and 4 of the SEC project:

- Subtask 3: Analysis of excess concentrations in streets
- Subtask 4: Local (street) emissions estimates

Subtask 3 has selected well defined station pairs from cities in Europe, a station pair being a street level station together with a nearby urban background station which represents well the contribution to the air pollution concentrations at the street station which do not come from the traffic in the street itself. There were several prerequisites for selecting a station pair to participate in the study:

- As a minimum, quality controlled hourly concentrations of NO_x , NO_2 and PM_{10} had to be available for a whole recent year at both stations of the pair. It was considered important that $PM_{2.5}$ was also measured, while CO data were considered useful as well;

- Traffic data (volume, speed, heavy-duty fraction) should be available, as well as meteorological data from a nearby station measuring the meteorological parameters above the roof level of the area.

Station pairs in London, Berlin, Hannover, Stockholm, and (nearby) Oslo have been selected. Station pairs in Prague, Thessaloniki, Madrid, Milan, Paris, Helsinki and Copenhagen have also been investigated. The result of this investigative phase is that data have been collected so far from London, Berlin, Stockholm, Oslo, Hannover, Madrid and Thessaloniki. Only London, Berlin, Stockholm, Hannover and Oslo have close to full data coverage of air pollutants as well as traffic and meteo data and data from these pairs have been fully analysed (see below). Traffic data are (partly) missing from the Madrid, Milan, Copenhagen and Paris pairs and data from these pairs have not yet been subject to the analysis of this project. Helsinki seems to have full coverage and data from this pair are being made available from the data provider for a full year up to March 2004. A suitable station pair has recently been established in Prague and it is foreseen that data from this pair will be available in 2005.

The main result of the data calculation/analysis process is the calculation of "delta concentrations" (DeltaC) and "delta ratio" (DR) for each pair:

DeltaC: the street station minus the background station concentrations, for each hour of the year.

Delta ratio (**DR**): the ratio between the NO₂ and PM deltas on the one hand and the NO_x delta on the other hand, also this for each hour of the year.

 NO_x is used as the "reference" compound because it is purely a primary composite pollutant and it is considered that the emission factor for NO_x from road vehicles is the one with the lowest uncertainty (among the compounds selected for this study).

The DeltaCs and DRs are presented as average values per hour of the day (thus as average daily variations), for four combinations of season and time of the week: Summer and winter workdays and weekend days.

The DRs are the output from subtask 3 that provides a basis for the testing of COPERT 3 vehicle exhaust emission factors (also ratios) in subtask 4. Additionally, by comparing the $PM_{2.5}$ and PM_{10} DRs, estimates can be derived of the non-exhaust emissions of PM.

At present, this analysis has been carried out for the situation at the Stockholm, London, Berlin, Oslo and Thessaloniki station pairs and the results are presented in this report.

Section 1.2 of this report presents a summary of the subtask 3 work and section 1.3 a summary of the subtask 4 work.

1.2 Analysis of excess concentrations in streets

1.2.1 Introduction

As already mentioned, the primary objective of subtask 3 is to study excess concentrations at street/road-side (traffic) stations over and above the urban background concentrations in the area where the hotspot station is located.

The work procedure is to select, based upon knowledge of monitoring stations and data in AirBase as well as through contact with data providers in cities where the team is aware of good monitoring activities relevant for this project, a number of stations pairs (street/road-side hotspot station and representative urban background station) in several cities geographically distributed throughout Europe. The selection of cities should reflect the varying meteorological and source structure situations in Europe.

The results of the analysis in this subtask should:

- contribute to knowledge of (relative) emission factors for vehicles, by comparing PM, NO₂ and NO_x concentrations, as a function of vehicle distribution in traffic
- contribute to the analysis of the road dust re-suspension source, by comparing $PM_{2.5}$, PM_{10} and NO_x concentrations, together with meteorological data
- provide a basis for model-measurement comparisons / model validation.

1.2.2 Selection of station pairs

1.2.2.1 Features of traffic related PM in Europe, from existing material

PM is measured mainly as PM_{10} , although the number of $PM_{2.5}$ stations is now rapidly increasing.

Figure 1.1 shows a summary of PM_{10} data for 2001 reported to AirBase from 25 countries, in total 818 stations. The figure shows the importance of the regional and urban background (UB) contributions to the concentrations close to streets. On average for all these stations (rightmost columns in the figure), the UB concentration makes up about 79% of the traffic station concentrations (and the rural background makes up about 80% of the UB concentration). This importance of the background is a special case for PM_{10} . For NO₂, the importance of the background is much smaller (see Figure 1.1).

Note that Figure 1.2 presents, for each station type, the variability in concentrations across Europe. Some rural background stations have higher concentrations than urban and even traffic stations and this reflects that they are located in different areas and cities.



Annual average country, PM₁₀, 2001

Figure 1.1. Country- average PM_{10} concentrations (annual average) for rural, urban background and traffic stations, 2001 AirBase data (number of sites on top of bars).

AirBase contains data from a fair number of cities where PM_{10} is measured continuously at least at one traffic and one UB station. These are listed in Table 1.1. For 2001, 14 cities in Europe reported such PM_{10} data. For NO₂, the number of cities with such station pairs is larger. The table contains coordinates, so it is possible to see how close the stations are located in the city, to see if they really constitute "station pairs".

For the PM Position Paper which has been prepared as a final draft by the CAFE PM Working Group (http://europa.eu.int:8082/comm/environment/air/cafe/pdf/working_groups/2nd_position_paper_pm.pdf) a selection of these station pairs, plus some other data were studied, in order to identify more clearly the additional PM_{10} burden at traffic exposed sites from AirBase and to remove the ambiguity of comparing hotspot data from one city with background data from another. From the resulting 89 station pairs, PM_{10} ratios for annual means were calculated. For conurbations where more than one urban background site was available, the average of the sites was taken to represent the urban background. The distance between the two stations in each pair was not considered. They may be in the same area and they may be fairly widely apart, so they may not all be "good" station pairs.



Figure 1.2. Concentrations of PM_{10} (36th highest day) and NO₂ (annual average) at stations in AirBase 1995-2000, averaged over each station type (rural, urban, traffic).

A frequency distribution of the ratios is presented in Figure 1.3. The ratios of the annual means span a considerable range from 1.9 to 0.7 and the majority of the ratios are above 1, indicating a higher PM_{10} burden at traffic exposed sites compared to the urban background. The arithmetic mean of the ratios is 1.34 (1.3 in a similar evaluation from 2000 data pairs, N = 37) with a standard deviation of \pm 0.25. The cases with ratio less than 1 indicate higher concentrations at the urban background locations compared to the traffic exposed locations, which obviously excludes the use of these station pairs for this kind of analysis.



Figure 1.3. Frequency distribution of ratios of PM_{10} levels (annual means, $\mu g/m^3$) at traffic exposed sites and in the urban background. Data from AirBase, 2001. Only pairs of data from the same city were taken into account. N = 89.

In the majority of cases, the number of "exceedance days" at traffic exposed sites is also considerably higher compared with to urban background (Figure 1.4). On average, there were 11.6 extra exceedance days (range up to 43 days).



Figure 1.4. Extra days of PM_{10} daily means > 50 µg/m³ at traffic exposed sites compared to the urban background. Data from AirBase, 2001. Only pairs of data from the same city were taken into account. N = 89.

The relationship between the annual average PM_{10} concentration and number of exceedances of the stage 1 and stage 2 short term (daily) limit values is shown in Figure 1.5, for street/road side (traffic) stations. The figure shows that the spread around the regression line is fairly limited, but that there are stations where the short term levels fall considerably above the line.

A special case is Hornsgatan in Stockholm, which shows up in the figure as the spot with very high short term value, i.e. the 36th and the 8th highest day. This is most probably due to road dust emissions created by the extensive use of studded tyres. Streets in Nordic countries are not well represented in AirBase. More street stations from Norway, Sweden and Finland would probably show similar feature as Hornsgatan. Other stations that are well above the regression line are Spanish stations, where the problem of re-suspended dust is also pronounced, although from a very different source.



PM₁₀ at traffic stations

Figure 1.5. Exceedances of PM_{10} annual and short term limit values (stage 1, squares and indicative values of stage 2, rhombus) at European street monitoring stations for the year 2001. Annual average vs highest 36th and 8th daily mean.

1.2.2.2 Selection of station pairs for this study

At station pairs to be selected for further analysis in this project, data from monitoring of the following parameters should all be available, as hourly averages over a period of at least several months, preferably one full year, as a minimum:

Concentration data: - PM₁₀, NO_x, NO₂, preferably also PM_{2.5}, O₃, CO

Traffic data: - traffic volume

- traffic speed
- vehicle composition
- data related to re-suspension (e.g. studded tyre use)
- preferably also cold start fraction
- vehicle fleet data (age, technology,...).

| Street/station configuration: | width, number of lanes, height of buildings, gradient station location relative to street: distance to kerb, intersection |
|-------------------------------|--|
| Meteorological data: | - wind speed and direction, temperature, preferably also parameters related to dispersion. |
| | The wind and temperature data should be representative |
| | for the area where the station are located and not situated within the street area. |

Table 1.3 gives an overview of station pairs which have been analysed in this project: station pairs in Stockholm, Berlin, London, Oslo and Thessaloniki.

Data from the Goettinger Strasse station pair in Hannover has recently been made available to this project and has been analysed. Apparent data quality issues have not yet been solved, which prevents the results to be used in the current report.

For Prague, available data series were evaluated, but a suitable station pair with traffic data is not available so far. A new station pair has been established recently (spring of 2004) which could provide suitable data for this project. Madrid, Milan, Copenhagen and Paris were also investigated for suitable station pairs. Those were found, but for most of these cities the necessary traffic data were not available. Thus these cities could not be considered in the current analysis. There are additional station pairs with data available in Helsinki, London, Madrid and Athens from campaigns carried out as part of the OSCAR project (http://www.eu-oscar.org/).These are 2-month long measurement periods during winter and summer separately.

Data from all these cities and station pairs would broaden the assessment and could be added to this analysis at a later stage.

Table 1.1. Selected station pairs and data years.

| City | Street station | Street type | Background station | Annual average daily traffic (AADT) vehicles/day | Data collected | Year | Period |
|--------------|-------------------|--------------------------------|--|--|--|------|-----------------------|
| Stockholm | Hornsgatan | Canyon | Roof-top (near street) | 34,800 ¹ | A.Q.: PM ₁₀ , PM _{2.5} , NO ₂ , NO _x Traffic: Vol., Speed, Composition Met. Data: Wind speed, Wind dir. Modelling available | 2000 | January - December |
| | | | | | | | |
| Oslo | Skaarer | "Open" | Ground level station nearby | 35,900 | A.Q.: PM ₁₀ , NO _x , NO ₂ , Traffic: Vol., Speed, Composition Met. Data: Wind speed, Wind dir. Modelling to be done | 2002 | January - April |
| | | | | | | | |
| Berlin | Frankfurter Allee | Canyon | Ground level station in the area | 56,000 | A.Q.: PM ₁₀ , NO _x , NO ₂ , CO Traffic: Vol., Speed Met. Data: Wind speed, Wind dir., Radiation, Temp., Delta temp. Modelling?? | 2002 | January - December |
| Thessaloniki | Ermou street | Close to street crossing | University, Thessaloniki | 13,500 ² | A.Q.: PM ₁₀ , NO _x , NO ₂ Traffic: Vol., Speed, Composition Met. Data: Wind speed, Wind dir., Temp. | 2001 | January - December |
| London | Marylebone Rd. | Canyon | Ground level station nearby (Bloomsbury) | 85,500 | A.Q.: PM ₁₀ , PM _{2,5} , NO ₂ , NO _x , NO, CO, SO ₂ , O ₃ Traffic: Vol., Speed, Composition Met. Data: | 2000 | January - December |

 $^{^{1}}$ Traffic was only counted in one direction during this period, but manual and more detailed traffic counts indicate that this direction has about 5% to 10% higher counts compared to the other direction. Nevertheless the counted number for 2001 (17,400) has been multiplied with a factor 2 to evaluate the total number of vehicles in Hornsgatan.

 $^{^{2}}$ The station at Ermou street is located close to a roundabout. Even though 13,500 cars pass the station in the Ermou street, there is 22,500 cars passing close to the station when the roundabout is included.

1.2.3 Data analysis

The basic objective of subtask 3 is to study the excess concentrations at street hotspot (traffic) stations (DeltaC: street concentration minus UB concentration) calculated from carefully selected station pairs, to provide the basis for:

- evaluation of vehicle class emission factors, such as from COPERT
- comparison for dispersion/calculation models for street/road (line) configurations
- estimation of emission factors for resuspended road dust.

For the validation of emission factors, the following analysis of the data is carried out:

- The data collected from the station pairs include, to the extent available, hourly time series for an entire recent year, of concentrations, traffic parameters and meteorological parameters (as listed in section 1.2.2.2);
- To some extent, from some of the cities, some of the parameters are only available as daily data, or even annual data (i.e. for traffic parameters);
- From the data available, the following is calculated:
- annual and monthly averages;

- average variation over the hours of the day (24 hours) and maximum concentration per hour;

- this calculation is made for separate periods: winter and summer, workdays and weekends. Such a distinction separation enables the evaluation of emission factors for light and heavy duty vehicles separately and also elucidates the effect of the resuspension PM source, as separate from the vehicle exhaust source.

These calculations are made for combinations of data series, resulting in the following "end" results:

- concentration statistics for each time series separately (e.g. PM_{2.5} at the street station and background station separately);
- "Delta concentrations" ("DeltaC": street background);
- "Delta ratios" (DRs): ratio between the DeltaCs, for each component compared to the DeltaNO_x.

In terms of providing the background for validation of emission factors, the DRs provide the main basis for comparison between the emission factors from various emission factor databases and the key results provided by the analysis in this report.

The DeltaC results themselves could also provide a basis for emission factor validation for individual streets, if a dispersion model for the street had already been validated, using for instance tracer substances emitted with known source strength.

For the *validation of line source dispersion models*, for street canyons or "open" street locations, the time series of concentrations and DeltaC provide the basis for this.

The database prepared under this project includes data from a number of carefully selected station pairs from various cities. The street canyons have different dimensions, the traffic amount varies over a large range and the climate/ meteorological conditions also vary over a large range. Therefore, this database enables the comparison of DeltaCs for various compounds ($PM_{2.5}$, PM_{10} , NO_x , NO_2 , CO) for differing streets, traffic and dispersion conditions characterised by parameters such as e.g. height/width ratio, traffic speed, average wind and dispersion parameters.

1.2.4 Synthesis of results from the selected station pair data analysis

The purpose of this synthesis chapter is to present extracted and summarised data from each station pair considered suitable for comparison, in such a way which is appropriate and sufficient for use in further subtasks of the project.

1.2.4.1 Station metadata

This includes the following:

- street/building topography
- street and urban background station locations
- traffic characteristics of the street
- meteorology characteristics of the area
- measurement methods and QA/QC procedures

Table 1.4 summarises the essential station metadata.

| Station pair | Method | Correction | Data used |
|--------------|----------------------|-------------------------|-----------------------|
| | | factor | |
| Stockholm | TEOM | | Uncorrected data used |
| London | TEOM | PM ₁₀ : 1.3 | Corrected data used |
| | | PM _{2.5} : 1.0 | |
| Oslo | Street: TEOM | PM ₁₀ : 1.1 | Uncorrected data used |
| | Background: Partisol | | |
| Berlin | Beta absorption | N/A | Corrected data used |
| Thessaloniki | Beta absorption | | Uncorrected data used |

Table 1.2. PM measurement methods.

Data quality

The quality of the data and the QA/QC procedures used to produce the final time series that were used in this project, is the reponsibility of the providers of the data. Many of the stations from which data were reported are stations which are also included in the AirBase database of the EEA-ETC/ACC. It was assumed that the quality of the air pollution concentration data was generally good and that proper QA/QC procedures had been used. When working with the data, to some extent the data were checked for peaks, holes, time consistency and other irregularities. Some problems were encountered and were evaluated to have little consequence to the correctness of the results obtained from analysing the time series.

Regarding the traffic data, it was concluded that the data quality needs to be checked. This is especially so for the data on the heavy duty (HDV) fraction.

Brief evaluation of the station pairs

Stockholm

The Hornsgatan station pair represents a well defined street canyon in a central urban area in a Scandinavian capital city, with 2-way traffic. The street has a gradient of about 2%. The background station is on a roof-top nearby and thus well located. The meteorological data are from this station. The compound and time coverage is good. NO_x, NO, NO₂ and CO are measured on both sides of the street. The measurements on the uphill side of the street were selected for this analysis, because the pollutant coverage was better there (as it included PM_{10} and $PM_{2.5}$ measurements). Time series were available for two years (2000 and 2001) and the year 2000 was selected because of the availability of PM_{25} data and the otherwise fairly complete time series of the needed parameters. The traffic data covered only the uphill traffic. These data were multiplied by a factor 2, to obtain a good estimate for the full traffic volume in the street. Annual average daily traffic (AADT) is 34,800. Manual counting and automatic counting from periods when the traffic counters at all lanes were working properly showed that the traffic in the westerly direction is about 5% to 10% higher compared to the eastward traffic, as an annual average. Average speed is 45 km/h and the heavy duty fraction is 5%. The number of heavy duty vehicles in Hornsgatan are almost entirely ethanol fuelled city buses. The diesel (taxi) fraction of light duty vehicles is about 5%.

At this station pair, there is considerable contribution to PM_{10} from suspension of road dust, created by the use of studded (spiked) tyres on a substantial fraction (about 70%) of the light duty vehicles.

London

The Marylebone station pair represents a well defined, horizontal street canyon in central London, with 2-way traffic. The background station, Bloomsbury, is an urban background station and is located 2km east of Marylebone Rd., but was the closest urban background for which data was available. The meteorological data are from station 1.89 miles east of the Marylebone canyon. Its representativeness must be evaluated. Data were available for the years 2000 and 2001. The year 2000 was chosen because of the best coverage of pollutant compounds. PM_{2.5} and ozone were measured at both stations. The traffic data are fairly complete and of good coverage. AADT is 85,500. The average traffic speed is about 40 km/h and the heavy duty fraction is 10.3%.

Berlin

The Frankfurter Allee station pair represents a well defined, horizontal street canyon in a central urban area, with 2-way traffic. Data is available for 2002. $PM_{2.5}$ is not measured, only PM_{10} measurements are available. The background station is at Neukölln, Nansenstrasse, 3.7 km away from Frankfurter Allee. Hourly traffic data include total vehicle count. The velocity is given as average speed for each hour and for each direction, there is no hourly data collected for Frankfurter Allee. The heavy duty fraction is given as a constant value. The AADT is 56,000, the average traffic speed is 40 km/h and the heavy duty fraction is 4.8%.

Thessaloniki

The Ermou pair repesents a situation where the street station is located at the mouth of a street where it enters into a round-about. The background station for NO_x and NO_2 is an urban background station located 700 meters away from the street station. The background station for PM_{10} is located outside town, thus this pair does not represent a well defined street configuration suitable for model testing, but the data can be used for DR calculations as a basis for validating emissions factors, providing the traffic flow passing near the station (which includes both the traffic in the Ermou street itself as well as the traffic in the roundabout) can be well defined in terms of traffic volume, speed and heavy duty fraction.

Oslo

The measurement campaign providing the data was carried out to measure the concentrations as a function of distance from the road. The pair represents a well defined horizontal highway situation with high traffic speed (average about 90 km/h) in a suburban area. The concentrations were measured at 3 distances downwind of the main wind direction and at a background station well upwind of the road. Here the measurements span only about 3 months (winter conditions). Meteorological and traffic data are fully covered. AADT is 35,900, the average speed is 91 km/h and the heavy duty fraction is 6.0 %.

A shortcoming here is that, due to the fact that not enough instruments were available, the PM_{10} at the background station was measured as 12-hour averages and not hourly, as was done at the road station.

As in Stockholm, a fraction of the vehicles use studded tyres, so there is a significant contribution to PM concentrations from suspension of road dust originating from the wear of the road surface (asphalt) by the tyres. The fraction of cars using studded tyres in Oslo was about 25% in 2002, while in Stockholm this fraction is much higher, about 70%.

| City | Year | Statio | Str | eet topogra | phy | | Traffic | Meteorology ^a (annual average) | | | |
|--------------|------|----------------------|-----------------------------|-----------------|---------------------------|----------------------------|-----------------|--|------------------------|------------------------|--------------|
| | | Street | Background | Width (m) | Building height (m) | No. of traffic lanes | AADT veh/day | Aver. speed (km/h) | HDV fraction (%) | Wind speed (m/s) | Temp (°C) |
| Stockholm | 2000 | Hornsgatan | Roof | 22 | 20 | 4 | 34,800 | 47 | 5.0 | 3.5 | 10.7 |
| London | 2000 | Marylebone Rd. | Bloomsbury | 35 | 22 | 6 | 85,500 | 40 | 10.3 | 5.2 | 12.2 |
| Oslo | 2002 | Skaarersletta | Nordby | 19.4 | 0 | 4 | 35,900 | 91 | 6.0 | 1.2 | 0.1 |
| Thessaloniki | 2001 | Ermou | University, Thessaloniki | 40 ^b | 25 | 4 | 22,500 | 19 | 9.6 | 2.1 | 17.3 |
| Berlin | 2002 | Frankfurter Allee | Neukoelln station | 42 | 21 | 6 | 56,000 | 40 | 4.8 | 2.9 | 9.8 |

 Table 1.3. Overview of stations pair metadata.

^a Representative for the area where the station pair is located. ^b Station located at end of street canyon.

1.2.4.2 Synthesis of air pollution concentrations

Annual averages

Table 1.4 gives summarised long term averaged data (annual averages, or in case of Oslo, winter average), for DeltaC and DRs, for the station pairs with such data available so far.

The fairly large differences in DeltaC values reflect mainly the differences in AADT and whether it is a street canyon or open road, as well as the vehicle speed and the heavy duty vehicle (HDV) fraction and also differences in the average wind speed. For PM_{10} , the differences between station pairs also reflect the use (or not) of studded tyres.

Note that the PM_{10} data made available for the SEC project is not entirely consistent in terms of correction factors for measurements methods. London and Berlin data has been corrected, the other station data were delivered uncorrected. This obviously affects the DR for PM_{10} and needs to be considered when comparing the DR from the different station pairs.

In the DR values, the AADT, street configuration and wind speed differences are in principle eliminated and the differences should reflect the differences in average emission factor ratios for the traffic flows due to differences in speed and HDV fraction.

The DR values for $PM_{2.5}$ for Marylebone Rd. are some 20% higher than in Hornsgatan. The traffic speed is about the same in the two streets. HDV fraction is twice higher in Marylebone (and in Hornsgatan the HDV vehicles are dominated by buses run on ethylene with low PM emissions) while the road dust contribution should be higher in Hornsgatan because of the studded tyres used there. These two influences seem to be of the same magnitude and even each other out on the annual scale.

The DR values for NO_2 cover quite a large range. The DR is lowest in Marylebone Rd. and highest in Ermou Street, more than 3 times higher. The delta values and DRs for NO_2 are affected by the ozone concentrations in the area and in the street air, which is again affected by the road configuration (street canyon or not), which needs to be taken into account when comparing DRs for NO_2 in different streets.

The DR values for PM_{10} are high in Hornsgatan and Skaarer near Oslo, as expected, where studded tyres are used. It is also surprisingly high in Frankfurter Allee in Berlin.

The DR values are studied in more detail in the section below, based upon short-term data.

Hourly averages

Table 1.5 gives summarised short-term averaged data for DeltaC and DRs for the Stockholm, Oslo, London and Berlin station pairs.

DR values are given for 4 traffic situations: winter workdays and weekend days and summer workdays and weekend days. By doing this, the effects on emission factors

by temperature and road dust emission can be studied. Also, by separating workdays from weekend days, differences due to HDV fraction differences can be studied, enabling validation of light duty and HDV emission factors separately.

In Figures 1.6 – 1.9, DeltaC and DR data (relative to NO_x), are shown for Hornsgatan Stockholm, Marylebone Rd. London, Frankfurter Allee Berlin and Skaarersletta near Oslo. Data are presented in terms of average numbers per hour-of-day, for winter and summer conditions and workdays and weekend days separately.

In Figures 1.10 - 1.13, data from these plots are extracted further, to give the average of the DRs for the middle 6 hours of the day (typically 10-15 o' clock, but can be one hour earlier or later, depending on the rush hours of the particular case study/street), for each of the season/workday-weekend combinations. This is shown for Hornsgatan, Marylebone Rd., Frankfurther Allee and Skaarersletta. The 6 middle-of-the-day hours have been selected to exclude the rush hours as well as with a view to the variation of the DRs over the day, so that a period with the smallest inter-hour variation in the DR is selected. This is done to select a period with as stable conditions as possible both regarding emissions and atmospheric conditions. The result of this is that the DRs will then be representative for emission and atmospheric conditions which can be reasonably well characterised, again enabling a better comparison with emission factor measurement/model based ratios.

There are significant differences in DRs between the four station pairs. Many of these are explained by the differences in traffic parameters and conditions, while some differences are surprising.

First we can compare Hornsgatan with Marylebone Rd., which have similar traffic speed, but Marylebone has twice the HDV fraction:

- The summer $PM_{2.5}$ DRs are much higher for Marylebone than for Hornsgatan, while the winter DRs are quite similar. The higher summer DRs in Marylebone could be explained by the higher HDV fraction (as well as the fact that the buses in Hornsgatan are ethanol fuelled). The similar winter DRs might be explained, considering that the re-suspension source should be much larger in the studded tyre city of Stockholm than in London, while the HDV fraction is higher in Marylebone.
- For PM₁₀, however, the summer DRs are not so different in the two cities (still more road dust in Stockholm?), while, as expected, the winter DR is much higher in Stockholm (more than 3 times higher!), again due to the road dust source.
- For NO₂, surprisingly, the DRs are higher in Stockholm than in London (while Marylebone in London has double the HDV fraction and is more southerly as well). Both places, the summer DR is higher than the winter DR, possibly reflecting the higher available ozone concentration in summer. The DRs are not much different on weekends than on workdays.

Frankfurter Allee in Berlin has 5% HDV fraction, same as in Hornsgatan, while Marylebone has 10%. The traffic speed in Frankfurter Allee is similar to the other streets.

- Frankfurter Allee has about twice as high PM_{10} DR compared to Marylebone. It would be interesting to test this result against emission factor models, that this is the result of the lower HDV fraction.
- Frankfurter Allee also has much higher NO₂ DR compared to Marylebone Rd.. Also this result should be tested against emission factor models. The differences between workday and weekend DRs are larger than in Marylebone Rd., and are similar to those for Hornsgatan.

At the Skaarer station pair, the PM_{10} DR for winter conditions is high, as expected due to use of studded tyres and at about the same level as in Hornsgatan in Stockholm. In Oslo, the fraction of cars using studded tyres was about 25% in 2002, while in Stockholm it was considerably higher in 2000 (about 70%). That the PM_{10} DR still is about the same at Skaarer reflects the higher traffic speed there (91km/h as opposed to 45 km/h in Hornsgatan). Higher speed causes increased road wear and road dust emissions. The NO₂ winter workday DR is lower than in Hornsgatan, while the weekend DR is a bit higher than in Hornsgatan. The effect of the open road configuration at Skaarer compared to the Hornsgatan street canyon will be evaluated. It would, however, be interesting to test this result against emission factor models, whether this difference can be explained by the differences in speed and HDV fractions in the two streets.

The emission factor for re-suspension of road dust can be estimated by comparing the DR from PM_{10} verses the $PM_{2.5}$, looking at differences between winter and summer. Considering the difference between the Scandinavian stations and stations in other countries, the re-suspension factor related to the use of studded tyres can be estimated. As the SEC project data become more complete, including more station pairs and $PM_{2.5}$ data, this will enable the estimation of an emission factor for re-suspension factors.

These results are compared to emission factor ratios from emission factor models in section 1.3. Additional data from further inclusion of street pairs will provide an improved basis for emission factor validations.

1.2.4.3 Estimation of the PM re-suspension source

The DR values for PM_{10} relative to those for $PM_{2.5}$ give a basis for estimating the resuspension source.

In Marylebone Rd., with no studded tyres (Figure 1.12), the DR for $PM_{2.5}$ and PM_{10} are both about the same for summer and winter, indicating that the PM sources in the street (vehicle exhaust, brake and tyre wear and dust re-suspension) are of about the same magnitude compared to the NO_x emissions irrespective of season (it is not likely that the average NO_x emissions factor differs much between summer and winter).

The DR for PM_{10} is 1.75 times higher than the DR for $PM_{2.5}$ in the summer and 2.08 times higher in the winter, averaged about 1.90 times higher. This gives the estimate that the re-suspension PM_{10} source in Marylebone Rd. is of about equal magnitude as the other particle sources (exhaust, brake and tyre wear). It will be further evaluated

whether the summer/winter difference in this factor is significant and could be explained.

In Frankfurter Allee in Berlin, where studded tyres are also not used (Figure 1.11), there is also no summer-winter difference in the DR for PM_{10} . Here $PM_{2.5}$ has not been measured throughout the year, but results from shorter campaigns here could be looked into. The DR for PM_{10} is more that 2 times higher than in Marylebone Rd. in London. This, combined with the lower HDV fraction in Frankfurter Allee, indicates a much larger non-exhaust/re-suspension PM source there than in Marylebone Rd..

Looking at Hornsgatan in Stockholm with studded tyres use (Figure 1.10), there are large winter-summer differences in DR, especially for PM_{10} , but also for $PM_{2.5}$. Road dust re-suspension in streets where studded tyres are used affect also the $PM_{2.5}$ level. The DR for $PM_{2.5}$ is 1.5 higher in winter than in summer.

The DR for PM_{10} is, averaged over all days, 3.3 times higher than DR for $PM_{2.5}$ in summer and 6.5 times higher in winter. The DR for PM_{10} is 3.0 times that in the summer, averaged over all days.

This indicates a road dust re-suspension source in Hornsgatan which is responsible for a considerable $PM_{2.5}$ emission even in summer and a very strong PM_{10} emission in winter and a significant source also in summer.

These estimates of the magnitude of the PM re-suspension source compared to the exhaust/brake/tyre wear PM source will be studied further, as soon as data from Goettinger Strasse and Helsinki have also been analysed. Based upon such analysis the re-suspension source can be quantified relative to the exhaust/brake/tyre wear source.

Chapter 1

| Street | Period | AADT | Speed | HDV | WS | Delta | aC (Street - (μg/ | – backgrou ′m³) | und) ^a | Delta ratios | | | |
|----------------------|--------------|------------|--------|------|-------|--------------------------------------|--|--------------------------|-------------------------|--|-------------------------------------|--|--|
| | 1 01100 | (veh./day) | (km/h) | (%) | (m/s) | NO _x | NO_2 | PM _{2.5} | PM ₁₀ | <u>PM_{2,5}</u> NO _x | PM ₁₀ NO _x | $\frac{NO_2}{NO_x}$ | |
| Hornsgatan | Year 2000 | 34,800 | 45 | 5.0 | | 155 | 29.8 | 5.2 | 24.5 | 0.033 | 0.158 | 0.192 | |
| Skaarersletta | Winter 2002 | 35,900 | 90 | 6.0 | | 104 ^b 144 ^c | 14.3 ^b 19.7 ^c | - | 31.3 ^c | - | 0.217 | 0.14 ^b 0.14 ^c | |
| Marylebone Rd. | Year 2000 | 85,500 | 40 | 10.3 | | 305 | 33.7 | 11.7 | 20.5 | 0.038 | 0.067 | 0.110 | |
| Ermou Street | Year 2001 | 22,500 | 20 | 9.6 | | 39.6 | 15.7 | - | 36.9 ^d | - | | 0.396 | |
| Frankfurter Allee | Year 2002 | 56,000 | 45 | 4.8 | | 59 | 16.5 | - | 9.6 | - | 0.163 | 0.279 | |

 Table 1.4. Synthesis of long-term average data.

^a Difference between annual average at street station and annual average at background station.
^b Based on hourly data.
^c Based on 12 hours average data (daytime only).
^d Background station for PM₁₀ at Thessaloniki is outside town and hence not suitable for this study.

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| Street | Period | DeltaC (Street – background) ^a (µg/m ³) | | | | Delta ratios | | | Limit value indicators, annual based | | | | |
|--------------------------|--------------------|--|-----------------|-------------------|------------------|--------------------------------------|-------------------------------------|-------------------------------|--------------------------------------|------------------------------|-------------------------------|-----------------------------|--|
| | | NO _x | NO ₂ | PM _{2,5} | PM ₁₀ | PM _{2,5} NO _x | PM ₁₀ NO _x | <u>NO2</u> NO _x | NO ₂ –18. hour | PM ₁₀ –35. day | PM _{2.5} –35. day | PM ₁₀ –7. day | |
| | Summer Workdays | 237 | 48.0 | 7.2 | 23.3 | 0.030 | 0.098 | 0.202 | | | 21 | | |
| Hornsgatan | Summer Weekend | 138 | 34.4 | 3.1 | 10.7 | 0.023 | 0.078 | 0.249 | 136 | 88 | | 127 | |
| 2000 | Winter Workdays | 271 | 40.9 | 10.9 | 67.8 | 0.040 | 0.251 | 0.151 | 130 | | | 127 | |
| | Winter Weekends | 180 | 29.5 | 7.9 | 55.1 | 0.044 | 0.306 | 0.165 | | | | | |
| Skaarersletta Jan Mar | Winter Workdays | 159 | 18.4 | - | - | - | - | 0.117 | 84 ^b | 41 ^b | - | 84 ^b | |
| 2002 | Winter Weekends | 60.1 | 10.7 | - | - | - | - | 0.179 | | | | 04 | |
| | Summer Workdays | 460 | 61.7 | 18.7 | 34.2 | 0.041 | 0.075 | 0.134 | 239 | | 27 | | |
| Marylebone Rd | Summer Weekend | 214 | 29.4 | 9.9 | 16.4 | 0.047 | 0.077 | 0.138 | | 67 | | 80 | |
| 2000 | Winter Workdays | 400 | 44.5 | 15.6 | 31.0 | 0.039 | 0.078 | 0.111 | | 07 | 57 | 07 | |
| | Winter Weekends | 212 | 37.4 | 7.9 | 17.2 | 0.037 | 0.081 | 0.106 | | | | | |
| Ermou Street 2001 | | | | | | | | | 173 | 53 | - | 117 | |

Table 1.5. Synthesis of short-term average data (hour, day).

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| Frankfurter Allee 2002 | Summer Workdays | 97.9 | 34.1 | - | 15.9 | - | 0.16 | 0.35 | | | - | 227 |
|------------------------------|--------------------|-------|------|---|------|---|------|------|-----|-----|---|-----|
| | Summer Weekend | 45.6 | 20.5 | - | 8.4 | - | 0.19 | 0.45 | 107 | 162 | | |
| | Winter Workdays | 107.4 | 21.3 | - | 19.7 | - | 0.18 | 0.20 | 127 | | | |
| | Winter Weekends | 50.6 | 11.9 | - | 8.9 | - | 0.18 | 0.23 | | | | |

^a Delta for each separate hour, then averaged over the included hours. ^b Only from 4 winter months.



Hornsgatan, Stockholm

Figure 1.6. Average concentration variation over the day, Hornsgatan, Stockholm, DeltaC and delta ratio (DR) relative to NO_x .



Marylebone Rd., London

Figure 1.7. Average concentration variation over the day, Marylebone Rd., London, DeltaC and delta ratio relative to NO_x .



Frankfurter Allee, Berlin

Figure 1.8. Average concentration variation over the day, Frankfurter Allee, Berlin, DeltaC and delta ratio relative to NO_x .



Skaarersletta, Oslo

Figure 1.9. Average concentration variation over the day, Skaarersletta, Oslo, DeltaC and delta ratio relative to NO_{x} . These graphs are for only four months of data (January – April).



Hornsgatan, Stockholm

Figure 1.10. Delta ratios for $PM_{2.5}$, PM_{10} and NO_2 relative to NO_x , for Winter and Summer conditions at Hornsgatan. Red columns: workdays. Blue columns: weekend days.



Frankfurther Allee, Berlin

Figure 1.11. Delta ratios for PM_{10} and NO_2 relative to NO_x , for Winter and Summer conditions at Frankfurter Allee. Red columns: workdays. Blue columns: weekend days.



Marylebone Road, London

Figure 1.12. Delta ratios for $PM_{2.5}$, PM_{10} and NO_2 relative to NO_x , for Winter and Summer conditions at Marylebone Rd. Red columns: workdays. Blue columns: weekend days.

Skårersletta



Figure 1.13. Delta ratios for PM_{10} and NO_2 relative to NO_x , for Winter conditions at Skaarersletta. Red columns: workdays. Blue columns: weekend days. Green column: whole all weekdays.

1.3 Local emission estimates

1.3.1 Introduction

The present subtask aims at contributing to the analysis of excess concentrations by providing data derived from emission estimation models to be compared with monitored data. For the interpretation of the analysis of excess concentrations in terms of local emission estimates, the application of the COPERT 3 methodology for the estimation of street emissions from road transport has been used. For this purpose a local scale calculation module was derived from COPERT, which was able to account for street level activity data. Traffic data monitored at the selected street stations (traffic volume and speed, vehicle composition) are used as input to the calculation module. The traffic volume is usually split into two major vehicle types, i.e. passenger cars and heavy duty vehicles (HDV), differentiated by the different vehicle length. In order to further distribute the number of cars monitored into all COPERT categories, accounting thus for the various vehicle classes and technologies, results from the TRENDS model were also used.

1.3.2 Hornsgatan, Stockholm

1.3.2.1 Basecase

Using the composition of the Swedish vehicle fleet for the year 2000 extracted from the TRENDS database, the share of each vehicle category is derived. The detailed monthly (Table A.1) and hourly (Tables A.2 & A.3) distribution of traffic into the various vehicle categories is presented in Annex A. (Note: The tables in Annex A are based upon the provided total traffic data, which cover only the traffic in one (the uphill) direction. In Figures 1.14-1.21 and the calculations on which these are based, this traffic is multiplied by 2, to account for the traffic in both directions).

As the street canyon is located in downtown Stockholm, it is assumed that only HDV with a Gross Vehicle Weight (GVW) lower than 16 tonnes were allowed, i.e. the share of HDV with a GVW of 16-32 tonnes and over 32 tonnes was set equal to zero. The 20% share of buses as part of total HDV, given by the TRENDS model, agrees well with the traffic counts in Hornsgatan, which gives 23% (Christer Johansson, personal communication). Added to this, all buses are run on ethanol, which was taken into account using appropriate emission factors. In total, six sets of runs were performed with COPERT, five for the hourly distribution and one for the monthly distribution of traffic emissions. The basic set of runs takes all days of the year into account for the calculations. Two more sets of runs were performed differentiating between workdays and weekends during winter time and another two for summer time. An additional set of runs was performed for the monthly distribution of traffic emissions, considering all days of the year. From the monitored traffic data, average hourly and monthly data were derived for the number of passenger cars, the heavy duty fraction and the average vehicle speed. For the calculations performed, the mileage of the vehicles was set equal to the length of the street canyon (160 m).

As an example of the COPERT application, the composition of the HDV, buses and coaches fleet in January, as its results from the TRENDS database, is presented in Table 1.6 showing the split in the various weight and classes according to legislation.

| Туре | Class | Legislation | Jan |
|------|--------------------|-------------------------------|------|
| | Gasoline >3,5 t | Conventional | 0 |
| | Diesel 3,5 - 7,5 t | Conventional | 6203 |
| | | Euro I - 91/542/EEC Stage I | 1441 |
| | | Euro II - 91/542/EEC Stage II | 2063 |
| | | Euro III - 2000 Standards | 0 |
| les | Diesel 7,5 - 16 t | Conventional | 6815 |
| hic | | Euro I - 91/542/EEC Stage I | 1583 |
| Ve | | Euro II - 91/542/EEC Stage II | 2266 |
| uty | | Euro III - 2000 Standards | 0 |
| Ď | Diesel 16 - 32 t | Conventional | 0 |
| avy | | Euro I - 91/542/EEC Stage I | 0 |
| He | | Euro II - 91/542/EEC Stage II | 0 |
| | | Euro III - 2000 Standards | 0 |
| | Diesel >32t | Conventional | 0 |
| | | Euro I - 91/542/EEC Stage I | 0 |
| | | Euro II - 91/542/EEC Stage II | 0 |
| | | Euro III - 2000 Standards | 0 |
| | Urban Buses | Conventional | 3231 |
| es | | Euro I - 91/542/EEC Stage I | 315 |
| ach | | Euro II - 91/542/EEC Stage II | 409 |
| Co | | Euro III - 2000 Standards | 0 |
| s. | Coaches | Conventional | 808 |
| use | | Euro I - 91/542/EEC Stage I | 79 |
| Ē | | Euro II - 91/542/EEC Stage II | 102 |
| | | Euro III - 2000 Standards | 0 |

Table 1.6. Heavy Duty Vehicles, buses and coaches composition, estimated from the TRENDS database for Hornsgatan, Stockholm, for January.

The calculated year averaged hourly vehicle emissions of CO, NO_x and PM_{2.5} and the measured DeltaCs of NO_x and PM_{2.5} are presented in Table 1.7. As practically all PM emitted by road vehicles are in the fine fraction, the entire PM emissions are considered as $PM_{2.5}$ and thus PM_{10} emissions are not separately examined in the present study, since the results will be identical to $PM_{2.5}$. From the above emissions and DeltaCs, $PM_{2.5}$ over NO_x and CO over NO_x emission ratios are produced, on an hourly basis and are presented in the same table. It has to be noted that the emissions calculated include hot emissions only as it is assumed that the cold start effect should be negligible in the specific street canyon.

In order to assess the differences between working days and weekends, as well as between summer and winter, hourly emission values and derived ratios are presented in Table 1.8 and Table 1.9.
Table 1.10 shows the calculated monthly variations in the mean hourly traffic emissions of CO, NO_x and $PM_{2.5}$ and the atmospheric concentration deltas of NO_x and $PM_{2.5}$. The derived $PM_{2.5}$ over NO_x ratios are also shown.

Table 1.7. Calculated hourly year averaged traffic emissions versus monitored hourly year averaged delta concentrations in Hornsgatan, Stockholm.

| | | | Emission | ns (g) | | Conce | entration | s (µg/m ³) |
|-------|--------|-----------------|-------------------|------------------------------------|--------------------|-----------------|-------------------|------------------------------------|
| Hour | СО | NO _x | PM _{2.5} | PM _{2.5} /NO _x | CO/NO _x | NO _x | PM _{2.5} | PM _{2.5} /NO _x |
| 01:00 | 435.9 | 108.8 | 1.8 | 0.017 | 4.007 | 77.8 | 3.0 | 0.039 |
| 02:00 | 382.0 | 103.8 | 2.1 | 0.021 | 3.682 | 78.6 | 3.4 | 0.043 |
| 03:00 | 306.7 | 86.4 | 1.9 | 0.023 | 3.549 | 62.4 | 2.9 | 0.046 |
| 04:00 | 262.9 | 76.2 | 1.7 | 0.023 | 3.451 | 63.4 | 2.6 | 0.041 |
| 05:00 | 191.5 | 57.2 | 1.5 | 0.026 | 3.347 | 42.1 | 1.9 | 0.045 |
| 06:00 | 219.3 | 63.8 | 1.6 | 0.025 | 3.435 | 57.6 | 1.7 | 0.030 |
| 07:00 | 618.6 | 160.3 | 3.5 | 0.022 | 3.859 | 141.9 | 3.9 | 0.027 |
| 08:00 | 1206.8 | 276.1 | 6.5 | 0.024 | 4.370 | 208.7 | 6.3 | 0.030 |
| 09:00 | 1328.9 | 300.5 | 7.4 | 0.025 | 4.422 | 215.0 | 7.2 | 0.033 |
| 10:00 | 1183.1 | 276.7 | 7.0 | 0.025 | 4.275 | 209.7 | 6.8 | 0.032 |
| 11:00 | 1327.0 | 305.5 | 7.6 | 0.025 | 4.344 | 195.3 | 7.4 | 0.038 |
| 12:00 | 1521.6 | 334.9 | 8.4 | 0.025 | 4.544 | 208.7 | 7.4 | 0.035 |
| 13:00 | 1698.8 | 361.7 | 8.9 | 0.025 | 4.697 | 223.6 | 8.0 | 0.036 |
| 14:00 | 1739.1 | 370.3 | 9.1 | 0.025 | 4.697 | 223.2 | 8.2 | 0.037 |
| 15:00 | 1819.4 | 383.7 | 9.4 | 0.024 | 4.741 | 225.7 | 8.0 | 0.035 |
| 16:00 | 1990.4 | 412.6 | 10.1 | 0.024 | 4.824 | 232.2 | 8.2 | 0.035 |
| 17:00 | 2037.0 | 411.5 | 9.7 | 0.024 | 4.950 | 224.5 | 7.3 | 0.033 |
| 18:00 | 1791.3 | 363.9 | 7.9 | 0.022 | 4.923 | 196.2 | 6.2 | 0.032 |
| 19:00 | 1467.6 | 307.8 | 6.1 | 0.020 | 4.768 | 167.4 | 5.4 | 0.032 |
| 20:00 | 1159.8 | 253.6 | 4.9 | 0.019 | 4.573 | 150.0 | 4.8 | 0.032 |
| 21:00 | 1002.9 | 217.9 | 3.8 | 0.017 | 4.602 | 131.8 | 4.0 | 0.030 |
| 22:00 | 942.1 | 204.7 | 3.5 | 0.017 | 4.602 | 126.0 | 4.0 | 0.032 |
| 23:00 | 731.8 | 163.9 | 2.8 | 0.017 | 4.465 | 109.1 | 3.6 | 0.033 |
| 24:00 | 599.1 | 139.5 | 2.3 | 0.017 | 4.295 | 95.9 | 3.3 | 0.034 |

| | | Woi | kdays - | summer | | Workdays - winter | | | | |
|-------|--------|-------|-------------------|------------------------------------|--------------------|-------------------|-------|-------------------|------------------------------------|--------------------|
| Hour | СО | NOx | PM _{2.5} | PM _{2.5} /NO _x | CO/NO _x | СО | NOx | PM _{2.5} | PM _{2.5} /NO _x | CO/NO _x |
| 01:00 | 533.2 | 128.3 | 2.2 | 0.017 | 4.156 | 458.6 | 108.7 | 1.9 | 0.018 | 4.220 |
| 02:00 | 349.4 | 90.2 | 1.6 | 0.018 | 3.873 | 328.1 | 82.8 | 1.4 | 0.017 | 3.964 |
| 03:00 | 285.4 | 80.5 | 1.8 | 0.022 | 3.544 | 260.5 | 71.6 | 1.6 | 0.023 | 3.636 |
| 04:00 | 205.9 | 61.3 | 1.5 | 0.024 | 3.360 | 194.0 | 56.2 | 1.4 | 0.025 | 3.453 |
| 05:00 | 171.7 | 52.2 | 1.3 | 0.025 | 3.291 | 168.7 | 49.5 | 1.3 | 0.025 | 3.407 |
| 06:00 | 129.1 | 41.2 | 1.1 | 0.027 | 3.132 | 132.6 | 40.0 | 1.2 | 0.029 | 3.312 |
| 07:00 | 201.0 | 59.6 | 1.6 | 0.026 | 3.372 | 190.4 | 54.1 | 1.5 | 0.028 | 3.517 |
| 08:00 | 763.2 | 196.6 | 4.6 | 0.024 | 3.881 | 792.0 | 194.4 | 4.4 | 0.023 | 4.075 |
| 09:00 | 1503.6 | 337.3 | 8.6 | 0.025 | 4.457 | 1646.2 | 345.5 | 9.0 | 0.026 | 4.764 |
| 10:00 | 1601.8 | 361.4 | 9.9 | 0.027 | 4.432 | 1835.2 | 382.2 | 10.4 | 0.027 | 4.802 |
| 11:00 | 1332.8 | 315.8 | 8.9 | 0.028 | 4.220 | 1388.9 | 318.6 | 9.0 | 0.028 | 4.359 |
| 12:00 | 1415.2 | 335.6 | 9.5 | 0.028 | 4.216 | 1409.6 | 328.9 | 9.3 | 0.028 | 4.286 |
| 13:00 | 1551.8 | 353.6 | 10.1 | 0.029 | 4.388 | 1546.5 | 344.3 | 10.0 | 0.029 | 4.492 |
| 14:00 | 1618.0 | 363.8 | 10.0 | 0.027 | 4.448 | 1704.5 | 365.9 | 10.4 | 0.028 | 4.658 |
| 15:00 | 1682.1 | 373.8 | 10.4 | 0.028 | 4.500 | 1746.2 | 380.1 | 10.6 | 0.028 | 4.594 |
| 16:00 | 1785.3 | 392.6 | 10.9 | 0.028 | 4.547 | 1852.4 | 395.3 | 10.9 | 0.028 | 4.686 |
| 17:00 | 2008.8 | 432.7 | 12.2 | 0.028 | 4.643 | 2127.7 | 442.6 | 12.2 | 0.028 | 4.808 |
| 18:00 | 2096.3 | 434.6 | 11.6 | 0.027 | 4.824 | 2127.7 | 422.3 | 11.5 | 0.027 | 5.038 |
| 19:00 | 1830.3 | 379.2 | 9.2 | 0.024 | 4.826 | 1874.4 | 369.8 | 8.9 | 0.024 | 5.069 |
| 20:00 | 1474.0 | 316.3 | 6.8 | 0.021 | 4.660 | 1512.2 | 308.8 | 6.6 | 0.021 | 4.897 |
| 21:00 | 1175.2 | 262.5 | 5.4 | 0.021 | 4.476 | 1189.0 | 256.1 | 5.0 | 0.020 | 4.644 |
| 22:00 | 1020.6 | 224.1 | 4.1 | 0.018 | 4.553 | 1011.4 | 216.2 | 3.8 | 0.017 | 4.679 |
| 23:00 | 966.9 | 211.5 | 3.8 | 0.018 | 4.571 | 943.4 | 202.0 | 3.6 | 0.018 | 4.670 |
| 24:00 | 761.6 | 172.4 | 3.2 | 0.018 | 4.418 | 699.1 | 156.0 | 2.7 | 0.017 | 4.482 |

Table 1.8. Calculated hourly average traffic emissions and associated emission ratios for summer and winter working days in Hornsgatan, Stockholm.

Table 1.9. Calculated hourly average traffic emissions and associated emission ratios for summer and winter weekends in Hornsgatan, Stockholm.

| | | Wee | ekends - | summer | | | We | ekends | - winter | |
|-------|--------|-------|-------------------|------------------------------------|--------------------|--------|-------|-------------------|------------------------------------|--------------------|
| Hour | СО | NOx | PM _{2.5} | PM _{2.5} /NO _x | CO/NO _x | СО | NOx | PM _{2.5} | PM _{2.5} /NO _x | CO/NO _x |
| 01:00 | 719.0 | 162.4 | 2.6 | 0.016 | 4.428 | 725.6 | 162.2 | 2.7 | 0.016 | 4.473 |
| 02:00 | 630.5 | 148.2 | 2.4 | 0.016 | 4.255 | 671.4 | 153.6 | 2.5 | 0.016 | 4.370 |
| 03:00 | 620.1 | 160.4 | 3.0 | 0.019 | 3.867 | 682.7 | 165.8 | 3.3 | 0.020 | 4.118 |
| 04:00 | 515.4 | 137.9 | 2.5 | 0.018 | 3.738 | 669.6 | 162.6 | 3.2 | 0.020 | 4.118 |
| 05:00 | 458.9 | 127.7 | 2.4 | 0.018 | 3.594 | 495.3 | 129.3 | 2.5 | 0.019 | 3.832 |
| 06:00 | 289.5 | 84.4 | 1.8 | 0.022 | 3.429 | 302.7 | 84.0 | 1.9 | 0.022 | 3.603 |
| 07:00 | 215.4 | 66.4 | 1.7 | 0.025 | 3.246 | 210.4 | 62.6 | 1.6 | 0.026 | 3.358 |
| 08:00 | 175.9 | 49.1 | 1.0 | 0.020 | 3.580 | 188.7 | 49.8 | 1.1 | 0.021 | 3.787 |
| 09:00 | 226.0 | 59.7 | 1.3 | 0.021 | 3.788 | 243.4 | 61.8 | 1.4 | 0.022 | 3.937 |
| 10:00 | 321.8 | 81.8 | 1.6 | 0.020 | 3.934 | 334.3 | 83.2 | 1.7 | 0.020 | 4.017 |
| 11:00 | 519.1 | 126.5 | 2.6 | 0.020 | 4.104 | 535.1 | 128.8 | 2.6 | 0.020 | 4.155 |
| 12:00 | 832.1 | 190.7 | 3.7 | 0.019 | 4.363 | 857.3 | 194.3 | 3.8 | 0.020 | 4.412 |
| 13:00 | 1139.9 | 249.3 | 4.5 | 0.018 | 4.572 | 1190.9 | 254.0 | 4.7 | 0.019 | 4.688 |
| 14:00 | 1494.6 | 314.4 | 5.6 | 0.018 | 4.754 | 1487.9 | 301.8 | 5.5 | 0.018 | 4.930 |
| 15:00 | 1553.3 | 325.7 | 5.6 | 0.017 | 4.769 | 1636.9 | 325.0 | 5.9 | 0.018 | 5.037 |
| 16:00 | 1580.3 | 329.4 | 5.8 | 0.018 | 4.798 | 1668.4 | 331.3 | 6.0 | 0.018 | 5.037 |
| 17:00 | 1558.6 | 328.8 | 5.7 | 0.017 | 4.740 | 1691.2 | 333.7 | 6.0 | 0.018 | 5.068 |
| 18:00 | 1507.8 | 318.2 | 5.6 | 0.018 | 4.739 | 1615.1 | 323.3 | 5.9 | 0.018 | 4.996 |
| 19:00 | 1325.9 | 280.7 | 5.1 | 0.018 | 4.723 | 1423.1 | 291.3 | 5.4 | 0.019 | 4.885 |
| 20:00 | 1146.3 | 245.4 | 4.4 | 0.018 | 4.672 | 1213.0 | 254.8 | 4.6 | 0.018 | 4.760 |
| 21:00 | 928.0 | 203.8 | 3.6 | 0.017 | 4.553 | 981.8 | 211.6 | 3.7 | 0.018 | 4.639 |
| 22:00 | 811.6 | 176.9 | 2.9 | 0.016 | 4.587 | 981.8 | 211.6 | 3.7 | 0.018 | 4.639 |
| 23:00 | 780.9 | 172.0 | 2.9 | 0.017 | 4.540 | 771.0 | 168.6 | 2.8 | 0.017 | 4.574 |
| 24:00 | 617.5 | 139.8 | 2.3 | 0.017 | 4.415 | 595.8 | 134.4 | 2.3 | 0.017 | 4.432 |

| | | | Emission | ns (g) | | Concentrations (µg/m ³) | | | |
|-----------|--------|-----------------|-------------------|------------------------------------|--------------------|-------------------------------------|-------------------|------------------------------------|--|
| Month | СО | NO _x | PM _{2.5} | PM _{2.5} /NO _x | CO/NO _x | NO _x | PM _{2.5} | PM _{2.5} /NO _x | |
| January | 984.9 | 217.8 | 5.1 | 0.023 | 4.523 | 168.6 | 4.1 | 0.024 | |
| February | 1068.0 | 233.5 | 5.7 | 0.025 | 4.573 | 179.2 | 6.2 | 0.035 | |
| March | 1083.7 | 237.7 | 5.3 | 0.022 | 4.559 | 181.6 | 10.8 | 0.059 | |
| April | 1032.0 | 227.6 | 4.9 | 0.022 | 4.534 | 180.6 | 6.8 | 0.038 | |
| May | 1084.8 | 242.4 | 5.5 | 0.023 | 4.476 | 152.6 | 5.6 | 0.037 | |
| June | 983.1 | 223.3 | 5.3 | 0.024 | 4.402 | 141.7 | 3.5 | 0.025 | |
| July | 807.3 | 194.8 | 4.7 | 0.024 | 4.145 | 150.1 | 4.6 | 0.031 | |
| August | 1020.5 | 236.9 | 6.1 | 0.026 | 4.307 | 167.5 | 4.7 | 0.028 | |
| September | 1077.2 | 238.3 | 5.6 | 0.023 | 4.519 | 194.5 | 5.6 | 0.029 | |
| October | 1096.5 | 239.8 | 5.5 | 0.023 | 4.572 | 110.4 | 3.2 | 0.029 | |
| November | 1118.3 | 240.7 | 5.5 | 0.023 | 4.645 | 104.4 | 3.7 | 0.035 | |
| December | 1018.6 | 220.3 | 5.0 | 0.023 | 4.623 | 132.2 | 3.4 | 0.026 | |

Table 1.10. Calculated monthly average traffic emissions versus monitored monthly average delta concentrations in Hornsgatan, Stockholm.

Figure 1.14 shows the hourly variation over the day of the $PM_{2.5}$ over NO_x concentration ratio against the respective calculated emission ratio. Overall, the modelled emission ratio is lower than the respective calculated concentration ratio. The PM emissions calculated with COPERT do not take into account possible resuspension of road dust (but only exhaust emissions) and, as a result, the PM emissions calculated might be underestimated. This could explain the generally lower ratio as compared to the respective concentration ratio.

In Figure 1.15, the summer – winter and working days – weekend effects are shown. As expected, the $PM_{2.5}$ over NO_x emission ratio is lower during the weekends, which is consistent with traffic without (or very low) HDV share. On the other hand workdays are associated with higher $PM_{2.5}$ over NO_x emission ratios. The effect of the season is negligible in the calculated emission ratios.

In Figure 1.16, the variation over the year in monthly averages of the concentration ratio between the deltas of $PM_{2.5}$ and NO_x are plotted against the respective calculated emission ratio. This figure provides an explanation for the underestimation shown in Figure 1.14. For the concentration ratio, a seasonal variation is observed (quite stable during summer and almost double in the winter months), which can most probably be attributed to road dust re-suspension during winter, particularly in February-April. In contrast to this, the calculated $PM_{2.5}$ over NO_x emission ratio varies only with the traffic and thus the seasonal variations due to climate and other conditions are not reproduced.



Figure 1.14. Year averaged diurnal variation of the $PM_{2.5}$ over NO_x ratios of traffic emissions and delta concentrations in Hornsgatan, Stockholm.



Figure 1.15. Diurnal variation of the $PM_{2.5}$ over NO_x ratios in Hornsgatan, Stockholm a) calculated emissions ratios from COPERT, b) measured ratios.

-Weekends summer - Weekends winter

•Workdays summer •

-Workdays winter



Figure 1.16. Monthly variation of the $PM_{2.5}$ over NO_x ratios of traffic emissions and delta concentrations in Hornsgatan, Stockholm.

1.3.2.2 Alternative runs – Sensitivity analysis

In order to assess the impact of various parameters in the calculated emissions, some older runs performed are presented here. The difference as compared to the basecase is that the HDV share is doubled, all buses run on diesel (instead of ethanol) and the gradient of the road, about 2%, is also taken into account in the calculations. All other parameters of the baseline run remained unchanged.

Similarly to the basecase, two sets of runs were performed with COPERT, for the hourly and monthly distribution of traffic emissions. From the monitored traffic data, average hourly and monthly data were derived for the number of passenger cars, the heavy duty fraction and the average vehicle speed.

The calculated hourly and monthly vehicle emissions of CO, NO_x and $PM_{2.5}$ and the measured DeltaCs of NO_x and $PM_{2.5}$ are presented in Table 1.11 and Table 1.12. From the above emissions and delta concentrations, $PM_{2.5}$ over NO_x and CO over NO_x emission ratios are derived, on an hourly and on a monthly basis and are presented in the same tables.

| | | | Emissio | ns (g) | | Conce | entrations | s (μg/m ³) |
|-------|--------|-----------------|-------------------|------------------------------------|--------------------|-----------------|-------------------|------------------------------------|
| Hour | СО | NO _x | PM _{2.5} | PM _{2.5} /NO _x | CO/NO _x | NO _x | PM _{2.5} | PM _{2.5} /NO _x |
| 01:00 | 457,5 | 131,3 | 3,7 | 0,028 | 3,484 | 77,8 | 3,0 | 0,039 |
| 02:00 | 397,1 | 131,4 | 4,5 | 0,034 | 3,023 | 78,6 | 3,4 | 0,043 |
| 03:00 | 308,4 | 109,5 | 4,0 | 0,037 | 2,816 | 62,4 | 2,9 | 0,046 |
| 04:00 | 271,6 | 98,8 | 3,7 | 0,037 | 2,749 | 63,4 | 2,6 | 0,041 |
| 05:00 | 190,6 | 75,7 | 3,2 | 0,042 | 2,518 | 42,1 | 1,9 | 0,045 |
| 06:00 | 218,9 | 83,8 | 3,4 | 0,041 | 2,614 | 57,6 | 1,7 | 0,030 |
| 07:00 | 642,6 | 204,9 | 7,3 | 0,036 | 3,137 | 141,9 | 3,9 | 0,027 |
| 08:00 | 1217,8 | 352,5 | 13,4 | 0,038 | 3,454 | 208,7 | 6,3 | 0,030 |
| 09:00 | 1338,9 | 387,8 | 15,3 | 0,039 | 3,453 | 215,0 | 7,2 | 0,033 |
| 10:00 | 1189,3 | 360,4 | 14,5 | 0,040 | 3,300 | 209,7 | 6,8 | 0,032 |
| 11:00 | 1335,1 | 396,7 | 15,9 | 0,040 | 3,366 | 195,3 | 7,4 | 0,038 |
| 12:00 | 1532,9 | 433,8 | 17,3 | 0,040 | 3,533 | 208,7 | 7,4 | 0,035 |
| 13:00 | 1714,3 | 465,7 | 18,3 | 0,039 | 3,681 | 223,6 | 8,0 | 0,036 |
| 14:00 | 1755,0 | 476,8 | 18,8 | 0,039 | 3,681 | 223,2 | 8,2 | 0,037 |
| 15:00 | 1837,0 | 492,9 | 19,3 | 0,039 | 3,727 | 225,7 | 8,0 | 0,035 |
| 16:00 | 2016,8 | 560,8 | 21,2 | 0,038 | 3,597 | 232,2 | 8,2 | 0,035 |
| 17:00 | 2062,0 | 522,5 | 19,8 | 0,038 | 3,946 | 224,5 | 7,3 | 0,033 |
| 18:00 | 1818,8 | 452,5 | 15,9 | 0,035 | 4,020 | 196,2 | 6,2 | 0,032 |
| 19:00 | 1494,2 | 374,2 | 12,0 | 0,032 | 3,993 | 167,4 | 5,4 | 0,032 |
| 20:00 | 1181,4 | 306,3 | 9,5 | 0,031 | 3,857 | 150,0 | 4,8 | 0,032 |
| 21:00 | 1025,1 | 256,6 | 7,2 | 0,028 | 3,995 | 131,8 | 4,0 | 0,030 |
| 22:00 | 962,9 | 241,0 | 6,7 | 0,028 | 3,995 | 126,0 | 4,0 | 0,032 |
| 23:00 | 747,6 | 193,2 | 5,4 | 0,028 | 3,869 | 109,1 | 3,6 | 0,033 |
| 24:00 | 612,3 | 163,5 | 4,4 | 0,027 | 3,745 | 95,9 | 3,3 | 0,034 |

Table 1.11. Calculated year averaged hourly traffic emissions versus monitored year averaged hourly average delta concentrations in Hornsgatan, Stockholm.

Table 1.12. Calculated monthly average traffic emissions versus monitored monthly average delta concentrations in Hornsgatan, Stockholm.

| | | | | Concentrations (µg/m ³) | | | | |
|-----------|--------|-----------------|-------------------|-------------------------------------|--------------------|-----------------|-------------------|------------------------------------|
| Month | CO | NO _x | PM _{2.5} | PM _{2.5} /NO _x | CO/NO _x | NO _x | PM _{2.5} | PM _{2.5} /NO _x |
| January | 1079,5 | 292,4 | 10,9 | 0,037 | 3,692 | 168,6 | 4,1 | 0,024 |
| February | 1165,1 | 289,6 | 11,2 | 0,039 | 4,023 | 179,2 | 6,2 | 0,035 |
| March | 1151,9 | 307,3 | 10,7 | 0,035 | 3,749 | 181,6 | 10,8 | 0,059 |
| April | 1096,3 | 292,4 | 10,0 | 0,034 | 3,749 | 180,6 | 6,8 | 0,038 |
| May | 1188,4 | 323,5 | 11,8 | 0,036 | 3,674 | 152,6 | 5,6 | 0,037 |
| June | 1048,0 | 294,4 | 10,9 | 0,037 | 3,559 | 141,7 | 3,5 | 0,025 |
| July | 862,9 | 259,8 | 9,9 | 0,038 | 3,321 | 150,1 | 4,6 | 0,031 |
| August | 1092,5 | 322,8 | 13,0 | 0,040 | 3,385 | 167,5 | 4,7 | 0,028 |
| September | 1147,2 | 313,3 | 11,5 | 0,037 | 3,662 | 194,5 | 5,6 | 0,029 |
| October | 1166,6 | 312,8 | 11,2 | 0,036 | 3,730 | 110,4 | 3,2 | 0,029 |
| November | 1189,4 | 313,7 | 11,3 | 0,036 | 3,791 | 104,4 | 3,7 | 0,035 |
| December | 1082,8 | 285,7 | 10,1 | 0,035 | 3,790 | 132,2 | 3,4 | 0,026 |

Figure 1.17 shows the hourly variation over the day of the $PM_{2.5}$ over NO_x concentration ratio against the respective calculated emission ratio. Overall, there seems to be a fair agreement between the observed and the modelled ratios.

In Figure 1.18, the monthly variation over the year of the concentration ratio between the deltas of $PM_{2.5}$ and NO_x are plotted against the respective calculated emission ratio. A good agreement in the $PM_{2.5}$ over NO_x ratios is observed again, as regards the average value.

Overall, the results indicate that what has been considered in the basecase may either underestimate the HDV fraction or overstate the effect of ethanol buses.



Figure 1.17. Year averaged diurnal variation of the $PM_{2.5}$ over NO_x ratios of traffic emissions and delta concentrations in Hornsgatan, Stockholm.



Figure 1.18. Monthly variation of the $PM_{2.5}$ over NO_x ratios of traffic emissions and delta concentrations in Hornsgatan, Stockholm.

1.3.2.3 Impact of road gradient

As mentioned in the previous section, the street has a gradient of about 2%. In order to investigate the impact of the road gradient on the calculated emissions, the above calculations were repeated without the slope correction. The calculated hourly vehicle emissions of CO, NO_x and $PM_{2.5}$ and the measured delta concentrations of NO_x and $PM_{2.5}$ are presented in Table 1.13. Similarly, Table 1.14 shows the calculated monthly variations in the mean hourly traffic emissions of CO, NO_x and $PM_{2.5}$ and the atmospheric concentration deltas of NO_x and PM_{10} .

Table 1.13. Calculated year averaged hourly traffic emissions without slope versus monitored year averaged hourly delta concentrations in Hornsgatan, Stockholm.

| | | | Emission | ns (g) | | Conce | entrations | s (μg/m ³) |
|-------|--------|-----------------|-------------------|------------------------------------|--------------------|-----------------|-------------------|------------------------------------|
| Hour | СО | NO _x | PM _{2.5} | PM _{2.5} /NO _x | CO/NO _x | NO _x | PM _{2.5} | PM _{2.5} /NO _x |
| 01:00 | 456,9 | 128,3 | 3,5 | 0,027 | 3,561 | 77,8 | 3,0 | 0,039 |
| 02:00 | 396,5 | 127,5 | 4,2 | 0,033 | 3,111 | 78,6 | 3,4 | 0,043 |
| 03:00 | 307,9 | 105,9 | 3,8 | 0,036 | 2,907 | 62,4 | 2,9 | 0,046 |
| 04:00 | 271,1 | 95,5 | 3,5 | 0,036 | 2,840 | 63,4 | 2,6 | 0,041 |
| 05:00 | 190,2 | 72,8 | 3,0 | 0,041 | 2,612 | 42,1 | 1,9 | 0,045 |
| 06:00 | 218,4 | 80,7 | 3,2 | 0,040 | 2,708 | 57,6 | 1,7 | 0,030 |
| 07:00 | 641,4 | 198,6 | 6,9 | 0,035 | 3,229 | 141,9 | 3,9 | 0,027 |
| 08:00 | 1214,8 | 341,4 | 12,5 | 0,037 | 3,559 | 208,7 | 6,3 | 0,030 |
| 09:00 | 1335,3 | 375,1 | 14,2 | 0,038 | 3,560 | 215,0 | 7,2 | 0,033 |
| 10:00 | 1185,9 | 348,1 | 13,6 | 0,039 | 3,407 | 209,7 | 6,8 | 0,032 |
| 11:00 | 1331,4 | 383,4 | 14,8 | 0,039 | 3,473 | 195,3 | 7,4 | 0,038 |
| 12:00 | 1528,5 | 419,5 | 16,1 | 0,038 | 3,644 | 208,7 | 7,4 | 0,035 |
| 13:00 | 1709,6 | 450,7 | 17,0 | 0,038 | 3,793 | 223,6 | 8,0 | 0,036 |
| 14:00 | 1750,2 | 461,4 | 17,4 | 0,038 | 3,793 | 223,2 | 8,2 | 0,037 |
| 15:00 | 1832,0 | 477,2 | 17,9 | 0,037 | 3,839 | 225,7 | 8,0 | 0,035 |
| 16:00 | 2004,6 | 513,3 | 19,3 | 0,038 | 3,905 | 232,2 | 8,2 | 0,035 |
| 17:00 | 2056,8 | 506,6 | 18,3 | 0,036 | 4,060 | 224,5 | 7,3 | 0,033 |
| 18:00 | 1814,8 | 439,8 | 14,8 | 0,034 | 4,126 | 196,2 | 6,2 | 0,032 |
| 19:00 | 1491,6 | 364,7 | 11,2 | 0,031 | 4,089 | 167,4 | 5,4 | 0,032 |
| 20:00 | 1179,5 | 298,8 | 8,9 | 0,030 | 3,948 | 150,0 | 4,8 | 0,032 |
| 21:00 | 1023,8 | 251,2 | 6,7 | 0,027 | 4,076 | 131,8 | 4,0 | 0,030 |
| 22:00 | 961,6 | 235,9 | 6,3 | 0,027 | 4,076 | 126,0 | 4,0 | 0,032 |
| 23:00 | 746,7 | 189,1 | 5,1 | 0,027 | 3,950 | 109,1 | 3,6 | 0,033 |
| 24:00 | 611,6 | 160,0 | 4,2 | 0,026 | 3,821 | 95,9 | 3,3 | 0,034 |

| | | | Emission | | Concentrations (µg/m ³) | | | |
|-----------|--------|-----------------|-------------------|------------------------------------|-------------------------------------|-----------------|-------------------|------------------------------------|
| Month | CO | NO _x | PM _{2.5} | PM _{2.5} /NO _x | CO/NO _x | NO _x | PM _{2.5} | PM _{2.5} /NO _x |
| January | 1051,6 | 283,1 | 10,1 | 0,036 | 3,715 | 168,6 | 4,1 | 0,024 |
| February | 1142,2 | 307,7 | 11,5 | 0,037 | 3,712 | 179,2 | 6,2 | 0,035 |
| March | 1121,9 | 298,1 | 10,0 | 0,034 | 3,763 | 181,6 | 10,8 | 0,059 |
| April | 1067,6 | 283,9 | 9,4 | 0,033 | 3,761 | 180,6 | 6,8 | 0,038 |
| May | 1157,5 | 313,4 | 11,0 | 0,035 | 3,694 | 152,6 | 5,6 | 0,037 |
| June | 1020,4 | 285,1 | 10,1 | 0,036 | 3,579 | 141,7 | 3,5 | 0,025 |
| July | 839,7 | 251,2 | 9,2 | 0,037 | 3,342 | 150,1 | 4,6 | 0,031 |
| August | 1063,8 | 311,5 | 12,1 | 0,039 | 3,415 | 167,5 | 4,7 | 0,028 |
| September | 1117,4 | 303,4 | 10,7 | 0,035 | 3,683 | 194,5 | 5,6 | 0,029 |
| October | 1136,3 | 303,2 | 10,5 | 0,035 | 3,748 | 110,4 | 3,2 | 0,029 |
| November | 1158,7 | 304,2 | 10,5 | 0,035 | 3,810 | 104,4 | 3,7 | 0,035 |
| December | 1054,8 | 277,1 | 9,4 | 0,034 | 3,806 | 132,2 | 3,4 | 0,026 |

Table 1.14. Calculated monthly average traffic emissions without slope versus monitored monthly average delta concentrations in Hornsgatan, Stockholm.

1.3.2.4 Impact of the "Artemis Reduction Factors"

In COPERT, hot emissions estimates for post-Euro I vehicles are calculated on the basis of reductions brought in the emission factors of Euro I vehicles due to the lack of experimental data. In the framework of the DG TrEn project Artemis, it was found that emissions of Euro II heavy-duty vehicles are underestimated by existing emission factor databases, a fact that affects especially NO_x emission levels. Consequently, NO_x emissions calculated with COPERT are expected to be underestimated. In order to investigate the impact of these findings, additional calculations were performed, which are presented in Table 1.15 and Table 1.16.

| Table 1.15 | 5. Calculat | ted year | averaged | hourly | traffic | emissions | with "A | Artemis |
|--------------|-------------|------------|-----------|--------|---------|-----------|---------|---------|
| Reduction | Factors" | versus | monitored | year | average | d hourly | average | e delta |
| concentratio | ons in Horn | isgatan, S | tockholm. | | | | | |

| | | | Emission | ns (g) | | Concentrations (µg/m ³) | | | |
|-------|--------|-----------------|-------------------|------------------------------------|--------------------|-------------------------------------|-------------------|------------------------------------|--|
| Hour | СО | NO _x | PM _{2.5} | PM _{2.5} /NO _x | CO/NO _x | NO _x | PM _{2.5} | PM _{2.5} /NO _x | |
| 01:00 | 457,5 | 132,7 | 3,6 | 0,027 | 3,448 | 77,8 | 3,0 | 0,039 | |
| 02:00 | 399,1 | 141,0 | 4,6 | 0,032 | 2,831 | 78,6 | 3,4 | 0,043 | |
| 03:00 | 308,4 | 111,1 | 3,9 | 0,035 | 2,775 | 62,4 | 2,9 | 0,046 | |
| 04:00 | 271,6 | 100,3 | 3,6 | 0,036 | 2,708 | 63,4 | 2,6 | 0,041 | |
| 05:00 | 190,6 | 77,0 | 3,1 | 0,040 | 2,475 | 42,1 | 1,9 | 0,045 | |
| 06:00 | 218,9 | 85,2 | 3,3 | 0,039 | 2,571 | 57,6 | 1,7 | 0,030 | |
| 07:00 | 642,6 | 207,7 | 7,1 | 0,034 | 3,093 | 141,9 | 3,9 | 0,027 | |
| 08:00 | 1217,8 | 357,8 | 13,0 | 0,036 | 3,403 | 208,7 | 6,3 | 0,030 | |
| 09:00 | 1338,9 | 393,9 | 14,8 | 0,038 | 3,399 | 215,0 | 7,2 | 0,033 | |
| 10:00 | 1189,3 | 366,2 | 14,1 | 0,039 | 3,248 | 209,7 | 6,8 | 0,032 | |
| 11:00 | 1335,1 | 403,0 | 15,5 | 0,038 | 3,313 | 195,3 | 7,4 | 0,038 | |
| 12:00 | 1532,9 | 440,7 | 16,9 | 0,038 | 3,478 | 208,7 | 7,4 | 0,035 | |
| 13:00 | 1714,3 | 472,9 | 17,8 | 0,038 | 3,625 | 223,6 | 8,0 | 0,036 | |
| 14:00 | 1755,0 | 484,1 | 18,2 | 0,038 | 3,625 | 223,2 | 8,2 | 0,037 | |
| 15:00 | 1837,0 | 500,4 | 18,7 | 0,037 | 3,671 | 225,7 | 8,0 | 0,035 | |
| 16:00 | 2016,8 | 569,7 | 20,6 | 0,036 | 3,540 | 232,2 | 8,2 | 0,035 | |
| 17:00 | 2062,0 | 530,1 | 19,2 | 0,036 | 3,890 | 224,5 | 7,3 | 0,033 | |
| 18:00 | 1818,8 | 458,5 | 15,5 | 0,034 | 3,967 | 196,2 | 6,2 | 0,032 | |
| 19:00 | 1494,2 | 378,7 | 11,7 | 0,031 | 3,946 | 167,4 | 5,4 | 0,032 | |
| 20:00 | 1181,4 | 309,9 | 9,3 | 0,030 | 3,812 | 150,0 | 4,8 | 0,032 | |
| 21:00 | 1025,1 | 259,2 | 7,0 | 0,027 | 3,955 | 131,8 | 4,0 | 0,030 | |
| 22:00 | 962,9 | 243,4 | 6,6 | 0,027 | 3,955 | 126,0 | 4,0 | 0,032 | |
| 23:00 | 747,6 | 195,2 | 5,3 | 0,027 | 3,831 | 109,1 | 3,6 | 0,033 | |
| 24:00 | 612,3 | 165,1 | 4,3 | 0,026 | 3,709 | 95,9 | 3,3 | 0,034 | |

Table 1.16. Calculated monthly average traffic emissions "Artemis Reduction Factors" versus monitored monthly average delta concentrations in Hornsgatan, Stockholm.

| | | | Emission | | Concentrations (µg/m ³) | | | |
|-----------|--------|-----------------|-------------------|------------------------------------|-------------------------------------|-----------------|-------------------|------------------------------------|
| Month | СО | NO _x | PM _{2.5} | PM _{2.5} /NO _x | CO/NO _x | NO _x | PM _{2.5} | PM _{2.5} /NO _x |
| January | 1079,5 | 296,6 | 10,6 | 0,036 | 3,639 | 168,6 | 4,1 | 0,024 |
| February | 1172,3 | 323,1 | 12,1 | 0,037 | 3,628 | 179,2 | 6,2 | 0,035 |
| March | 1151,9 | 311,4 | 10,5 | 0,034 | 3,699 | 181,6 | 10,8 | 0,059 |
| April | 1096,3 | 296,2 | 9,7 | 0,033 | 3,701 | 180,6 | 6,8 | 0,038 |
| May | 1188,4 | 328,1 | 11,5 | 0,035 | 3,622 | 152,6 | 5,6 | 0,037 |
| June | 1048,0 | 298,7 | 10,6 | 0,035 | 3,508 | 141,7 | 3,5 | 0,025 |
| July | 862,9 | 263,7 | 9,6 | 0,036 | 3,273 | 150,1 | 4,6 | 0,031 |
| August | 1092,5 | 328,0 | 12,6 | 0,038 | 3,331 | 167,5 | 4,7 | 0,028 |
| September | 1147,2 | 317,7 | 11,2 | 0,035 | 3,611 | 194,5 | 5,6 | 0,029 |
| October | 1166,6 | 317,1 | 10,9 | 0,035 | 3,679 | 110,4 | 3,2 | 0,029 |
| November | 1189,4 | 318,1 | 11,0 | 0,035 | 3,739 | 104,4 | 3,7 | 0,035 |
| December | 1082,8 | 289,6 | 9,8 | 0,034 | 3,739 | 132,2 | 3,4 | 0,026 |

1.3.2.5 Results – Discussion

In Figure 1.19, the results of the above sensitivity analysis are summarised. The hourly variation over the day of the $PM_{2.5}$ over NO_x concentration ratio against the respective calculated emission ratio is plotted for all variants described above.

As expected, NO_x and $PM_{2.5}$ emissions are lower in the case of road without gradient (see also Table 1.13 and Table 1.14). The resulting $PM_{2.5}$ over NO_x ratio is then somewhat lower, as well as when taking the "Artemis Corrections" into account. The latter is the combined result of the higher NO_x emissions and the lower $PM_{2.5}$ emissions.

In both cases the differentiations from the case "with road gradient" are relatively low, mainly because the higher GVW classes of the HDV were excluded from the calculations as explained in 1.0, but also because of the relatively low share of Euro II vehicles in the year 2000.

The exact share of HDVs in the fleet seems to be very significant in assessing the traffic contribution to pollutant concentrations in the atmosphere. This is also indicated by the much higher $PM_{2.5}$ over NO_x ratio when the results of the various scenarios with the increased (double) share of HDVs are compared with those of the basecase.



Figure 1.19. Year averaged diurnal variation of the $PM_{2.5}$ over NO_x ratios of traffic emissions for various scenarios and delta concentrations in Hornsgatan, Stockholm.

1.3.3 Marylebone Rd., London

Using the composition of the British vehicle fleet for the year 2000 extracted from the TRENDS database, the share of each vehicle category is derived. The detailed monthly (Table B1) and hourly (Tables B.2 & B.3) distribution of traffic into the various vehicle categories is presented in Annex B.

The traffic station is located close to the centre of London and thus, as in the case of Stockholm, it is assumed that only HDV with a GVW lower than 16 tonnes were allowed, i.e. no HDV with a GVW of 16-32 tonnes and over 32 tonnes were considered. The street has six traffic lanes in total, with different vehicle volumes. From the traffic data monitored, average hourly and monthly data were derived for the number of passenger cars, the number of heavy duty vehicles and the average vehicle speed. Two sets of runs were performed with COPERT, for the hourly and monthly distribution of traffic emissions.

The calculated hourly vehicle emissions and the measured delta concentrations of CO, NO_x and $PM_{2.5}$ are presented in Table 1.17. From the above emissions and delta concentrations, $PM_{2.5}$ over NO_x and CO over NO_x ratios are derived, on an hourly basis and are also presented in the same table.

In the same manner, Table 1.18 shows the calculated monthly variations and the corresponding ratios in traffic emissions and the atmospheric concentration deltas of CO, NO_x and $PM_{2.5}$.

Table 1.17. Calculated year averaged hourly traffic emissions versus monitored year averaged hourly delta concentrations in Marylebone Rd., London.

| | | | Emissio | ns (g) | | Concentrations ($\mu g/m^3$) | | | | | |
|-------|---------|-----------------|-------------------|------------------------------------|--------------------|--------------------------------|-----------------|-------------------|------------------------------------|--------------------|--|
| Hour | СО | NO _x | PM _{2.5} | PM _{2.5} /NO _x | CO/NO _x | СО | NO _x | PM _{2.5} | PM _{2.5} /NO _x | CO/NO _x | |
| 01:00 | 9035,4 | 2483,8 | 77,3 | 0,031 | 3,638 | 1214,0 | 224,7 | 7,6 | 0,034 | 5,402 | |
| 02:00 | 6360,7 | 1911,9 | 59,3 | 0,031 | 3,327 | 892,7 | 178,9 | 5,7 | 0,032 | 4,990 | |
| 03:00 | 4958,2 | 1603,1 | 53,5 | 0,033 | 3,093 | 729,4 | 157,6 | 5,1 | 0,032 | 4,628 | |
| 04:00 | 4329,6 | 1506,2 | 55,0 | 0,036 | 2,874 | 629,5 | 150,6 | 5,5 | 0,036 | 4,179 | |
| 05:00 | 4233,2 | 1622,8 | 65,7 | 0,040 | 2,609 | 577,3 | 155,0 | 5,2 | 0,034 | 3,725 | |
| 06:00 | 6097,3 | 2473,3 | 109,2 | 0,044 | 2,465 | 715,5 | 208,3 | 7,7 | 0,037 | 3,435 | |
| 07:00 | 11376,8 | 4270,1 | 197,2 | 0,046 | 2,664 | 1207,4 | 297,2 | 11,6 | 0,039 | 4,062 | |
| 08:00 | 14064,6 | 5271,4 | 243,2 | 0,046 | 2,668 | 1684,3 | 358,7 | 15,8 | 0,044 | 4,696 | |
| 09:00 | 17901,3 | 5713,9 | 285,2 | 0,050 | 3,133 | 1785,6 | 364,6 | 18,2 | 0,050 | 4,898 | |
| 10:00 | 17944,3 | 5757,5 | 286,9 | 0,050 | 3,117 | 1467,8 | 334,9 | 15,1 | 0,045 | 4,383 | |
| 11:00 | 19012,9 | 6051,0 | 306,8 | 0,051 | 3,142 | 1416,8 | 340,7 | 14,5 | 0,042 | 4,158 | |
| 12:00 | 20298,4 | 6224,9 | 319,3 | 0,051 | 3,261 | 1601,9 | 378,7 | 16,4 | 0,043 | 4,230 | |
| 13:00 | 21434,8 | 6276,2 | 320,7 | 0,051 | 3,415 | 1750,0 | 394,4 | 16,9 | 0,043 | 4,437 | |
| 14:00 | 21910,1 | 6168,1 | 309,9 | 0,050 | 3,552 | 1836,4 | 386,7 | 14,9 | 0,039 | 4,749 | |
| 15:00 | 21885,5 | 5943,4 | 291,2 | 0,049 | 3,682 | 1868,9 | 384,4 | 15,9 | 0,041 | 4,862 | |
| 16:00 | 22191,3 | 5722,5 | 272,3 | 0,048 | 3,878 | 2130,5 | 386,9 | 13,8 | 0,036 | 5,507 | |
| 17:00 | 22857,4 | 5458,1 | 248,3 | 0,045 | 4,188 | 2482,9 | 385,0 | 12,9 | 0,033 | 6,450 | |
| 18:00 | 23611,9 | 5261,7 | 228,2 | 0,043 | 4,487 | 2731,9 | 364,5 | 12,3 | 0,034 | 7,495 | |
| 19:00 | 22370,3 | 4930,6 | 196,0 | 0,040 | 4,537 | 2592,3 | 329,9 | 10,8 | 0,033 | 7,859 | |
| 20:00 | 19768,0 | 4462,1 | 171,0 | 0,038 | 4,430 | 2410,4 | 315,7 | 10,2 | 0,032 | 7,635 | |
| 21:00 | 16857,6 | 3959,4 | 149,7 | 0,038 | 4,258 | 2291,6 | 323,2 | 10,6 | 0,033 | 7,091 | |
| 22:00 | 14809,7 | 3584,5 | 129,4 | 0,036 | 4,132 | 2027,7 | 297,6 | 10,4 | 0,035 | 6,814 | |
| 23:00 | 14803,0 | 3582,8 | 129,3 | 0,036 | 4,132 | 1838,6 | 276,5 | 9,8 | 0,036 | 6,649 | |
| 24:00 | 12755,5 | 3188,9 | 107,4 | 0,034 | 4,000 | 1703,8 | 271,5 | 9,4 | 0,035 | 6,275 | |

| | | | Emi | ssions (g) | | | (| Concentr | ations (µg/m | 1 ³) |
|-----------|---------|-----------------|-------------------|------------------------------------|--------------------|--------|-----------------|-------------------|------------------------------------|--------------------|
| Month | СО | NO _x | PM _{2.5} | PM _{2.5} /NO _x | CO/NO _x | СО | NO _x | PM _{2.5} | PM _{2.5} /NO _x | CO/NO _x |
| January | 13728,4 | 3963,3 | 168,5 | 0,043 | 3,464 | 1651,0 | 276,7 | 8,1 | 0,029 | 5,967 |
| February | 15382,2 | 4391,8 | 194,3 | 0,044 | 3,502 | 2687,3 | 413,4 | 15,5 | 0,038 | 6,500 |
| March | 14615,2 | 4325,6 | 187,8 | 0,043 | 3,379 | 1468,1 | 212,9 | 9,6 | 0,045 | 6,897 |
| April | 14164,5 | 4060,1 | 172,1 | 0,042 | 3,489 | 1553,6 | 229,5 | 9,0 | 0,039 | 6,771 |
| May | 15014,6 | 4351,4 | 191,1 | 0,044 | 3,451 | 1299,1 | 232,3 | 7,6 | 0,033 | 5,593 |
| June | 14596,5 | 4316,1 | 188,3 | 0,044 | 3,382 | 1710,6 | 321,4 | 12,5 | 0,039 | 5,323 |
| July | 15038,2 | 4351,0 | 189,8 | 0,044 | 3,456 | 1267,9 | 207,7 | 10,7 | 0,052 | 6,104 |
| August | 14324,0 | 4232,0 | 182,3 | 0,043 | 3,385 | 1544,7 | 300,6 | 12,2 | 0,041 | 5,139 |
| September | 14028,7 | 4195,5 | 182,7 | 0,044 | 3,344 | 1653,4 | 338,1 | 13,7 | 0,041 | 4,890 |
| October | 14008,3 | 4131,6 | 183,1 | 0,044 | 3,391 | 1383,0 | 388,0 | 14,4 | 0,037 | 3,564 |
| November | 15081,8 | 4440,5 | 200,1 | 0,045 | 3,396 | 2267,2 | 440,4 | 16,1 | 0,037 | 5,148 |
| December | 13771,6 | 3942,5 | 167,1 | 0,042 | 3,493 | 1531,1 | 300,6 | 11,0 | 0,037 | 5,094 |

Table 1.18. Calculated monthly average traffic emissions versus monitored monthly average delta concentrations in Marylebone Rd., London.

In Figure 1.20, the hourly variation over the day of the concentration ratio between the deltas of $PM_{2.5}$ and NO_x is plotted against the respective calculated emission ratio. There is a fair agreement between the observed and the modelled ratios as regards the general trend, although the calculated ratio is somewhat higher. This may explained by the fact that NO_x emissions factors for post Euro I HDV in COPERT are underestimated and thus the calculated NO_x emissions are slightly underestimated too (see also sensitivity analysis for Hornsgatan, Stockholm).



Figure 1.20. Year averaged diurnal variation of the $PM_{2.5}$ over NO_x ratios of traffic emissions and delta concentrations in Marylebone Rd., London.

In Figure 1.21, the monthly variations of the above ratios are plotted. For the concentration ratio a variation over the year is observed, which seems to have a seasonal character, which, contrary to Hornsgatan, shows higher $PM_{2.5}$ in summer. In contrast, the calculated ratio is found quite stable, since during the day it varies only with traffic volume and average speed and thus the seasonal variation could not be reproduced.



Figure 1.21. Monthly variation of the $PM_{2.5}$ over NO_x ratios of traffic emissions and delta concentrations in Marylebone Rd., London.

1.3.4 Frankfurter Allee, Berlin

Using the composition of the German vehicle fleet for the year 2002 extracted from the TRENDS database, the share of each vehicle category is derived. The detailed monthly (Table C.1) and hourly (Tables C.2 & C.3) distribution of traffic into the various vehicle categories is presented in Annex C.

The traffic station is located in the Frankfurter Allee, a busy main road consisting of 6 lanes in Berlin and thus, as in the case of Stockholm, it is assumed that only HDV with a GVW lower than 16 tonnes were allowed. The road traffic is divided into westbound and eastbound traffic having different vehicle volumes and recorded by automatic detection devices. From the traffic data monitored, average hourly and monthly data were derived for the total number of vehicles and the average vehicle speed. Due to lack of data regarding the variation of the heavy duty fraction, an average value of 4.8% was considered. Four sets of runs were performed with COPERT, for the hourly and monthly distribution of traffic emissions and for both westbound and eastbound traffic.

The calculated hourly vehicle emissions and the measured delta concentrations of CO, NO_x and PM are presented in Table 1.19. As for the specific traffic station no $PM_{2.5}$ concentration was measured, only PM_{10} data are presented below. From the above emissions and delta concentrations, PM_{10} and $PM_{2.5}$ over NO_x and CO over NO_x ratios are derived, on an hourly basis and are presented in the same table.

In addition, Table 1.20 shows the calculated monthly variations and the corresponding ratios in traffic emissions of CO, NO_x and PM.

| | | Emissio | ns (g) | Concentrations (µg/m ³) | | | | | | |
|-------|---------|---------|-------------------|-------------------------------------|--------------------|-------|-----------------|-------------------------|-----------------------------------|--------------------|
| Hour | СО | NOx | PM _{2.5} | PM _{2.5} /NO _x | CO/NO _x | СО | NO _x | PM ₁₀ | PM ₁₀ /NO _x | CO/NO _x |
| 01:00 | 3426,7 | 698,8 | 33,7 | 0,048 | 4,903 | 183,1 | 19,1 | 8,8 | 0,459 | 9,604 |
| 02:00 | 2354,5 | 491,2 | 23,3 | 0,047 | 4,794 | 152,9 | 16,4 | 5,0 | 0,306 | 9,307 |
| 03:00 | 1661,8 | 348,9 | 16,5 | 0,047 | 4,762 | 131,6 | 14,6 | 3,4 | 0,234 | 9,035 |
| 04:00 | 1252,7 | 261,7 | 12,4 | 0,047 | 4,787 | 139,4 | 18,9 | 3,4 | 0,180 | 7,370 |
| 05:00 | 1242,2 | 261,4 | 12,3 | 0,047 | 4,751 | 222,4 | 39,2 | 4,3 | 0,109 | 5,670 |
| 06:00 | 2158,3 | 460,1 | 21,4 | 0,047 | 4,691 | 382,3 | 65,7 | 6,3 | 0,095 | 5,820 |
| 07:00 | 7766,0 | 1528,9 | 75,4 | 0,049 | 5,079 | 473,6 | 80,4 | 9,4 | 0,116 | 5,891 |
| 08:00 | 10394,2 | 1842,1 | 96,7 | 0,053 | 5,643 | 457,0 | 82,9 | 12,4 | 0,149 | 5,511 |
| 09:00 | 11225,0 | 1989,3 | 104,5 | 0,053 | 5,643 | 436,6 | 85,1 | 14,2 | 0,167 | 5,128 |
| 10:00 | 10798,3 | 1936,1 | 101,0 | 0,052 | 5,577 | 458,5 | 86,7 | 15,4 | 0,178 | 5,289 |
| 11:00 | 10621,0 | 1995,5 | 101,4 | 0,051 | 5,322 | 456,2 | 87,6 | 15,2 | 0,174 | 5,206 |
| 12:00 | 11915,8 | 2115,9 | 111,2 | 0,053 | 5,631 | 467,9 | 89,3 | 14,8 | 0,166 | 5,240 |
| 13:00 | 12037,9 | 2144,2 | 112,5 | 0,052 | 5,614 | 488,9 | 87,9 | 16,6 | 0,189 | 5,563 |
| 14:00 | 12157,5 | 2201,6 | 114,3 | 0,052 | 5,522 | 516,3 | 86,2 | 15,1 | 0,175 | 5,988 |
| 15:00 | 11953,2 | 2231,7 | 113,8 | 0,051 | 5,356 | 598,4 | 90,9 | 11,3 | 0,124 | 6,585 |
| 16:00 | 13532,0 | 2482,3 | 127,9 | 0,052 | 5,451 | 670,1 | 93,1 | 13,3 | 0,142 | 7,200 |
| 17:00 | 15090,4 | 2624,5 | 139,6 | 0,053 | 5,750 | 628,5 | 84,1 | 13,6 | 0,161 | 7,476 |
| 18:00 | 15389,2 | 2592,7 | 140,4 | 0,054 | 5,936 | 566,2 | 73,9 | 12,3 | 0,166 | 7,660 |
| 19:00 | 13649,2 | 2386,4 | 126,5 | 0,053 | 5,720 | 513,1 | 62,3 | 11,4 | 0,184 | 8,242 |
| 20:00 | 12717,9 | 2231,0 | 118,1 | 0,053 | 5,701 | 435,1 | 48,4 | 9,3 | 0,192 | 8,986 |
| 21:00 | 10042,0 | 1785,7 | 93,7 | 0,052 | 5,624 | 359,3 | 38,0 | 6,7 | 0,175 | 9,450 |
| 22:00 | 7385,3 | 1427,6 | 71,3 | 0,050 | 5,173 | 332,6 | 33,9 | 6,8 | 0,200 | 9,805 |
| 23:00 | 5468,1 | 1091,4 | 53,4 | 0,049 | 5,010 | 287,5 | 26,0 | 6,3 | 0,241 | 11,073 |
| 24:00 | 4804,5 | 962,8 | 46,9 | 0,049 | 4,990 | 225,8 | 21,5 | 5,2 | 0,240 | 10,490 |

Table 1.19. Calculated year averaged hourly traffic emissions versus monitored year averaged hourly delta concentrations in Frankfurter Allee, Berlin.

Table 1.20. Calculated monthly average traffic emissions versus monitored monthly average delta concentrations in Frankfurter Allee, Berlin.

| | | | Emis | sions (kg) | | | (| Concentr | ations (µg/m | ı °) |
|-----------|--------|-----------------|-------------------|------------------------------------|--------------------|-------|------|-----------|-----------------------------------|--------------------|
| Month | СО | NO _x | PM _{2.5} | PM _{2.5} /NO _x | CO/NO _x | СО | NOx | PM_{10} | PM ₁₀ /NO _x | CO/NO _x |
| January | 6478.9 | 1241.6 | 61.2 | 0.049 | 5.218 | 573.5 | 57.1 | 16.9 | 0.296 | 10.044 |
| February | 5592.6 | 1071.7 | 52.9 | 0.049 | 5.218 | 432.4 | 46.1 | 3.2 | 0.069 | 9.379 |
| March | 5276.2 | 1011.1 | 49.9 | 0.049 | 5.218 | 451.2 | 54.8 | 9.5 | 0.173 | 8.236 |
| April | 5695.1 | 1074.9 | 54.6 | 0.051 | 5.298 | 453.1 | 59.6 | 5.9 | 0.099 | 7.596 |
| May | 6477.4 | 1222.6 | 62.0 | 0.051 | 5.298 | 350.8 | 54.8 | 8.1 | 0.148 | 6.400 |
| June | 5743.3 | 1084.0 | 55.0 | 0.051 | 5.298 | 291.1 | 60.6 | 9.2 | 0.152 | 4.807 |
| July | 5255.7 | 992.0 | 50.3 | 0.051 | 5.298 | 338.4 | 65.7 | 8.3 | 0.126 | 5.154 |
| August | 5446.0 | 1027.9 | 52.2 | 0.051 | 5.298 | 308.9 | 51.2 | 9.7 | 0.190 | 6.039 |
| September | 6524.3 | 1231.4 | 62.5 | 0.051 | 5.298 | 312.1 | 56.3 | 9.9 | 0.175 | 5.544 |
| October | 6702.7 | 1265.1 | 64.2 | 0.051 | 5.298 | 412.2 | 79.5 | 10.5 | 0.133 | 5.184 |
| November | 6754.6 | 1274.9 | 64.7 | 0.051 | 5.298 | 422.8 | 67.5 | 11.8 | 0.175 | 6.266 |
| December | 6345.4 | 1197.7 | 60.8 | 0.051 | 5.298 | 405.6 | 53.8 | 11.4 | 0.212 | 7.537 |

For the reasons explained above, the PM over NO_x ratios are not directly comparable and thus only the CO over NO_x ratios are considered.

In Figure 1.22, the hourly variation over the day of the concentration ratio between the deltas of CO and NO_x is plotted against the respective calculated emission ratio. For the concentration ratio a large variation over the day is observed, which might be attributed to the variation in traffic composition throughout the day, e.g. lower heavy duty fraction in the evening and during the night. This variation, however, could not be reproduced by the emission model as the heavy duty fraction has been kept constant due to lack of more detailed data.

On the other hand, the calculated ratio is quite stable during the day varying with the traffic volume and average speed.

Figure 1.23 presents the monthly variation of the above ratio, where a large discrepancy is observed in January, converging though towards the summer months.



Figure 1.22. Year averaged diurnal variation of the CO over NO_x ratios of traffic emissions and delta concentrations in Frankfurter Allee, Berlin.



Figure 1.23. Monthly variation of the $PM_{2.5}$ over NO_x ratios of traffic emissions and delta concentrations in Frankfurter Allee, Berlin.

1.4 Summary and conclusions

The investigation of suitable station pairs in Europe has been fairly successful and has resulted in a number of well defined and suitable station pairs, for which data on pollutant concentrations and traffic and meteorological parameters have been transferred to a SEC database. So far the collected data include station pairs in Stockholm, London, Berlin, Thessaloniki, Hannover and Oslo and these have also been analysed (except Hannover data where data quality issues are as yet unresolved) according to the procedures defined for SEC subtask 3. Station pairs in Helsinki, Madrid, Milan, Paris and Praha are considered as good candidates for the further work.

The collected data has been used for comparison study of street scale dispersion models (see chapter 3 and 4).

The data analysis (section 1.2) has produced DRs of concentrations (representing the street traffic's own contribution to the street level concentrations), meaning the concentration of pollutants (PM_{10} , $PM_{2.5}$, NO_2) relative to NO_x . These delta ratios have been calculated for workday and weekend conditions separately, for summer and winter conditions. This represents a basis against which ratios from emission factor databases (such as COPERT 3) can be tested.

The results of this analysis allow an estimation of the strength of the road dust resuspension source to PM_{10} and PM_{2.5}, by comparing DRs for winter/summer/workdays/weekends, for PM10 and PM2.5. For Marylebone Rd. in London, it is estimated that the re-suspension source to PM_{10} is of about the same magnitude as the combined exhaust/brake/tyre wear source. In Hornsgatan, where studded tyres are used in winter, the re-suspension source dominates PM₁₀ relative to the exhaust. The re-suspension source is significant even in the summer and it also gives a significant contribution to $PM_{2.5}$ in the street (see Section 1.2.4.3). Also in Frankfurter Allee in Berlin the re-suspension source is very strong and relatively larger than in Marylebone. This analysis shows that this is a promising method of estimating "emission factors" for the re-suspension source and similar analysis should be done for more streets.

COPERT 3 emission factor ratios have been tested (section 1.3) on data from Hornsgatan, Stockholm and Marylebone Rd., London ($PM_{2.5}$ relative to NO_x) and on data from Frankfurter Allee (CO relative to NO_x). The testing has been done for complete annual time series, as well as separate for summer/winter/workday/weekend conditions. The testing has produced reasonably good results: the calculated emission factor ratios compare in general reasonably well with the measured delta ratios. This comparison shows that there is room for a significant re-suspension source to $PM_{2.5}$ in Hornsgatan.

Chapter 2: Global analysis: Validation of road traffic emission inventories by means of concentration data measured at several air quality monitoring stations

2.1 Introduction

Despite reductions in emissions, road transport is still one of the main causes of exceedances of air quality limit levels, particularly in urban areas. Anthropogenic emissions of carbon monoxide (CO) and nitrogen oxides (NO_x) are precursors for photo oxidant formation, while substantial health risk could be associated with high particulate matter (PM) concentrations in ambient air (Künzli et al., 2000).

Air quality models require emission data of individual compounds, which are calculated by complex emission models and which, in turn, are based on appropriately chosen emission factors. The assessment of road-traffic-related emission factors of pollutants are normally based on exhaust gas measurements of single vehicles on chassis dynamometers using various driving cycles. While dynamometer tests are essential to establish uniform emission standards for regulatory purposes and for testing of new technologies, they do not necessarily reflect the real on-road driving conditions and the level of maintenance of the actual vehicle fleet. Thus, there is a need for on-road emission estimates of air pollutants from the actual vehicle fleet. To this aim the most common approaches are (a) road-tunnel studies, (b) car chasing experiments to better simulate the atmospheric dilution conditions and (c) atmospheric studies at air quality monitoring sites.

As regards the atmospheric studies to evaluate real-world emission factors, the method of 'inverse modelling' of atmospheric pollution dispersion models is usually used (Palmgren et al., 1999; Ketzel et al., 2003). Another technique used is the determination of the emission ratios from the concentration ratios measured at a receptor site during extensive campaigns (Klemp et al., 2002; Mannschreck et al., 2002).

While all the above methods require also special measuring campaigns focusing on local emissions (Kühlwein et al., 2002a and 2002b), this paper presents a more global approach, making use of already available measurements stored in a common database. To this aim, comparisons between experimentally determined and modelled CO/NO_x , NO_x/PM and PM/CO emission ratios are performed. It aims at adding to the current knowledge on the use of air quality data for the validation of urban emission inventories by using atmospheric concentration data from several monitoring stations.

2.2 Methodology

2.2.1 Determination of emission ratios using atmospheric concentration measurements

It is known that the large-scale background concentration constitutes an appreciable fraction of the pollutant concentrations in busy streets. In order to estimate the contribution of road traffic to the concentrations, a straightforward and reliable procedure is subtracting the concentrations measured at a background station from concentrations at a nearby traffic station. Hence, the measured concentration of pollutant results from the background concentration plus the traffic contribution, which will be diluted during transport. Under constant background conditions the measured variability of pollutant concentration is due to variations in source strength and dilution.

In those situations where the traffic contribution is much larger than the urban background concentration, the ratios of the concentrations may be assumed to reflect the ratios of the local traffic emissions. Therefore, those days are selected for which the difference between the maximum and the minimum concentration is larger by a factor of ten than the minimum concentration for at least one pollutant. Ratios are then calculated for all individual hours on those days and averaged. In fact, the 50 percentile of the distribution of results is calculated in order to reduce the influence of large fluctuations.

For the present analysis, air quality data for CO, NO_x and PM_{10} at traffic stations in five European countries have been analysed. Urban traffic stations with hourly data for the year 2000 were selected from AirBase, the air quality information system of the European Environment Agency. AirBase contains air quality data for a selection of stations and a number of components and meta information on air quality monitoring networks and stations. The information is collected by the European Topic Centre on Air Quality and is stored and made widely available by means of AirBase, accessible on the Internet (http://air-climate.eionet.eu.int/databases/airbase.html).

The selected stations included 10 German, 13 Spanish, 2 Finnish, 2 Portuguese and 5 British traffic stations. As mentioned above, an appropriate factor of ten was selected in order to distinguish those days with the largest traffic contribution. Emission ratios were then derived for all individual hours on those days, median values were calculated for each hour and averaged over the day for each station. Furthermore, weighted averages were also calculated following the same procedure, but only for those hours of the day with the highest CO concentrations, which is a further indication that traffic contribution is the most significant. The results are summarised in Table 2.1 and Table 2.2, where also the stations with the maximum or minimum ratios are shown for each procedure. As an indication of the consistency of the resulting ratios, the products of the three ratios – ideally equal to unit – may be used. These products have been calculated for all stations and average values over the stations for each country are also presented in the same Tables (under column "Check"). From the resulting values when a simple average (Table 2.1) and a weighted average (Table 2.2) are calculated, it is evident that the average product of the emission ratios in the latter case is closer to unity and thus they will be used for any comparisons in the following sections.

| hourly data pair s | eries. | | | | | | | | | |
|--------------------|--------------------|------|-------|---------------------|------|-------|-------|-------|-------|-------|
| | CO/NO _x | | | NO _x /PM | | | PM/CO | | | Check |
| | avg | min | max | avg | min | max | avg | min | max | |
| Germany | 6.48 | 3.85 | 9.82 | 4.85 | 3.44 | 6.88 | 0.044 | 0.023 | 0.072 | 1.217 |
| Spain | 10.54 | 5.45 | 16.92 | 3.60 | 1.63 | 6.12 | 0.035 | 0.021 | 0.058 | 1.147 |
| Finland | 8.46 | 6.73 | 10.20 | 3.72 | 2.76 | 4.69 | 0.040 | 0.039 | 0.042 | 1.200 |
| Portugal | 6.41 | 6.27 | 6.54 | 2.32 | 2.24 | 2.40 | 0.066 | 0.063 | 0.068 | 0.976 |
| United Kingdom | 4.74 | 1.69 | 8.76 | 10.08 | 5.03 | 12.66 | 0.031 | 0.020 | 0.054 | 1.178 |

Table 2.1. Summarised results of data analysis from traffic stations in the selected countries. Averages (avg), maxima (max) and minima (min) of emission ratios for all hourly data pair series.

Table 2.2. Summarised results of data analysis from traffic stations in the selected countries. Weighted averages (wavg), maxima (max) and minima (min) of emission ratios for selected hourly data pair series.

| | CO/NO _x | | | NO _x /PM | | | PM/CO | | | Check |
|----------------|--------------------|------|-------|---------------------|------|-------|-------|-------|-------|-------|
| | wavg | min | max | wavg | min | max | wavg | min | max | |
| Germany | 6.25 | 4.09 | 8.81 | 5.42 | 3.76 | 7.71 | 0.036 | 0.020 | 0.048 | 1.103 |
| Spain | 9.42 | 5.44 | 12.82 | 4.18 | 2.13 | 6.46 | 0.031 | 0.018 | 0.044 | 1.078 |
| Finland | 6.36 | 5.15 | 7.57 | 4.52 | 3.25 | 5.79 | 0.038 | 0.034 | 0.041 | 1.012 |
| Portugal | 6.97 | 6.78 | 7.17 | 2.49 | 2.37 | 2.61 | 0.057 | 0.053 | 0.060 | 0.984 |
| United Kingdom | 4.67 | 1.93 | 8.61 | 10.99 | 6.21 | 13.46 | 0.026 | 0.017 | 0.045 | 1.083 |

2.2.2 Modelled emission data

The calculations presented here have been conducted with the use of the TRENDS (TRansport and ENvironment Database System) model, which is the successor of the FOREMOVE model (FORecast of Emission from MOtor VEhicles), both developed under contract for the Commission of the European Communities (European Commission, 2003; Samaras et al., 1993). TRENDS is a system for calculating a range of environmental pressures due to transport. These environmental pressures include air emissions from the four main transport modes, i.e. road, rail, ships and air.

For the estimation of air pollutant emissions from road transport in urban environments a calculation module was derived following a top down approach. Focus of the calculation was the annual air emissions of CO, NO_x and PM for each of the investigated countries for the year 2000. For air emissions the COPERT 3 calculation module was applied (Ntziachristos and Samaras, 2000). After annual air emissions were estimated on a country basis, a spatial disaggregation module allocated the above annual air emissions to the urban areas of the countries, using the initial COPERT estimates for urban, rural and highway split of the emissions for the different vehicle categories.

The methodological approach used for the calculation of the emissions is briefly described below. Firstly, the appropriate databases for the calculation modules were created. All available databases were used in order to construct the appropriate input for the calculations. In this respect, data concerning vehicle stocks, vehicle new registrations, vehicle usage indicators (such as tonne-kilometres, passenger-kilometres etc.), fuel consumption, technology splits of vehicle fleets for certain years, annual mileage for different vehicle categories, vehicle representative speeds, split of the annual mileage to different road classes, etc were used. Secondly, a System Dynamics Module was established in order to (a) extrapolate the main vehicle categories into the future using data of the past and resulting thus in producing estimates of vehicle stocks per country; (b) simulate the vehicle turnover for the main vehicle categories; and (c) supplement the above with corresponding data on emissions technology parameters which were introduced via a number of suitable implementation tables per country, including simultaneous introduction of different legislation, scrappage schemes, etc. At a final step, the data resulting from the aforementioned processes were adapted in such a way as to produce the input tables for the calculation of annual air emissions required by the methodology of COPERT. These input tables were produced for the year 2000.

2.3 Results and discussion

In Table 2.3, the emission ratios calculated with TRENDS are compared with those obtained from concentration measurements. Figure 2.1 to Figure 2.3 show a graphical representation of the above results for the three ratios investigated. Based on the findings in paragraph 2.2.1 only the weighted average values are used for comparisons with the modelled emission ratios.

Table 2.3. Comparison between emission ratios calculated with TRENDS and concentration ratios resulting from the data analysis from traffic stations in the selected countries.

| | CO/NO _v | | | NO _v /PM | | | PM/CO | | |
|----------------|--------------------|------|--------|---------------------|-------|--------|-------|-------|--------|
| | avg | wavg | TRENDS | avg | wavg | TRENDS | avg | wavg | TRENDS |
| Germanv | 6.48 | 6.25 | 7.16 | 4.85 | 5.42 | 13.12 | 0.044 | 0.036 | 0.011 |
| Spain | 10.54 | 9.42 | 5.25 | 3.60 | 4.18 | 11.60 | 0.035 | 0.031 | 0.016 |
| Finland | 8.46 | 6.36 | 6.80 | 3.72 | 4.52 | 13.90 | 0.040 | 0.038 | 0.011 |
| Portugal | 6.41 | 6.97 | 3.90 | 2.32 | 2.49 | 14.72 | 0.066 | 0.057 | 0.017 |
| United Kingdom | 4.74 | 4.67 | 8.96 | 10.08 | 10.99 | 17.72 | 0.031 | 0.026 | 0.006 |



Figure 2.1. Comparison between measured and modelled CO over NO_x ratios for the selected countries. Weighted average (AQ average), maxima (AQ max) and minima (AQ min) versus values calculated with TRENDS.



Figure 2.2. Comparison between measured and modelled NO_x over PM ratios for the selected countries. Weighted average (AQ average), maxima (AQ max) and minima (AQ min) versus values calculated with TRENDS.



Figure 2.3. Comparison between measured and modelled PM over CO ratios for the selected countries. Weighted average (AQ average), maxima (AQ max) and minima (AQ min) versus values calculated with TRENDS.

Modelled CO/NO_x emission ratios are generally within (or very close to) the range defined by measured air quality ratios. A tendency towards the maximum concentration values may be observed for the northern countries (Germany, Finland and the UK), while this tendency is towards the minimum values for the southern countries (Spain and Portugal). The above do not give a clear indication of whether the modelled CO and/or NO_x emissions are under- or overestimated. Hausberger et al. (2003) suggest that emissions of modern heavy-duty vehicles are underestimated by existing emission factor databases, which affects especially the NO_x emission levels. Consequently, NO_x emission levels of this vehicle category did not decrease since the introduction of EURO 1 limits in real world driving conditions and thus NO_x emissions are expected to be underestimated in TRENDS. This underestimation may explain the slightly higher calculated emission ratios as compared to the average concentration ratios measured for the northern countries mentioned above.

 NO_x/PM emission ratios calculated with TRENDS are clearly overestimated, being up to six times higher than the weighted average concentration ratios. Since NO_x emissions are most probably underestimated by TRENDS – as mentioned above – this indicates that PM emissions are also underestimated and that this underestimation should be even higher. With regard to the modelled PM emissions it has to be noted that TRENDS covers solely tailpipe diesel PM, i.e. emissions from gasoline-fuelled vehicles and non-tailpipe emissions (such as from brakes, tire wear, road wear and resuspension of road dust) are not taken into account. While PM emissions from gasoline-fuelled vehicles are at least two orders of magnitude lower than diesel PM emissions, several studies indicate that non-tailpipe emissions constitute a significant fraction of the total road traffic PM emissions. It is also known that practically all PM emitted by TRENDS can be considered as $PM_{2.5}$ emissions. Taking the above into

account it may be concluded that modelled PM emissions are significantly underestimated.

As a result of the underestimation in the PM emissions calculated by TRENDS the PM/CO emission ratios are underestimated as well since there is no indication of any under- or overestimation of the CO emissions. The respective ratio is well below the observed concentration ratio, being underestimated by a factor of two to four. A recent study showed that, although a valid European-wide $PM_{2.5}$ to PM_{10} ratio can not be proposed, site-specific ratios can be obtained, ranging between 0.57 and 0.85 (Van Dingenen et al., 2004).

Apart from the reasons mentioned above, there might be other reasons possibly contributing to the observed discrepancies. Measuring errors as well as unusual meteorological and traffic conditions may result in 'outliers' in the calculated concentration ratios. Meteorological parameters, mainly wind speed and direction, may influence the measured concentrations of pollutants in the atmosphere, particularly as regards the re-suspension and dispersion processes. Whereas the variation in NO_x concentrations is generally limited and is mostly guided by the parallel variations in meteorological conditions, PM varies more, as a result of resuspension of road dust, especially during the winter months. Special traffic conditions, such as the exclusion of certain vehicles, may lead to ambient air concentrations not representative of the contribution of the entire vehicle fleet. However, other sources of emissions apart from road traffic may add to the emissions concentration in the atmosphere.

On the other side, traffic emissions calculated with TRENDS are a complex function of a large number of parameters, as already mentioned in paragraph 0. As a result, many uncertainties related to the correct estimation of these parameters are introduced in the model. Older technology vehicles, enhanced cold start effects and – probably more important – poorer than expected vehicle maintenance could explain – to a certain extent – the variations.

In view of the above, an assessment of the emission inventories compiled with TRENDS is presented in the following section, in an attempt to make best use of the available data obtained from air quality measurements and – eventually – to calibrate the model.

2.4 Model validation

For the reasons explained in the previous section and in accordance with the results presented above, the CO/NO_x ratio is the most appropriate one for this analysis. In an attempt to investigate the influence of the share of emissions allocated to urban driving conditions, the share of vehicle-kilometres driven in urban areas was extracted from TRENDS for the major vehicle categories. The country-specific percentage shares are summarised in Table 2.4.

After conducting a number of sensitivity runs with the COPERT model changing the urban shares of the various vehicle categories it was concluded that the emission ratio was most sensitive to changes in the shares of the diesel Light- (LDV) and HDV categories.

| | Germany | Spain | Finland | Portugal | United Kingdom |
|-----------------------------------|---------|-------|---------|----------|-------------------|
| Gasoline passenger Cars | 37.2 | 30.5 | 30 | 24 | 46 |
| Diesel passenger Cars | 37.2 | 68.8 | 30 | 24 | 46 |
| LPG Passenger Cars | 0 | 100 | 30 | 0 | 0 |
| Gasoline Light Duty Vehicles | 37.2 | 42 | 30 | 0 | 46 |
| Diesel Light Duty Vehicles <3,5 t | 40.5 | 78 | 30 | 4.3 | 46 |
| Heavy Duty Vehicles 3,5 - 16 t | 40 | 40 | 40 | 20.8 | 29 |
| Heavy Duty Vehicles >16 t | 6.8 | 24.9 | 20 | 20.8 | 29 |
| Urban Buses | 100 | 100 | 100 | 100 | 100 |
| Coaches | 0 | 0 | 0 | 0 | 0 |
| Mopeds | 45 | 100 | 20 | 15.2 | 100 |
| Motorcycles | 18.5 | 73.7 | 30 | 21.8 | 54 |

Table 2.4 Estimated values of urban share of mileage (in %) driven by the various vehicle categories as used in TRENDS.

Tables 2.5 summarises the suggested changes in urban shares and the resulting new ratios versus the respective concentration ratios. These values do not differentiate considerably from the 'default' ones, which have been estimated rather than measured.

Table 2.5. Suggested changes in the urban shares of TRENDS and comparison with concentration ratios resulting from the data analysis from traffic stations in the selected countries.

| | CO/NO _x | NO _x /PM | PM/CO |
|---|--------------------|---------------------|-------|
| Germany | | | |
| TRENDS default | 7.16 | 13.12 | 0.011 |
| +15% for HDV>16 t | 6.40 | 13.28 | 0.012 |
| Air Quality weighted average | 6.25 | 5.42 | 0.036 |
| Spain | | | |
| TRENDS default | 5.25 | 11.60 | 0.016 |
| -30% for diesel PC, diesel LDV = gasoline LDV, -20% for all HDV | 8.62 | 12.43 | 0.016 |
| Air Quality weighted average | 9.42 | 4.18 | 0.031 |
| Finland | | | |
| TRENDS default | 6.80 | 13.90 | 0.011 |
| Air Quality weighted average | 6.36 | 4.52 | 0.038 |
| Portugal | | | |
| TRENDS default | 3.90 | 14.72 | 0.017 |
| +15% for all PCs, -15% for HDV>16 t, +50% for mopeds | 5.88 | 15.98 | 0.017 |
| Air Quality weighted average | 6.97 | 2.49 | 0.057 |
| United Kingdom | | | |
| TRENDS default | 8.96 | 17.72 | 0.006 |
| +20% for HDV<16 t | 8.42 | 16.95 | 0.007 |
| Air Quality weighted average | 4.67 | 10.99 | 0.026 |

In order to further investigate the reasons contributing to the observed discrepancies, but also in an attempt to quantitatively define the 'outliers' (eventually supporting a better definition of hotspots), data for the individual stations are used. Figure 2.4 presents the case of Germany, where a scatter plot of the CO/NO_x ratios calculated for each station – resulting from the analysis described in paragraph 2.2.2 – is shown. The weighted average over the country is plotted on the same graph, as well as the respective exhaust emission ratio as calculated by TRENDS – resulting from the procedure described above. All station values situated outside an appropriately chosen range, defined here by ± 1.5 times the standard deviation (dashed lines), are considered as 'outliers'. Figure 2.5 shows the case of Spain, while the other countries are not shown due to the limited number of stations available. Evidently, the inclusion of as many as possible stations in the analysis will allow for a more thorough assessment.

Once the outliers have been identified, "zooming" in the street level will reveal any special conditions governing the measured concentrations. Prerequisite for this is the availability of hourly concentrations at both the traffic station and a nearby urban background station representing concentrations attributed to sources other than traffic.



Figure 2.4. Calculated CO over NO_x ratios for the individual stations in Germany against country weighted average and modelled with TRENDS.



Figure 2.5. Calculated CO over NO_x ratios for the individual stations in Spain against country weighted average and modelled with TRENDS.

In that case the traffic contribution may be calculated by simply subtracting the street concentrations from the background levels. Furthermore, detailed traffic data (traffic volume, fleet composition, average speeds) are necessary in order to enable the calculation of emissions with the COPERT model. Finally, meteorological data (temperatures, wind speed and direction) are particularly relevant to the interpretation and evaluation of various phenomena, such as the re-suspension of road dust and complicated dispersion processes. A further investigation at station level is however outside the scope of the present paper.

2.5 Conclusions and follow-up

In general, the agreement between measured and modelled CO/NO_x emission ratio suggests that the measured concentrations originate from traffic-related emissions. On the other hand, the large underestimation in the modelled PM/CO ratio clearly indicates that emission sources other than exhaust from diesel vehicles significantly contribute to the PM levels at urban hotspots. As diesel PM emissions are constantly decreasing due to technological improvements, PM emissions from gasoline-fuelled vehicles may constitute a considerable fraction of the total PM emitted from road traffic in the near future. Furthermore, primary non-exhaust particles, i.e. particles emitted directly as a result of the wear of surfaces and secondary particles, i.e. those resulting from the re-suspension of previously deposited material, add to the total PM concentrations in the ambient air.

Particle concentrations are measured mainly as PM_{10} , although the number of $PM_{2.5}$ stations is now increasing. However, in order to allow for a more consistent evaluation of the $PM_{2.5}$ emissions provided by TRENDS, more information on $PM_{2.5}$ concentrations needs to be collected at the monitoring sites.

It has been demonstrated that air quality data collected at urban traffic monitoring stations can be used to evaluate emission inventories. As a next step, a calibration of the TRENDS model used to compile the emission inventory is possible with reallocations of the mileage driven in urban environments based on reasonable assumptions. However, it should be borne in mind that there might also be other reasons possibly contributing to the observed discrepancies between modelled and measured ratios, including meteorological data, other sources of pollution, special traffic conditions, or combination of the above.

In any case, the inclusion of air quality data from as many as possible traffic stations well distributed over the countries will add to the confidence on their consistency and representativeness, reducing thus the noise of the various effects mentioned above. In view of the above it has to be mentioned that the results presented here are indicative and their role is mainly to present a methodology and the potential outcome of its application.

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Chapter 3: Air quality modelling

3.1 Introduction

The air quality modelling subtask in 2004 aimed at continuing the work started in 2003 and extending the number of models and cases applied with emphasis on City-Delta cities. Until September 2004, the data available allowed for three case studies, Stockholm (Hornsgatan), London (Marylebone Rd.) and Berlin (Frankfurter Allee). The Operational Street Pollution Model (OSPM) (Berkowicz et al., 1997), the recently developed Semi-Empirical Parameterised Street Canyon Model (SEP-SCAM) (URL1) and the Eulerian three-dimensional, prognostic, CFD model for microscale applications MIMO (Ehrhard et al, 2000), were applied to the three case studies. For all cases, the street emissions were calculated using COPERT 3 methodology and local traffic data.

3.2 The OSPM, SEP-SCAM and MIMO model applications

3.2.1 Stockholm, Hornsgatan

Street level concentrations of NO2, PM2.5 and NOx in Hornsgatan were calculated for the year 2000. Urban background was assumed to be properly described by the data from the corresponding monitoring station as this was located at roof level above Hornsgatan. Emission data were computed using COPERT 3 and the local traffic data. As the street canyon is located in downtown Stockholm, it was assumed that only HDVs with a Gross Vehicle Weight (GVW) lower than 16 tonnes were allowed, i.e. the share of HDVs with a GVW of 16-32 tonnes and over 32 tonnes was set equal to zero. The road gradient (about 2%) was also taken into account. The assumptions regarding the fleet composition and the additional information concerning the road gradient (this information was made available at a later stage during the course of the SEC project) lead to a slightly different set of emission data compared to that used in the Model Intercomparison study (see chapter 4). Although by considering the road gradient the NO_x emissions increase by ~4% and the PM_{2.5} emissions by ~7%, the overall effect (including the assumption that very large HDVs are not allowed to cross Hornsgatan street) is a reduction of the emissions with respect to those used in the Model Intercomparison study by ~15% for NO_x and ~10% for PM_{2.5}. This reduction in emissions leads to slightly reduced concentration estimates compared to those in chapter 4. In Figures 3.2 and 3.3 that follow, the SEP-SCAM and OSPM model runs have been performed using the latest set of emission data, whereas the MIMO model runs were performed using the initial dataset provided for the Model Intercomparison Exercise. However, as the differences are small, the results are comparable. It should also be noted that the COPERT methodology allows for the calculation of PM_{2.5} exhaust emissions from diesel vehicles only.



Figure 3.1. Diurnal variation of the total number of vehicles (top) and the HDV (bottom) in Hornsgatan.

The HDV percentage ranges from around 7-8% of the total number of vehicles in the evening hours until around 1:00 am, then rises quite rapidly to around 15 %-16 % in the early morning hours (2:00-6:00 am) and then remains relatively stable (between 10 %-12 %) during the rest of the day.

In Figure 3.2, the OSPM, SEP-SCAM and MIMO results for the average hourly concentrations in 2000 are compared with corresponding values from the traffic (street level) monitoring station. It should be underlined that the microscale flow and dispersion model MIMO was used in the framework of the air quality modelling subtask to calculate normalised concentrations (also referred to as c* values) for NO_x and $PM_{2.5}$ (not NO_2), for 16 wind directions. The different scaling methods to calculate hourly concentration time series from c* values are described in detail in Ketzel et al. (2001). In this modelling subtask, the TPT (Traffic Produced Turbulence) scaling method was used.



Figure 3.2. SEP-SCAM, OSPM and MIMO results for the average daily variation of NO_2 , NO_x and $PM_{2.5}$ concentrations at street level in Hornsgatan in 2000 compared with observations.



Figure 3.3. SEP-SCAM, OSPM and MIMO results for the monthly variation of NO_2 , NO_x and $PM_{2.5}$ concentrations at street level in Hornsgatan in 2000 compared with observations.

Results show that the diurnal patterns of the observed concentrations are generally underestimated by all models. Overall, all three models provide a good impression of the observations, closely following the diurnal and monthly patterns observed in the monitoring data. The slightly increased emissions used in the MIMO model runs lead to higher concentration estimates and thus provide a better impression of the average daily variation for NO_x and PM_{2.5} concentrations at street level, compared to the other two models. Comparing the semi-empirical model results, OSPM underestimates the actual concentrations more than the SEP-SCAM model. This is due to the additional concentration increment that is calculated by SEP-SCAM in order to consider the dependence of the flow regime on the aspect ratio and the fact that the traffic emissions are not uniformly distributed across the canyon. This factor is directly proportional to the emissions and hence larger concentrations are observed mainly during the day, when the traffic intensity is higher. Overall, in the case of $PM_{2.5}$, the underestimation of the model results compared to the measurements may indicate that emission sources other than diesel vehicles (e.g. contributions of gasoline vehicles) should also be taken into account in the calculations. An even greater underestimation is observed for NO₂ and especially NO_x for OSPM and SEP-SCAM. As was also discussed in the model intercomparison session during the 9th Model Harmonisation Conference, this may be due to a general underestimation of NO_x emissions. The ARTEMIS project findings and other emission factors are being compared with those used by the COPERT methodology, in order to study this possibility further.

3.2.2 Berlin, Frankfurter Allee

Street level concentrations of NO₂, PM_{10} , NO_x and CO in Frankfurter Allee were calculated for 2002 using SEP-SCAM, OSPM and MIMO models. Urban background was assumed to be properly described by the data from the corresponding monitoring station, although this was located at a distance of 2km from Frankfurter Allee. Emission data were computed using COPERT 3 and the local traffic data. It should again be noted that these emission data account for the PM_{2.5} exhaust emissions of diesel vehicles only.

As the detailed hourly counts for the number of HDV were not entirely reliable, an average factor of 4.8 % was suggested by the data provider and used for the model calculations. This percentage varies from 5.6 % on working days (Mo-Fr), to 3.4 % on Saturdays and 2.6 % on Sundays and public holidays. Compared to Hornsgatan, the HDV percentage in Frankfurter Allee is quite low. Although the number of vehicles moving along Frankfurter Allee is significantly higher than that moving along Hornsgatan (56,000 vehicles per day, compared to 35,000), differences in the vehicle fleet (vehicle classes), the lower percentage of HDV and the different height-to-width aspect ratio, lead to lower concentrations in Frankfurter Allee.



Figure 3.4. Diurnal variation of the number of vehicles in Frankfurter Allee.


Figure 3.5. SEP-SCAM, OSPM and MIMO results for the average daily variation of NO₂, NO_x PM_{10} and CO concentrations at street level in Frankfurter Allee in 2002 compared with observations.

All three model results provide a very good impression of the observations, closely following the diurnal and monthly patterns observed in the monitoring data. Results show that MIMO generally overestimates slightly the observed concentrations, while on the other hand SEP-SCAM and OSPM underestimate them. Furthermore, SEP-SCAM produces slightly higher concentrations than OSPM (this is further explained in section 3.2.1 - Hornsgatan case study analysis).

The slight underestimation in the CO and NO_x concentrations computed by the SEP-SCAM and OSPM models may be due to an underestimation of the average height of the buildings adjacent to the street. The data source used estimated the height to be around 21m, whereas other data sources indicate that it may even be around 30m. For PM₁₀, the monitoring data reveal a diurnal pattern that is rather unusual for a traffic station, but a similarly strange pattern is also observed for the background concentrations. It is not clear what local effects produce these patterns. However, the calculated data closely follow the monitoring data pattern and the underestimation observed in the modelled results is to be expected, since only PM_{2.5} diesel vehicle emissions are considered.





Figure 3.6. SEP-SCAM, OSPM and MIMO results for the monthly variation of NO_2 , NO_x , PM_{10} and CO concentrations at street level in Frankfurter Allee in 2002 compared with observations.



Figure 3.6. (continued).

3.2.3 London, Marylebone Rd.

Street level concentrations of NO_2 , PM_{10} , NO_x and CO in Marylebone Rd. were calculated for 2000.



Figure 3.7. Diurnal variation of the total number of vehicles (top) and the HDV (bottom) in Marylebone Rd..

Urban background concentrations were assumed to be properly described by the data from the urban background monitoring station in Bloomsbury. This is located at a distance of 2 km east of Marylebone Rd. and was the only station that could be used

for the analysis, as there was no other urban background station located closer. Similarly, the meteorological data was obtained from a station located 3.7 km away from Marylebone Rd. at 43 m above the ground, as no other roof level meteorological station was located closer by.

Emission data were computed using COPERT 3 and the local traffic data. It should once again be noted that these emission data account for the $PM_{2.5}$ exhaust emissions of diesel vehicles only. The HDV percentage in Marylebone Rd. is high compared to other case studies and ranges between 11-14% of the total number of vehicles during the day and then drops to vary between 5-9% during the evening and early morning hours (17:00-9:00). Although the average number of vehicles moving along Marylebone Rd. per day is 85,500 and therefore high and comparable to that of Frankfurter Allee (56,000), the measurements show significantly higher concentrations in London compared to Berlin for all pollutants. The large number of HDV, in conjunction with the low vehicle speed during the day (average speed of 35 km/h between 9:00-17:00) and the smaller road width (but similar building height) could be the reasons behind these high concentrations.



Figure 3.8. SEP-SCAM, OSPM and MIMO results for the average daily variation of NO_2 , $NO_x PM_{2.5}$ and CO concentrations at street level in Marylebone Rd. in 2000 compared with observations.



Figure 3.9. SEP-SCAM, OSPM and MIMO results for the monthly variation of NO_2 , NO_x , $PM_{2.5}$ and CO concentrations at street level in Marylebone Rd. in 2000 compared with observations.



Figure 3.9 (continued).

In a qualitative sense, all three model results for Marylebone Rd. generally reproduce well the diurnal and monthly patterns observed in the monitoring data. MIMO presents better coincidence with $NO_x PM_{2.5}$ monitoring data. In particular the predicted concentrations by SEP-SCAM and OSPM are systematically much lower than both the ones predicted by MIMO and the observed ones. The underestimation of the street level concentrations by all models may be due to the high wind speeds observed, as it is likely that due to the distance of the meteorological station from Marylebone Rd. the wind speed is not representative and thus higher dispersion is assumed leading to lower concentrations. Similarly to the other cases, an underestimation in $PM_{2.5}$ is expected as emission sources other than diesel vehicles (e.g. contribution of gasoline vehicles) have not been considered in the calculations.

3.3 Conclusions

Results from the application of OSPM, SEP-SCAM and MIMO models for the three aforementioned case studies, show that the concentrations measured at street level can be satisfactorily reproduced. Moreover, these results show that the diurnal patterns of the observed concentrations are generally underestimated by all models, with the exception of the Berlin case where MIMO has demonstrated an overestimation of the street level NO_x and $PM_{2.5}$ concentrations. However, both MIMO and SEP-SCAM provide a better impression of the observations than OSPM. Overall, MIMO has demonstrated better agreement with the observed data than SEP-SCAM with the exception of the Berlin case.

Further steps of the SEC modelling work will include the application of the aforementioned models to the case study of Prague (data is currently being collected and assessed) and other cities, provided that data is made available.

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Ketzel M., Berkowicz R., Flassak T., Lohmeyer A., Kastner-Klein P. (2001). Adaption of Results from CFD-Models and Wind-Tunnels for Practical Traffic Pollution Modelling. 7th International Conference on Harmonisation within Atmospheric Dispersion Modelling for Regulatory Purposes, Belgirate, Italy - 28-31 May 2001. Proceedings European Commission. Joint Research Centre. Environment Institute 261-265.

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Chapter 4: Model intercomparison report

4.1 Introduction

The model intercomparison exercise was planned in conjunction with the work performed within the Street Emission Ceilings (SEC) exercise of the ETC/ACC 2004 workprogramme, whose aim was to study specific hotspots and quantify the influence of local and urban emissions and other smaller scale effects on concentrations and exceedances. The intercomparison exercise was expected to provide an insight in the level of uncertainty that is inherent in the various model calculations and a first estimate of the uncertainty that enters from the street level, into a complete regional-urban-street scale model application. Moreover, the large number of models participating in the intercomparison and the variety of cases available enabled the evaluation of the model performance, bearing in mind the restrictions of the input data. The cases studied were: Hornsgatan (Stockholm), Frankfurter Allee (Berlin) and Marylebone Rd. (London). These are all busy streets, with available street level monitoring data (concentrations and traffic counts).

4.2 Procedure

The launch of the model intercomparison took place in March 2004, when various institutions were informed of the Hornsgatan data availability and the possibility to submit model results. The "call for participation" was open to all interested institutes and recipients of the information were encouraged to forward the call to other potential participants. Ten institutes took part in the Hornsgatan intercomparison and an additional eight were interested, but did not submit results. The interest of the participants led to the launch of the Frankfurter Allee and Marylebone Rd. cases, where additional institutes participated. Participation and presentation of model results was not anonymous.

The purpose of the model intercomparison was to assess the suitability of various models to describe the contribution of street level emissions to air quality levels in urban street canyons. The explicit comparison of the model results against the measured concentrations at street/road-side level (hotspot), as well as with the street/urban background level, led to interesting conclusions as regards the contribution of street emissions to the air quality inside street canyons. The detailed time schedule followed is summarised in Table 4.1.

Table 4.1. Analytic time schedule of the model intercomparison.

- 16/3/2004 E-mail informing the scientific community of the intension of launching the pilot model intercomparison for the Hornsgatan case study ("call for participation")
 24/3/2004 Public availability of the Hornsgatan dataset
 14/5/2004 Deadline for the receipt of model results
 3/6/2004 Presentation of Hornsgatan intercomparison results in the SEC session during the 9th Harmonisation Conference. Launch of the Marylebone Rd. and Frankfurter Allee cases
- 26/6/2004 Availability of Frankfurter Allee dataset
- 19/7/2004 Availability of Marylebone Rd. dataset
- 20/8/2004 Deadline for the receipt of Frankfurter Allee and Marylebone Rd. results

To ensure the comparability of model results, the participants were requested to follow a specific format and for this reason an excel worksheet was made available for the transfer of the results to the co-ordinator of the exercise.

The data requested included results for the full year (only average hourly and monthly values were required, not the complete hourly dataset), for a specific day (characterised by high concentration observations) and a specific hour of that day. This report concentrates on the models and results received for the full year, as these are the most relevant for the Street Emission Ceilings (SEC) task of the ETC/ACC 2004 workprogramme.

4.3 Input data

All input data were made available through http://aix.meng.auth.gr/sec using an excel file. Unless indicated otherwise, all data were collected by NILU¹ during the SEC Data analysis subtask of the ETC/ACC 2004 workprogramme and provided for the intercomparison. In all cases, the emission data were calculated by AUT/LAT².

4.3.1 Hornsgatan

4.3.1.1 Meteorological data

The meteorological data set included hourly data for wind speed, wind direction, temperature and global radiation for the period 1/1/2000-31/12/2000. Wind speed and direction were measured at a roof top monitoring station nearby Hornsgatan. Temperature and global radiation measurements were performed at Torkel monitoring station and downloaded from URL1.

4.3.1.2 Traffic data

The hourly traffic data included total number of vehicles, HDV percentage and vehicle speed for the period 1/1/2000-31/12/2000. Average hourly data for total number of vehicles, HDV percentage and vehicle speed were calculated by

³ Norwegian Institute for Air Research

² Laboratory of Applied Thermodynamics, Aristotle University Thessaloniki.

AUT/LHTEE³ and provided to the participants. The hourly traffic data were obtained from NILU.

4.3.1.3 Emission data

The average hourly emissions for NO_x and $PM_{2.5}$ were calculated using the COPERT 3 methodology. The length of the street canyon was set at 160 m. At the time of the calculation of the emissions, the road gradient (~2%) was not known and hence not considered in the calculations. Moreover, it was considered that all types of vehicles included in the TRENDS database are allowed to circulate in Hornsgatan street, including HDVs >16 tons.

4.3.1.4 Background concentrations

The hourly NO_x and $PM_{2.5}$ urban background concentrations were measured at a roof top nearby Hornsgatan and were available for the period 1/1/2000-31/12/2000. The hourly NO_2 background concentrations were measured at the urban background monitoring station Sodermalm and were downloaded from URL1.

4.3.1.5 Geometric characteristics

The street geometry was partly obtained from the data analysis report prepared by NILU and partly estimated from maps (Table 4.2).



Table 4.2. Geometric characteristics of Hornsgatan street canyon.

Figure 4.1. Hornsgatan street canyon and location of the street monitoring station.

³ Laboratory of Heat Transfer and Environmental Engineering, Aristotle University Thessaloniki.



Figure 4.2. Street and roof top stations in Hornsgatan. The street monitoring station used for the intercomparison is indicated by N (North side of the street).

4.3.1.6 Position of the monitoring station

Hourly NO_x , NO_2 and $PM_{2.5}$ street level concentrations were monitored on both sides of the street during the period 1/1/2000-31/12/2000. However, the north side measurements were selected for the intercomparison, as the pollutant coverage was better (measurements included $PM_{2.5}$). The hourly NO_2 street concentrations were downloaded from URL1 (station name Hornsgatan, located on the north side of the street).



Figure 4.3. Overview of Hornsgatan and street station.

4.3.2 Frankfurter Allee

4.3.2.1 Meteorological data

The hourly meteorological data set included wind speed, wind direction, temperature and global radiation for the period 1/1/2002-31/12/2002. Wind speed and direction, as well as temperature, were measured at station DEBE043, located at roof level, 25 m above ground and 9 km away from Frankfurter Allee. The hourly global radiation measurements were from the Berlin-Dahlem WMO-station, 14 km SW-bound of Frankfurter Allee, but still representative. These were obtained from the Senate Department of Urban Development in Berlin.

4.3.2.2 Traffic data

The total number of vehicles per hour for the period 1/1/2002-31/12/2002 was available separately for the westbound and the eastbound traffic. From this data, the average number of vehicles per hour was calculated and provided to the participants. The average hourly vehicle speed and a fixed daily HDV percentage (4.8%) were also available and provided for the intercomparison.

4.3.2.3 Emission data

The average hourly emissions for CO, NO_x and $PM_{2.5}$ were calculated using the COPERT 3 methodology.

4.3.2.4 Background concentrations

The hourly CO, NO_x, NO₂, PM_{10} and O₃ urban background concentrations were measured at Neukölln, Nansenstrasse, 3.7 km away from Frankfurter Allee, as there was no other background station located closer.



Figure 4.4. An overview of Frankfurter Allee.



Figure 4.5. Location of the traffic detectors and the street level monitoring station.

4.3.2.5 Geometric characteristics

The height and width of street canyon as well as the number of lanes were obtained from the data analysis report prepared by NILU. The angle of the street with respect to north was estimated using maps of the area. The inlet height was provided by the Senate Department of Urban Development in Berlin.

| Table 4.3. Geometric characteristics of Frankfurter Allee structure | eet canyon |
|---|------------|
|---|------------|

| Buildings' height on the northern side of the street (m): | 21 |
|---|------|
| Buildings' height on the southern side of the street (m): | 21 |
| Width (m): | 41.6 |
| Approximate angle the street axis makes with North (degrees): | 98 |
| Number of lanes: | 6 |
| Height of inlet (m): | 3.8 |

4.3.2.6 Position of the monitoring station

CO, NO_x , NO_2 and PM_{10} street level concentrations were monitored inside Frankfurter Allee.

4.3.3 Marylebone Rd.

4.3.3.1 Meteorological data

The hourly meteorological data set included wind speed, wind direction, temperature and global radiation for the period 1/1/2000-31/12/2000. Wind speed and direction, as well as temperature, were measured at the London Weather Centre, which is the only site with comprehensive meteorological data that can be obtained in Central London. This station is located 3 km away from Marylebone Rd. at 43 m above the ground. No other roof level meteorological station is located closer by. Another station that could be used was Heathrow Airport station, but this is located even farther away from the measurement site of Marylebone Rd.. The data analysis of the relevant wind speed data revealed an average yearly wind speed of 5.2 m/sec for 2000, which is higher than what one would expect to measure at roof level above a street canyon in central London. Moreover, the data is measured at 53 m above the ground (building height including mast), which is higher than the average building height close to Marylebone Rd.. The effect of this high wind speed is further analysed in section 4.5.3.1.

The hourly wind speed, wind direction, temperature data were obtained from the British Atmospheric Data Centre (URL 4) and provided by the Met Office (URL5). The solar radiation data were provided by the Environmental Research Group of King's College London.

4.3.3.2 Traffic data

The hourly traffic data included vehicle speed and number of vehicles for various classes that could be distinguished between LDVs and HDVs. The average traffic speed, the total number of vehicles and the percentage of HDVs per hour were calculated and provided to the participants.

4.3.3.3 Emission data

The average hourly emissions for CO, NO_x and $PM_{2.5}$ were calculated using the COPERT 3 methodology.

4.3.3.4 Background concentrations

CO, NO_x , NO_2 , $PM_{2.5}$ and O_3 urban background concentrations were measured at Bloomsbury station located at a distance of 2 km east of Marylebone Rd. and was the only station that could be used for the analysis, as there was no other urban background station located closer.

4.3.3.5 Geometric characteristics

The street geometry was provided by the Environmental Research Group of King's College London and completed using maps of the area (http://www.maporama.com and http://streetmap.co.uk).

| it 4.4. Ocometric endracteristics of Marylebolic Rd. street earlyon. | |
|---|-----|
| Buildings' height on the northern side of the street (m): | 22 |
| Buildings' height on the southern side of the street (m): | 22 |
| Width (m): | 35 |
| Approximate angle the street axis makes with North (degrees): | 76 |
| Number of lanes: | 6 |
| Height of the receptor inlet (m): | 3.5 |
| | |

Table 4.4. Geometric characteristics of Marylebone Rd. street canyon



Figure 4.6. An overview of Marylebone Rd.



Figure 4.7. Location of the street level monitoring station on Marylebone Rd..

4.3.3.6 Position of the monitoring station

CO, NO_x , NO_2 and $PM_{2.5}$ street level concentrations were measured on the south side of Marylebone Rd..

4.4 Participants and models used

Street level concentrations of specific pollutants for each test case were calculated as average daily variations for a whole year and/or specific day and/or specific hour using different models. The models, their type and the corresponding users during the intercomparison are presented in Table 4.5.

| Type of model | Model name | Applied by | |
|-------------------|----------------------------------|---------------------------------|--|
| Box model | BOXSTREET | CORIA (France) | |
| | CPB3 | Agenzia Milanese (Italy) | |
| Sami_amnirical | SEP-SCAM | LHTEE (Greece) | |
| models | | NERI (Denmark), | |
| moucis | OSPM | ESMG (Spain) and | |
| | | LHTEE (Greece) | |
| Caussian models | CALINE4 | Pisa University (Italy) | |
| Gaussian mouers | ADMS-Roads-Extra | ZAMG (Austria) | |
| Lagrangian models | LASAT | ZAMG (Austria) | |
| | MIMO | LHTEE (Greece) | |
| Eulerian models | ADREA-HF | NCSR "Demokritos" (Greece) | |
| | MISKAM | NERI (Denmark) and ZAMG | |
| | | (Austria) | |
| Lagrangian | VADIS | University of Aveiro (Portugal) | |
| and Eulerian | d Eulerian FLUENT CIEMAT (Spain) | | |
| combinations | GRAL | Gratz University (Austria) | |

 Table 4.5. Type of models and corresponding user.

Every model had a unique user, apart from OSPM which was applied by NERI (Denmark), ESMG (Spain) and LHTEE (Greece). Therefore, in the case of OSPM a different "modeller" intercomparison using the same input data emerges, leading to interesting conclusions related to a user-oriented sensitivity analysis. The simulation character of each model, the consideration of chemical transformation of the pollutants and the corresponding computational time required for the simulations are shown in Tables 4.6 and 4.7 respectively. Additional model details can be found in EEA's Model Documentation System (MDS) (URL 2).

It should be underlined that the flow and dispersion model MISKAM (version 4.2) was used in the framework of the model intercomparison to calculate normalised concentrations (also referred to as c* values) for 36 wind directions. The different scaling methods to calculate hourly concentration time series from c* values are described in detail in Ketzel et al. (2001). In the model intercomparison, the simple 1/u-scaling and the TPT (Traffic Produced Turbulence) scaling methods were used. Both MISKAM and MIMO results (average daily variation) that appear in this report were computed using the TPT scaling method, though the MIMO results were computed using 16 wind directions.

'n

| Simulation character | Model name | Chemistry |
|--|-------------|-----------|
| | CPB3 | _ |
| Statistical | MIMO | |
| (analysis of long-term AQ indicators) | SEP-SCAM | |
| | BOXSTREET | |
| | SLP-2D | _ |
| | VADIS | _ |
| Episodic | ADMS- | 2 |
| (analysis of short-term AQ indicators) | Roads-Extra | N |
| | CALINE4 | |
| | ADREA-HF | |
| | GRAL | - |
| Statistical/Enjandia | OSPM | |
| Statistical/Episourc | MISKAM | _ |
| | LASAT | |

Table 4.6. The simulation character of the models.

| | Table 4.7. The | simulation | period and | computation | al times. |
|--|----------------|------------|------------|-------------|-----------|
|--|----------------|------------|------------|-------------|-----------|

| Simulation period | Duration of the simulation | Model name | |
|-------------------|----------------------------|------------------|--|
| | Up to 10 minutes | BOXSTREET | |
| | Up to 10 minutes | OSPM | |
| | Up to 10 minutes | SEP-SCAM | |
| 1 year results | 1 to 24 hours | ADMS-Roads-Extra | |
| | 1 to 24 hours | LASAT | |
| | More than 24 hours | GRAL | |
| | More than 24 hours | MISKAM | |
| 1 day results | Up to 10 minutes | CPB3 | |
| | 1 to 24 hours | CALINE4 | |
| | 1 to 24 hours | VADIS | |
| | 10 minutes to 1 hour + | SLP-2D + Fluent | |
| | More than 24 hours | | |
| 1 hour results | 10 minutes to 1 hour | MIMO | |
| | 1 to 24 hours | ADREA-HF | |

4.5 Model results and intercomparison

4.5.1 Introduction

For all three cases studied, the models applied ranged from simple semi-empirical models to complex microscale models (Table 4.5). The former were applied for a full year, while the latter were used to simulate shorter time periods. In the analysis, four different comparisons can be distinguished (Table 4.8).

| Type of comparison | Hornsgatan | Frankfurter Allee | Marylebone Rd. |
|--|-----------------------|----------------------|---------------------|
| Model results for the full year | 2000 | 2002 | 2000 |
| OSPM model results for the full year, applied by different users | 2000 | 2002 | 2000 |
| Model results for a single day | 27.11.2000 | 3.7.2002 | 1.4.2000 |
| Model results for a specific hour | Hour 10 of 27.11.2000 | Hour 11 of 3.7.2002 | Hour 11 of 1.4.2000 |

Table 4.8. Type of comparisons and reference year for the three test cases.

For the full year application, only the average hourly diurnal variation was requested and submitted by the participants for the intercomparison. The hourly values for the whole year were not available and hence not analysed. In this report, only a representative sample of the intercomparison results is presented. The complete presentation of the intercomparison results compared to measurements and the corresponding comparison of model Delta Concentration(s) (DeltaCs = Modelled – Background concentrations) with the observed Delta Concentration (DeltaC = Hotspot – Background measurements) are available through URL 3. The OSPM results that are included in the following paragraphs originate from the NERI application, using the dataset provided for the intercomparison.

The model results corresponding to Figures 4.8-4.25 (actual concentrations, not DeltaCs) are presented and compared to hotspot measurements in Annex D. The statistical DeltaC results (Average, Bias, NMSE and Correlation Coefficient (CC)) are depicted in Annex E.

4.5.2 The Stockholm case

The results of the Hornsgatan case were presented at the 9th International Conference on Harmonisation within Atmospheric Dispersion Modelling for Regulatory Purposes held in Garmisch-Partenkirchen (Germany). Ten institutes provided model results and an additional eight participated in the dedicated session in Garmisch. The pollutants studied in the Hornsgatan case were NO_x , NO_2 and $PM_{2.5}$. Street level concentrations were calculated for the year 2000 using 12 of the 13 street scale models (Table 4.5). In Figures 4.8-4.10, model DeltaCs for the average daily concentration variation in the reference year are compared to the corresponding observed DeltaC.



Figure 4.8. DeltaCs intercomparison for NO_x average daily variation at street level in Hornsgatan in 2000 compared to DeltaC observed.

In Figure 4.8, NO_x DeltaCs are presented. All models reproduce the diurnal contribution of traffic emissions to the background concentrations with a correlation coefficient above 0.85. BOXSTREET, GRAL and MIMO model results are closest to measurement with BIAS values of 4.7, 5.8 and -8.3 respectively. During the early morning hours, the deviation of all DeltaCs with respect to observed DeltaC is low, but the results are generally underestimated thereafter.



Figure 4.9. DeltaCs intercomparison for NO₂ average daily variation at street level in Hornsgatan in 2000 compared to DeltaC observed.

In Figure 4.9, OSPM and SEP-SCAM NO_2 DeltaCs are generally the closest to the observed, with OSPM achieving better comparison during early morning hours, but underestimating the concentrations from 7:00 onwards. SEP-SCAM results overestimate the concentrations observed during the early morning hours before 8:00 and are closer to measurements thereafter. LASAT model also achieves results close

to the observed concentrations during the late evening and early morning hours, but underestimates the concentrations from 9:00 until 20:00. Although ADMS model reproduces the diurnal pattern observed in the monitoring data (the correlation coefficient is 0.76), the results overestimate the observed DeltaCs. BOXSTREET and LASAT Δ Cs have a correlation coefficient less than 0.5.



Figure 4.10. DeltaCs intercomparison for PM_{2.5} average daily variation at street level in Hornsgatan in 2000 compared to DeltaC observed.

Similarly to NO_x , $PM_{2.5}$ DeltaCs correlation coefficient for all model results is high, above 0.9 (Figure 4.10). MIMO has the highest correlation coefficient 0.98. Most model results are close to the measured data, although OSPM, SEP-SCAM, LASAT and MIMO models slightly underestimate the observed concentrations between 10:00 and 24:00.

4.5.2.1 The OSPM model applications for the Hornsgatan case

In Figures 4.11-4.13, the OSPM model results (DeltaCs) obtained by various users are compared with observations. NERI performed additional runs using modified input data with slightly increased street emissions based on emission factors deviating from those used by the COPERT 3 methodology. These results are depicted as NERI* in the intercomparison charts.



Figure 4.11. OSPM user DeltaCs intercomparison for NO_x average daily variation at street level in Hornsgatan in 2000 compared to DeltaC observed.

In Figure 4.11, NERI* application gives a DeltaC closest to the observed DeltaC, although for the period 9:00 - 20:00 the results are slightly overestimated. NERI, LHTEE and ESMG underestimate the traffic contribution, especially for the period 07:00 - 20:00 when road emissions are the highest. The correlation coefficients for all OSPM user DeltaCs contributions are close to 1.



Figure 4.12. OSPM user DeltaCs intercomparison for NO₂ average daily variation at street level in Hornsgatan in 2000 compared to DeltaC observed.

In Figure 4.12, NERI DeltaCs are generally underestimated, while ESMG and LHTEE are close to the observed DeltaC between 19:00 and 2:00, they fluctuate between a slight overestimation and a slight underestimation between 3:00-7:00 and underestimated the concentrations thereafter. NERI* give the highest concentration estimates as expected, achieving good results between 7:00 and 15:00, but slightly over predict the concentrations between 16:00 and 6:00.

In Figure 4.13, NERI* application gives higher $PM_{2.5}$ street contributions for nearly the whole day, while NERI and LHTEE applications underestimate the observed DeltaCs between 8:00 and 24:00, when the traffic contribution is highest. All correlation coefficients are above 0.96.



Figure 4.13. OSPM user DeltaCs intercomparison for $PM_{2.5}$ average daily variation at street level in Hornsgatan in 2000 compared to DeltaC observed.

4.5.3 The Berlin case

All models contributing to the Stockholm case study were also applied to the Frankfurter Allee case, and in addition the ADREA-HF model participated at this intercomparison. All 13 street scale models that appear in Table 4.5 were used to calculate street level concentrations. The pollutants studied were CO, NO_x , NO_2 and PM_{10} . In Figures 4.14-4.17, model DeltaCs for the average daily concentration variation in 2002 are compared to the corresponding observed DeltaC.



Figure 4.14. DeltaCs intercomparison for CO average daily variation at street level in Frankfurter Allee for 2002 compared to DeltaC observed.

In Figure 4.14, the results for CO are presented. All models have high correlation coefficients, although they underestimate the actual concentrations. OSPM, SEP-SCAM and GRAL DeltaCs are the closest to the observed, with BIAS values of -0.04, -0.07 and -0.05 respectively. ADMS, LASAT and CPB3 models underestimate the observed DeltaCs throughout the day. This can be attributed to an underestimation of the CO emissions, as in all case studies only hot emissions were considered. However, in the case of Frankfurter Allee the cold start CO emissions appear significant since the monthly concentrations analysis reveals model results close to measurements for the summer months, but underestimated values are computed for the winter months.



Figure 4.15. DeltaCs intercomparison for NO_x average daily variation at street level in Frankfurter Allee for 2002 compared to DeltaC observed.

In Figure 4.15, all model DeltaCs have a high correlation coefficient. OSPM, SEP-SCAM and GRAL model results are the closest to the hotspot contribution. ADMS, LASAT and CPB3 model results reproduce the average diurnal variation of the concentrations and have correlation coefficients of 0.88, 0.85 and 0.81 respectively, although they underestimate the actual concentrations and have corresponding BIAS values of -24.42, -15.01 and -44.57. BOXSTREET model gives results close to the observed DeltaCs, although the concentrations are slightly overestimated from 12:00 onwards.



Figure 4.16. DeltaCs intercomparison for NO₂ average daily variation at street level in Frankfurter Allee for 2002 compared to DeltaC observed.

In Figure 4.16, OSPM and SEP-SCAM model results prove to be the closest to the observed DeltaCs, with BIAS values of -0.28 and 2.03 respectively. ADMS and LASAT overestimate the concentrations at peak morning and afternoon hours. BOXSTREET model gives high NO₂ concentrations, while its diurnal pattern deviates from the observed, especially for the period 09:00 - 17:00.



Figure 4.17: DeltaCs intercomparison for PM₁₀ average daily variation at street level in Frankfurter Allee for 2002 compared to DeltaC observed.

In Figure 4.17, the PM_{10} DeltaCs are presented. With the exception of MIMO, all models underpredict the measured concentrations, which is not surprising since only exhaust $PM_{2.5}$ emissions from diesel cars were calculated and used as input data for the models. Although MIMO generally overestimates the actual concentrations, it presents the lowest NMSE compared to all the other models (0.261). BOXSTREET and MIMO present the highest correlation coefficient 0.84 and 0.81 respectivelly.

Unfortunately, $PM_{2.5}$ street level and background concentrations were not available to compare with the model results. However, the underestimation of most of the model results in Figure 4.17 denotes the important contribution of non-exhaust $PM_{2.5}$ particles such as pavement erosion, break and tyre abrasion, but also the contribution of other emissions such as re-suspension particles, to the PM_{10} concentrations observed at street level.

4.5.3.1 The OSPM model applications for the Frankfurter Allee case

Figures 4.18-4.21 show OSPM DeltaCs for the average daily variations of the street level concentrations obtained by various users compared to corresponding observed DeltaC. As in the case of Stockholm, NERI performed additional runs not using the input data provided for the intercomparison, but a slightly different dataset. This was characterised by increased PM street emissions, in order to obtain an estimation of the PM₁₀ emission data from the traffic observed in the street. The PM₁₀ emissions were calculated as the PM_{2.5} emissions given for the intercomparison (i.e. the exhaust contribution) plus non-exhaust emissions (30 mg/km for LDV and 300 mg/km for HDV) according to the emission factors suggested by Düring and Lohmeyer (2004). These results are depicted as NERI* in the intercomparison charts.



Figure 4.18. OSPM user DeltaCs intercomparison for CO average daily variation at street level in Frankfurter Allee for 2002 compared to DeltaC observed.

In Figure 4.18, the diurnal variation is reproduced well by all models. LHTEE and ESMG results compare well to the observed DeltaC for the early morning hours (1:00-6:00), but underestimate the concentrations thereafter. NERI and NERI* applications are generally closer to the actual measurements, but with a slight underestimation of the second peak presented in the pattern and have BIAS values of -0.04 and -0.06 respectively.



Figure 4.19. OSPM user DeltaCs intercomparison for NO_x average daily variation at street level in Frankfurter Allee for 2002 compared to DeltaC observed.

In Figure 4.19, NERI and NERI* give results close to the measured data, while LHTEE and ESMG applications both underestimate the concentrations observed. All models have high correlation coefficients (all above 0.86).



Figure 4.20. OSPM user DeltaCs intercomparison for NO₂ average daily variation at street level in Frankfurter Allee for 2002 compared to DeltaC observed.

In Figure 4.20, all applications reproduced the diurnal variation observed in the measured data, although the ESMG application generally underestimates the observed DeltaC and NERI, LHTEE and NERI* give higher concentration estimates between 18:00 and 3:00. LHTEE application presents the lowest NMSE (0.05) compared to the other three applications.



Figure 4.21. OSPM user DeltaCs intercomparison for PM_{10} average daily variation at street level in Frankfurter Allee for 2002 compared to measurements.

In Figure 4.21, all four OSPM users underestimate observed DeltaC, with the exception of NERI*, which computed slightly higher concentration estimates for periods 7:00 - 8:00 and 21:00 - 24:00. The NMSE for NERI* (0.11) is significantly lower than the one of the other three users. Additionally, NERI* has the highest correlation coefficient (0.83) and the lowest BIAS (-1.90) and hence describes best the hotspot contribution.

4.5.4 The London case

In Marylebone Rd. intercomparison case, the models that were applied and the pollutants under consideration were the same as those applied in the Frankfurter Allee case. In Figures 4.22-4.25, model DeltaCs for the average daily concentration variation in 2000 are compared to the corresponding observed DeltaC.



Figure 4.22. DeltaCs intercomparison for CO average daily variation at street level in Marylebone Rd. for 2000 compared to DeltaC observed.

In Figure 4.22, it is apparent that all model results are underestimated compared to DeltaC observed. All five applications present high negative BIAS values, which are -1.05, -0.96, -1.31, -1.22 and -1.47 for SEP-SCAM, GRAL, ADMS, LASAT and CPB3 respectively. However, the diurnal pattern is reproduced well and all models have a correlation coefficient above 0.8.



Figure 4.23. DeltaCs intercomparison for NO_x average daily variation at street level in Marylebone Rd. for 2000 compared to DeltaC observed.

As in the case of CO, in Figure 4.23, all models underestimate NO_x concentrations compared to DeltaC observed, although there is a reproduction of the diurnal variation by all models. The correlation coefficient for all models is again above 0.8. SEP-SCAM, GRAL and MIMO model DeltaCs results present the lowest NMSE (0.39, 0.23 and 0.10 respectively) values compared to the other four models.



Figure 4.24. DeltaCs intercomparison results for NO₂ average daily variation at street level in Marylebone Rd. for 2000 compared to DeltaC observed.

In Figure 4.24, SEP-SCAM NO₂ DeltaCs are the closest to DeltaC observed, whereas ADMS and LASAT are overestimated, especially during the traffic peak hours. BOXSTREET DeltaCs are underestimated, especially for the period 6:00 - 23:00. In addition, BOXSTREET model does not reproduce the diurnal variation well (the correlation coefficient is -0.44). The highest correlation coefficient was achieved by SEP-SCAM (0.97).

As in the cases of CO and NO_x, all models underestimate ΔC observed for PM_{2.5} (Figure 4.25). MIMO presents the lowest underestimation (BIAS: -0.93). SEP-SCAM, GRAL and MIMO models give results closest to the hotspot contribution (NMSE 0.20, 0.10 and 0.03 respectively) and all models have a correlation coefficient above 0.90.



Figure 4.25. DeltaCs intercomparison results for $PM_{2.5}$ average daily variation at street level in Marylebone Rd. for 2000 compared to DeltaC observed.

It is apparent that the models applied cannot describe sufficiently the hotspot contribution for the Marylebone Rd. case. All models for all pollutants, with the exception of LASAT and ADMS for NO₂, give underestimated results compared to the measurements. The overall weak performance is attributed to the fact that the available meteorological data, which were used as input to the models, cannot be considered representative for the specific application (see section 4.3.3.1 for details).

4.5.3.1 The high wind speed effect on the Marylebone Rd. concentrations

The effect of the high wind speeds used in the Marylebone Rd. case study is apparent in Figure 4.26, where SEP-SCAM DeltaCs for the average daily variation at street level for each of the four pollutants, is compared with DeltaC observed and with indicative SEP-SCAM#2 results, which were performed using the same input data, but with reduced hourly wind speeds compared to the actual measurements. In particular the hourly wind speed values were halved for the following reason: the wind speed, u₃₂, hypothetically measured on a mast of 10 m located at the roof level of Marylebone canyon is given by the following equation (Stull, R.B., 1988):

$$u_{32} = u_{53} \frac{\ln\left(\frac{32 - d_2}{z_{02}}\right)}{\ln\left(\frac{53 - d_1}{z_{01}}\right)}$$

where,

 u_{53} : wind speed measured on a 10 m mast located at the 43 m above ground roof level station approximately 1.88 miles away from Marylebone

 z_{01} , z_{02} : roughness length scales for the area where the roof level station is located d_1 , d_2 : scales of surface displacement above true surface for the area where the roof level station is located

Realistic values for z_{01} , z_{02} , d_1 , d_2 lead to $u_{32} \approx 0.5 \cdot u_{53}$. As can be seen in Figure 4.26, the wind speed reduction gives results much closer to the actual measurements, with the exception of CO, where especially after hour 11:00, the concentrations are still severely underestimated.



Figure 4.26. SEP-SCAM results for the average daily variation DeltaCs for all four pollutants at street level in Marylebone Rd. for 2000 compared to DeltaC observed and indicative SEP-SCAM DeltaCs results using halved hourly wind speeds intensity.

4.6 Conclusions

Overall, the model results for the Hornsgatan pilot case were close to the actual measurements, especially for $PM_{2.5}$ and NO_2 . This can also be seen in the Annex D of this report where all the model results (actual concentrations, not DeltaCs) are presented and compared to hotspot measurements. Larger deviations were observed for NO_x . One reason for this is the dominance of the urban background level for NO_2 and $PM_{2.5}$, as opposed to NO_x , where the street contribution dominates (which can be

easily seen in the corresponding DeltaCs). Thus, for NO_2 and $PM_{2.5}$, model deviations are to a large extent masked.

The intercomparison revealed that the models formulated specifically for describing pollutant dispersion in street canyons, yielded results closest to the actual measurements. OSPM results obtained by the three different modelling groups were in good agreement to each other. This result reveals that user introduced errors remain small for well documented modelling tools.

The models that participated in the Frankfurter Allee case generally underestimated the observed concentrations, especially in the case of $PM_{2.5}$ and NO_2 . On the other hand MIMO seems to overestimate the street level concentrations. The OSPM NERI* approach, with adjusted PM emissions, in order to obtain a better estimate for PM_{10} emissions and hence a better comparison with the PM_{10} concentrations measured, proved successful in describing the hotspot contribution.

Overall, as it has already been previously mentioned, the effect of the high wind speeds used in the Marylebone Rd. case study has possibly resulted in the underestimation of the hotspot contribution by nearly all models. This underestimation can be attributed to the fact that the available meteorological data, which were used as input to the models, cannot be considered representative for the specific application.

The results of both the Frankfurter Allee and the Marylebone Rd. cases emphasise the importance of correct and representative input data and the need for a consequent sensitivity analysis. An important issue in this context is the availability of representative traffic data and corresponding traffic patterns which have a major influence on the hourly variation of the emissions calculated. In addition to the above, appropriate station pairs (urban background and street level) rarely exist and are often (as in the case of Marylebone Rd. and Frankfurter Allee) not located close to one another. This situation leads to uncertainties as regards the representativeness of the background concentrations occurring in the area where the street is located. An additional problem is the location of the street level monitoring stations close to junctions, which leads to difficulties in the estimation of the number of vehicles contributing to the pollutant concentrations observed. It is of vital importance that specific guidance on best practices for the combined use of monitoring methods and models to assess AQ in hotspot/street level are established. Moreover, the standardisation of the methods used to provide input for AQ assessment would lead to reliable and accurate data and would enhance quality assurance. Last but not least, the increase of station pairs is imperative in order to broaden hotspot assessment in European cities.

The model intercomparison results discussed in the present report show the feasibility of using a number of street scale models to study the contributions of street scale emissions to the air pollutant concentration levels at hotspots. For demonstrating the usefulness of the approach with regard to policy related applications it is necessary to extend such applications to more urban areas and additional street canyon situations in individual cities. It must be emphasised that in order to continue such model intercomparison activities in the future, it is important that valid datasets are prepared and made available and that a minimum set of requirements is specified for the submission of information on specific street canyons. In addition, a comprehensive Street Canyon Database should be established to include all essential information characterising major hotspots in European cities, so that street scale models can be applied using this data, thus providing the possibility of comparing results against a number of applications. Considering also the aim of the Street Emission Ceilings exercise (under which the intercomparison datasets where collected) to quantify the influence of local emissions on the concentrations and exceedances and acquire an estimate of the uncertainty that enters from the street level into a complete regionalurban-street scale model application, such intercomparison exercises would contribute significantly to this goal. Furthermore and considering the needs of non-expert model users, the intercomparison demonstrated that easy-to-use models can estimate the concentrations in hotspots and thus improve assessments and evaluations of measures to attain compliance with limit values.

Last but not least, the increase in the number of participants from one case to the next shows the interest of the scientific community to participate in such exercises and is promising in terms of continuing such work in the future, provided that complete and reliable datasets are available.

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Chapter 5: Street typology

5.1 Introduction

5.1.1 Background and purpose

This report builds on the report of Phase 1 of the Street Emission Ceilings (SEC) project (ETC/ACC, 2004). The SEC project has been set up as a three year project. Its aims are (1) to develop a simple model for city authorities for identifying streets with possibly high levels and (2) to make a simple tool for providing estimates of urban street levels to the integrated assessment modelling in CAFE. In view of the timetable of CAFE, the current Phase 2 focuses on the model development to serve CAFE.

Even though it is likely that the final result of the three year project will be more accurate than the Phase 2 version presented here for support in CAFE, we feel that the accuracy of the model is not the limiting issue. A rigorous treatment of streets in integrated assessment modelling would require a database of street properties throughout the EU, which is currently lacking and inclusion of a street module in the RAINS model, which is currently not feasible. The Phase 2 model proposed here should be applied with caution; in view of its limitations it should be regarded as nothing more than a tool for making estimates of street levels in the EU. Especially when one compares a calculated concentration with a limit value, one should be aware that the uncertainty in the *difference* between the two values can be very large.

Application in Integrated Assessment Modelling

An important goal of SEC is to provide a tool for integrated assessment, such as the work currently done in CAFE. The typology development work in Phase 2 has particularly focused on this. Application in integrated assessment at the European scale could be carried out along the following lines.

On the short term, integration of the SEC model with models for the urban and European scale cannot be foreseen. It is not yet clear what City-Delta will deliver and the optimisation system of RAINS cannot be simply applied to a system that includes hotspots. A more feasible approach is to use the SEC model for evaluation of the impact of given scenarios. After calculations by RAINS of the regional background and additional calculations of the urban background (preferably using the result of City-Delta, if that is not available using other approaches, e.g. the one of MERLIN), the SEC model can be used to produce a table of typical levels in the various street types under a given scenario. The typology described below would result in a table of twelve street types per European region.

Without further work, it will not be possible to quantify how many streets of each street type exists in Europe, because data on this do not exist. It is relevant to collect data on this. It does not seem possible to do this rigorously for the whole of Europe, but sufficient insight may be gained by collecting data from a limited number of cities across the EU. For e.g. 10 cities that have a database on their streets, the parameters needed in the street typology should then be collected. Cities with a traffic-orientated database would probably have these data readily available, except the two parameters characterising the street configuration (canyon or not; broad or narrow canyon – see below). For the determination of those two parameters, some inventory work needs to be done, but as the study would not be aiming at describing individual streets, the effort can be limited to the work needed to acquire a statistically representative database.

In the SEC Phase 1 report, we have proposed to develop a typology based on Table 5.3 *Possible key parameters* of that report. This table is repeated below as Table 5.1; it will be the starting point of the street typology development in Phase 2. On second consideration, we have changed a few entries; these are marked in the table.

Key parameters are candidate parameters for the model to be developed. These can either be *Classified parameters* (fixed in classes, representing ranges) or *Continuous parameters* (retained as explicit continuous parameters in the model formula(s)). The intention of the typology development is to keep the number of continuous parameters as low as possible, preferably to have only one continuous parameter. See the Phase 1 report.

| Parameter | a. Importance | b. Suitability | c. Data availability | |
|--------------------|------------------------|------------------|----------------------|---------------|
| | for air | for modelling | On specific | Statistics at |
| | pollution ^a | | street for local | European |
| | | | authorities | level |
| | Str | eet parameters | | |
| Emission of local | +++ | +++ | ++ | +++ |
| traffic | | | | |
| Average daily | +++ | +++ | +++ | ++ |
| traffic intensity | | | | |
| Mean percentage | ++ | +++ | ++ | ++ |
| trucks | | | h | |
| Age of vehicle | ++ | ++ | ++ 0 | +++ |
| fleet | 1- | | | |
| Annual mean | ++/+++ 0 | +++ | +++ | +++ |
| wind speed at | | | | |
| nearby meteo | | | | |
| station | h | | | |
| Enclosure by | ++ 0 | ++ | +++ | + |
| buildings | . h | | | |
| Traffic behaviour | +/++ 0 | + | +++ | + |
| Street width | ++ | ++ | +++ | - |
| Distance to | ++ | +++ 0 | +++ | - |
| locations with | | | | |
| population | | | | |
| exposure | | | | |
| | Backg | ground parameter | rs | Γ |
| Distance from | +/++ | ++ | +++ | +++ |
| centre | | | | |
| City size | +/++ | ++ | +++ | +++ |
| Region in EU or | +/++ | +++ | +++ | +++ |
| latitude | | | | |
| Spatial isolation | +/++ | +++ | ++ | ++ |
| from other sources | | | | |
| Presence of | +/++ | + | ++ | + |
| industry | | | | |

^a The importance for air pollution indicates how much the variability of the parameter in streets with considerable traffic influences the total annual concentration characteristics (annual mean, percentile) near the street:

+++ Order of magnitude for NO_x , CO, benzene; factor of two for NO_2 and PM_{10}

++ Factor of two for NO_x , CO, benzene; tens of percents for NO_2 and PM_{10}

+ Tens of percents for NO_x , CO, benzene; ten percent for NO_2 and PM_{10}

^b Changed with respect to the corresponding Table 3 of the Phase 1 report.

Table 5.1 gives criteria for judging the relevance of a parameter. A further criterion, not indicated in the table, could be whether the parameter is likely to be changeable by measures. If it is, it is more interesting to distinguish than if it is not. A reason for distinguishing the percentage trucks as a separate parameter is that forthcoming emission reductions of trucks and private cars are quite considerable and follow different tracks in time.
In this report, we will develop the typology further for the street parameters. The characterisation of the urban background levels is left to the City-Delta project or an alternative approach. It should be noted that for the calculation of NO₂ concentrations the urban background level should be known not only for NO₂, but also for ozone.

An iterative procedure is envisaged, in which (a) a typology is proposed, which (b) is then applied in formulae or nomogrammes for each type. The result will then be reconsidered in terms of sensitivity for variations within a type, after which the typology and formulae may be improved as in steps (a) and (b). The first round, reported here, will be largely based on expert judgement, in the second round further substantiation by sensitivity analyses is envisaged.

The model will calculate annual statistics, in particular annual mean concentrations and numbers of exceedances of hourly or daily thresholds (or corresponding percentiles). As the typical user of the model will not have hourly input data available, the purpose will be to develop a model based on permanent or annual characteristics of the streets. This is particularly true for CAFE, where not specific streets but generic street types are of interest.

We will not attempt developing different typologies for different pollutants or for different concentration parameters (annual mean and percentiles). In principle, the optimum division in street type can be expected to depend on this. However, in view of the inherent uncertainties it is doubtful whether this complication would significantly increase the accuracy. Consequently we will not make this differentiation in the current phase.

5.1.2 Typology and model application

Below, we will first describe the development of the *typology*, i.e. the selection and quantification of street characteristics. After that, we will present an *application* of the typology using a street pollution model.

The calculation of statistics of the hourly and daily concentrations deserve special attention here. The typology only defines permanent and annual characteristics, so the calculation of hourly and daily statistics will need to be based on default assumptions. In the model application given below, the hourly and daily statistics are calculated from (fairly robust) empirical relations with the annual mean concentrations. Alternatively, it is also possible to construct hourly (or daily) time series of meteorological and traffic data, based on typical patterns and then calculate hourly and daily statistics by hourly (or daily) calculations. It is questionable, however, whether this will result in higher accuracy, given the fact that the typology, as defined below, does not provide input on how intra-annual variations deviate from normal conditions. It is therefore tempting to simplify the method and define the use of empirical relations between the annual mean and hourly or daily statistics as belonging to the typology. However, from a more basic point of view, we prefer to regard the calculation of hourly and daily statistics as a model application, thus leaving it up to the modeller how to arrange this.

5.2. Definition of the typology

5.2.1 Selection of key parameters

In the typology, a trade-off has to be made between model accuracy (requiring many explicit and continuous parameters) and simplicity (requiring a limited number of parameters, classified as much as reasonable). In this section, we will select the parameters that we need to distinguish explicitly because their variability in Europe is so large that it cannot be characterised by a single default value.

In Table 5.1, only one parameter is variable enough to cause (on an annual basis) the local contribution to air pollution to range over an order of magnitude:

• the average daily traffic intensity.

This parameter is proposed as continuous parameter.

Starting from Table 5.1, we will consider other parameters that may cause a large variation in the local contribution to air pollution; these are variable enough to cause (on annual basis) the local air contribution to range over about a factor of two between streets. We have renamed some parameters and have added four other parameters to consider: cold start, tunnel, trees and road slope. The evaluation of the variability below relies largely on expert judgement of the SEC team and occasional consultation of other experts; for most parameters it was hardly possible anyway to calculate the variability, but also the limited resources of the study made it necessary to resort to judgement.

Driving pattern

We will distinguish motorway and urban street traffic. Congested and free-flowing traffic may be considered for a second division, but as the differences for the total emissions on an annual basis are expected to be of the order of 30-50%, we will not make this distinction. For each of the two types, we hence choose a pattern intermediate between free-flowing and congested traffic.

• Cold start

In the first minutes after departure, emissions of some pollutants are much higher than normal. For busy streets, however, it is considered unlikely that total emissions are much higher than normally due to cold start effects.

• Obstacle geometry

The distinction in street configurations most commonly made is street canyon and non-canyon configuration. For canyons, it is customary to regard the aspect ratio (i.e. the ratio of street width and building height) as the most important variable, but in practice the concentrations are more sensitive to the street width than to the aspect ratio (for given street width). For non-canyon streets we will not take rural surroundings into account, because we are targeting the typology to urban environments. Motorways would therefore be limited to those in urban environment, which will be characterised by an urban roughness ($z_0=1m$). This results in two obstacle geometries: street canyons and urban non-street canyons (the latter including motorways, e.g. urban ring roads).¹

¹ In wind tunnel experiments, the highest concentrations were found in roads with canyon-like buildings on one side and no buildings on the other side. This is due to the fact that in such a configuration the wind at street level

Street width

The street width is the most relevant geometric parameter for street canyons. For street canyons the distance of road traffic to the receptor point is in practice usually linked to the street width. For non-canyon streets, this distance sufficiently defines the geometry. Therefore the street width will be indirectly characterised by the distance to the receptor point (see below).

Tunnels

High concentrations are know to occur at tunnel exits. There are models for such situations, but the levels depend strongly on the configuration and surroundings. We will not attempt to develop a typology for tunnels, but we need to retain it as a highly relevant category, with probably the highest traffic related pollution levels that exist.

Trees

The presence of trees is known to affect dispersion in streets and may increase concentrations significantly [Hout et al, 1989]. Of the current standard models, only the CAR model has a provision for trees, a tree factor that increases levels by 25% or 50% depending on the tree density. Since this is not a generally accepted approach, we will not include trees in the models and hence consider it as a contributor to the variability within a street type.

• Mean % trucks

As the major part of the local street contribution may be due to trucks and streets may have significantly different percentages of trucks, this parameter is considered important enough to distinguish.

- Annual mean 'meteo' wind speed For practical applications, it is not useful to have the wind speed in the street or at roof top as input parameter, as this is usually not available. Statistics of wind speed at meteorological stations is generally available. It varies across Europe by more than a factor of two, but less than an order of magnitude. It could be taken into account explicitly, but we will attempt to include it as a variable dependent on
 - the EU region.
- Other meteorological characteristics

Possibly the annual mean wind speed is not sufficient for characterising the local dispersion regime, e.g. the wind direction distribution may be very asymmetrical. Another relevant feature may be the topography of a city, which could e.g. lead to high episodic levels. It is not clear how strong deviations from the average behaviour can be brought about by these characteristics (apart from wind speed). For the current phase, we will not take other meteorological variables into account, at least not for the street level (the importance for the urban background levels is not considered here). This will be revisited when more specific information from the COST 715 action on Meteorology applied to Urban Air Pollution Problems will become available.

• Orientation of the road

The orientation of the road with respect to wind direction is known to be important for the concentrations near streets. For usefully including the orientation of the road, it has also to be known whether relevant receptors are upwind or downwind of the (local street level) wind. Generally, the hourly concentrations are very dependent on whether the receptor location it is upwind or downwind of the

virtually always blows from road to building (Den Tonkelaar et al., 1987). This geometry is represented as a street type in the CAR model, but because the phenomenon is not generally accepted, we will not include this street type here.

traffic, but the annual concentration statistics are not very dependent on the wind direction. The variability depends not only on frequency of wind directions relative to the street orientation, but also on wind speeds per wind sector. Model calculations with the TNO hourly traffic pollution model for the Netherlands (where southerly to westerly winds prevail to some extent) gave dependence of the order of 10-20%. As the dependence is, for the annual concentration statistics, expected to be considerable less than a factor of two in most situations and a simple characterisation could not be found, the road orientation was not included in the typology.

Road slope

The emission depends on whether cars ride on flat terrain, uphill or downhill. However, usually uphill and downhill traffic on the same road roughly compensate the differences with traffic on a flat road, but for unidirectional traffic this is not the case. Although it is not clear how much the concentrations can be increased in unfavourable cases, we will in this phase not distinguish unidirectional upslope traffic as a special type.

• Composition of fleet

The composition of the fleet (diesels, age of cars, etc) is important for the total emission of street traffic. This composition is known to vary across the EU, but is largely country dependent. We will attempt to include it as a variable dependent on the EU region.

Base year

For the base year, i.e. the reference year for scenario variants, we are taking the current situation (e.g. 2004) or a scenario year (2010, 2020). The emission factors in the model should be available for each relevant year.

Distance to receptor point

A major question is whether the concentrations should be calculated at locations where human exposure occurs or also at shorter distances. From a health perspective, exposure would be the obvious choice, but the air quality directives may be read as defining the limit values irrespective of exposure. For street canyons this distinction is often not so important, because the distance of exposure, usually at the kerb not far from the building faces, is linked to the distance of the buildings, which is already characterised by a classified parameter (canyon width). For open roads on the other hand, especially motorways, the distance to exposure can vary strongly, largely independent of other parameters. As the distance to the nearest relevant location can be very important for the concentration, there is reason to define the distance from the traffic or the road axis as a continuous parameter. However, to avoid complicating the approach by introducing a second continuous parameter, we will make a division in classes. The class borders of motorways and urban non-canyons can be chosen to be different.

5.2.2 Variability within a street type: unfavourable cases

The Phase 1 report discusses the fundamental problem that in a typology based on classes the unfavourable cases within a type are not taken into account, because the most normal street for a type will be taken. Especially for evaluating the attainability of limit values in streets, these unfavourable cases are highly relevant. We will attempt to solve this by giving for each street type a *typical case* and an *unfavourable case*, corresponding to:

- A *typical case calculation*: for estimating the typical levels in the street type.
- A *worst case calculation*: for identification purposes: in which types may problem situations occur?

This means that two model curves per street type are needed. In the Phase 1 report, it has been shown that the variability within a street type can only partly be modelled. The variability within a street type may in principle be derived from measurements, but then air quality data need to be available per street type, which is not the case. In this phase, we will estimate indicative factors for the concentration ratios between the unfavourable case and the typical case. It may be argued that quantifying this variability is belongs to the typology methodology, but it is more practical to estimate this while applying the methodology; hence the quantification of unfavourable cases will be addressed in Chapter 3.

5.2.3 Specification of street types

Based on the considerations above, Table 5.2 below lists the parameters that will be taken into account in the typology and indicates how the parameters will be dealt with.

| Parameter | Characterisation |
|------------------------------------|--|
| Traffic intensity | Continuous parameter (mean total number of vehicles per day) |
| Driving pattern ¹ | 2 types related to obstacle geometry: typical for motorway; typical for urban streets |
| Geometry | 2 geometries: urban non-canyon; canyon |
| Canyon width | Only for canyon: 2 types, with class border at 20m – this will be taken into account in the 'distance road axis to receptor' below |
| Distance road axis to receptor | 2 types depending on geometry and driving pattern. Class border: for non-canyon motorway at 50m, for non-canyon urban traffic 30 m, for canyon ³ / ₄ of the canyon width |
| Wind at meteo station ¹ | Link to EU region |
| % of trucks ¹ | 2 types; class border 10% |
| Age of fleet | Link to EU region |
| EU region | To be decided in relation to urban background model. If no useful combination can be made, the treatment of wind and fleet age should be reconsidered. |
| Base year | 2004, 2010, 2020 (depending on the application) |

Table 5.2. Street parameter taken into account in the typology and method of characterisation

¹ As annual characteristic

The table above leads to four combinations (2 distances (for canyons these are linked to canyon width, so canyon width is not an independent parameter), 2 percentages of trucks) in each of the three street geometry/driving pattern combinations, resulting in $4 \times 3 = 12$ street types for a given base year and a given EU region. Table 5.3 gives for each of these types input data on an annual basis for model calculations. For

models based on hourly input data, hourly wind speed and traffic data should be taken from a realistic or idealised case and rescaled to the annual averages.

| Geometry/driving pattern | Geometry paramete r | % trucks | Canyon width | Driving pattern 2) | Wind speed | Fleet age | Distance 3) |
|--|---------------------------|-------------|-----------------|--------------------------|----------------------------|----------------------------|--------------|
| Urban motorway (4 combinations) | z ₀ =0.1m | 7%/15% | - | 80 km/h | - | | 25m; 100m |
| Urban non-canyon street (4 combinations) | z ₀ =1m | 7%/15% | - | 26km/h | Coupled to EU region | Coupled to EU region | 10m; 40m |
| | | | | | | | |
| Canyon (4 combinations) | H=15m | 7%/15% | 15m 40m | 26km/h | | | 5m 15m |

Table 5.3. Input parameters for the modal (typical) street of street types¹⁾

¹⁾ In addition the age of the fleet and the average meteo wind speed has to be taken, dependent on the EU region. This needs to be defined later, consistent with the regions chosen in City-Delta.

²⁾ The speeds in the table are a crude indication. If emission data allow, the emission should be based on a pattern intermediate between free-flowing and congested for the street types concerned.

³⁾ The lower distance should not be combined with unrealistically high traffic intensities.

5.3 Application of the typology

In this chapter, we will apply the typology. We will use the CAR model (Hout and Baars, 1988; Eerens et al., 1993) as an example, as it has been developed along the same principles as the current SEC approach. We will use it for the annual average concentrations and use its approach for the exceedance statistics, but based on new empirical relations for statistics of the hourly and daily concentrations in Europe.

For a model for local authorities, resulting from a possible next phase, we will need to develop a full set of such curves, preferably in the form of formulas. For support to CAFE, this is not yet needed. The concentrations can then be calculated with existing models, as in the example based on CAR below.

5.3.1 Calculation of the annual mean concentration using the CAR model

Typical streets

Using the input parameters of Table 5.3, the curves as a function of distance to the road axis are presented in Figures 5.1 and 5.2 (annual mean DeltaCs, where Delta C= Street – Background concentrations). Table 5.4 lists the input parameters for each of the twelve street types. For the 'EU region' (as mentioned in Table 5.3) we have chosen an arbitrary location in Flandres (Belgium). The annual mean urban background concentration was 35 μ g/m³ for PM₁₀, 25 μ g/m³ for NO₂ and 40 μ g/m³ for O₃. The average wind speed at meteorological stations was 3.7 m/s, considerably higher than in many other EU regions. For application in CAFE, these calculations have to be done for all EU regions that are distinguished, but for this example only one EU region is sufficient.

It should be noted that all curves for canyon and non-canyon streets have been plotted for traffic intensities up to 100,000 vehicles per day - as this intensity is in practice not attainable in narrow street types, the highest values in the figures should be read as theoretical, which will not occur in practice.



Figure 5.1. Annual mean PM_{10} DeltaC, as a function of street type and traffic intensity (based on conditions in Belgium).



Figure 5.2. Annual mean NO_2 DeltaCs, as a function of street type and traffic intensity (based on conditions in Belgium).

| Street type | | Geometry | Fraction of trucks (%) | Traffic behaviour | Distance receptor to road axis (m) |
|-------------------|------|---------------------------|---------------------------|-------------------|--|
| Motorway 1 | | Open z ₀ =0.1m | 7 | Typical motorway | 25 |
| Motorway 2 | 2 | Open $z_0=0.1m$ | 7 | Typical motorway | 100 |
| Motorway 3 | | Open $z_0=0.1m$ | 15 | Typical motorway | 25 |
| Motorway 4 | | Open $z_0=0.1m$ | 15 | Typical motorway | 100 |
| Urban | non- | Open, z ₀ =1m | 7 | Typical urban | 10 |
| Urban canyon 2 | non- | Open, z ₀ =1m | 7 | Typical urban | 30 |
| Urban canyon 3 | non- | Open, z ₀ =1m | 15 | Typical urban | 10 |
| Urban canyon 4 | non- | Open, z ₀ =1m | 15 | Typical urban | 30 |
| Canyon 1 | | Width/height = 1 | 7 | Typical urban | 5 |
| Canyon 2 | | Width/height = 2.7 | 7 | Typical urban | 15 |
| Canyon 3 | | Width/height = 1 | 15 | Typical urban | 5 |
| Canyon 4 | | Width/height = 2.7 | 15 | Typical urban | 15 |

Table 5.4. Street type parameters for *typical street cases*¹.

¹ Non-urban motorways and tunnels are not included.

Unfavourable streets

As discussed above, in unfavourable streets within a street type the levels can be higher for many reasons: lower distance or higher fraction of trucks than typical, unfavourable traffic behaviour, presence of trees, lower wind speed than typical for the region, higher background levels than typical for the city type. Tentatively, we estimate that the local contribution to the concentrations in unfavourable streets is a factor 2 higher for PM_{10} and (taking the non-linear relation with emissions into account) 1.5 for NO₂.

5.3.2 Calculation of exceedances of the hourly and daily limit values

5.3.2.1 Approach taken

For model calculations of the number of exceedances of the hourly limit value of NO_2 and the daily limit value for PM_{10} , one could ideally use hourly and daily input data. This is not feasible for the simple model envisaged here. One could also construct hourly/daily time series from annual statistics using default assumptions and then do hourly/daily calculations. This would give an impression of higher detail due to the hourly calculations, but it would in reality still rely fully on annual statistics as input. Another way of calculating number of exceedances is to use the modelled annual mean concentrations together with empirical relationships between the annual concentrations and numbers of exceedances. This approach is taken here. As AirBase provides data for hundreds of streets stations throughout the EU, this provides at the same time a good insight in the accuracy of the approach.

Instead of the number of exceedances (this is the parameter specified in the limit values), we will model the corresponding percentile. There are several reasons for this. For comparisons with the limit value, it does not matter whether number of exceedances or percentiles is used: if the percentile is higher / lower than the percentile corresponding with the limit value, the number of exceedances is higher / lower than allowed. Another reason is that for the number of exceedances the formula depends on the threshold, while for the percentile the formula is independent of the threshold. A very practical further reason, finally, is that percentiles could easily be extracted from available AirBase data, while calculating the numbers of exceedances would have required considerably more effort.

5.3.2.2 Empirical information

In Figures 5.3 and 5.4, the percentiles corresponding with the daily and hourly limit values are plotted against the annual average concentration. The figures present the street station data of 2001 and 2002 from AirBase. Stations with a data capture below 90% were not taken into account. For PM_{10} this resulted in 230 PM_{10} stations in 2001 and 339 in 2002. For NO₂, there were 447 such stations in 2001 and 427 in 2002.



Figure 5.3. The 90.1 percentile of daily concentrations of PM_{10} (corresponding to the daily limit value) versus the annual mean concentration of PM_{10} , for European street stations in 2001 and 2002. Source: AirBase.



Figure 5.4. The 99.8 percentile of hourly concentrations of NO_2 (corresponding to the hourly limit value) versus the annual mean concentration of NO_2 , for European street stations in 2001 and 2002. Source: AirBase

Figure 5.3 shows a distinct correlation of the 90.1 percentile for the daily mean (corresponding to the daily limit value) with the annual mean for PM_{10} , with $R^2 = 0.92$. The regression line shows a small intercept of $+2.5 \,\mu g/m^3$ on the 90.1 percentile axis.

A similar plot for NO₂ in Figure 5.4 of the 99.8 percentile of hourly concentrations (corresponding to the hourly limit value) against the annual mean, shows that the relation deviates significantly from linear (taking into account that the relationship has to go through the origin (0,0). As should be expected for a percentile as high as the 99.8 percentile, the scatter is considerable. For the model, the most relevant values are those around or above the 99.8 percentile 200 μ g/m³. When selecting only values >150 μ g/m³, there is no significant deviation from proportionality: we found a ratio of 2.8, with a standard deviation of the relative error of 18%.

One of the reasons for the non-linearity in Figure 5.4 for NO_2 is that the variability of the local contribution to hourly concentrations tends to be lower than the variability of the background concentrations. A more accurate approximation might perhaps be achieved when the contribution of the background to the total concentration would be known. As these data were not available and complications due to the non-additivity of contributions to percentiles are likely to arise, this would require more research than could be done in this work.

A difficulty for a percentile as high as the 99.8 percentile is that measuring errors are likely to play a significant role at some stations. Erroneous high values that have not been removed from the data set may directly contribute to the 99.8 percentile. As practitioners should be reluctant to remove without clear reasons high readings from measurements that are done for surveillance, one may speculate that the real ratio is lower than the regression formula found here. On the other hand one may argue that these errors are inherent to the current compliance checking practice and hence it can be justified to use the database of measuring results as the reference for the model.

5.3.2.3 Modelling the percentiles

Typical street cases

For PM_{10} , we have found a regression line with a small intercept. Physically, the curve should obviously go through the origin (0,0). We closely approximate the regression line found by neglecting the intercept:

 $[90.1 percentile] = 1.52 x [annual mean] for PM_{10}$.

In the dataset used, the error in the prediction of the measured 90.1 percentile by this expression has a relative standard deviation of 10%.

For NO₂ the intercept is more significant, but also here the curve should go through the origin. By excluding streets with low concentrations (annual mean < $30 \ \mu g/m^3$), which are not relevant for the SEC purposes, we can use the regression line as a simple approximation:

 $[99.8 \ percentile] = 2.0 \ x \ [mean] + 40 \ \mu g/m^3 \ for \ NO_2 \ (for \ [mean] > 30 \ \mu g/m^3).$

In the dataset used, the error in the prediction of the measured 99.8 percentile by this expression has relative standard deviation of 17%.

Unfavourable street cases

The above formulas are for calculating the percentiles of *typical cases* of streets types. For *unfavourable cases*, most of the variability between streets within a type may already been comprised in the assumed factor for the annual mean (2 for PM_{10} and 1.5 for NO₂), but one may argue that the variability between streets is in principle larger for the percentiles. However, the uncertainty in the factors for the annual mean concentrations is so large that we will also use the indicative factors for the annual means as indicator for the percentiles. Hence we will apply the relations between the percentile and the annual mean given above both for typical cases and unfavourable cases.

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Chapter 6: Recommendation on the treatment of the street scale in ETC's own IA methodology - current possibilities and future perspectives

6.1 Current possibilities in the existing context

In the developments of EU AQ legislation prior to CAFE, as well as projections of AQ across Europe accounting for existing and new policies and measures (EEA and DGEnv work), Integrated Assessment Modelling has been carried out with the RAINS model. The approach focuses on the regional scale concentrations in Europe, in line with the analyses needed for the CLTRAP, and dealt primarily with long-range transport and the impact on vegetation and ecosystems. However, air quality is still poor in numerous densely populated areas and population exposure is in some cases alarmingly high despite the adopted policies and measures. In addition, as health effect studies are continuously providing new evidence rendering air quality one of the most important parameters to the European citizen's well being, compliance with limit values is of prime importance. Exceedances of limit values are in their vast majority observed in urban areas and particularly hotspots, which should therefore be included in the assessment.

To support this need, the JRC has set up the City-Delta study, targeted at modelling the urban background levels in Europe in order to provide an urban module for use in IAM. In a further straightforward step, the hotspot levels can be modelled.

SEC proposes to make use of urban scale model results, either via the City-Delta methodology (see City-Delta final report) or any suitable urban scale AQ model, which will be driven by the regional scale model, in order to provide the urban background conditions for a street scale model and thus consider hotspots. This approach can be applied to the street/traffic configurations that have now been defined in the SEC project (see chapter 5). The approach allows for base year and scenario projections as the impact of particular policies and measures to be accounted for at the regional, urban and street scales providing information that can then be used to calculate population exposure.

The tools available to the ETC/ACC (urban and street scale models) are currently being applied and tested in this context and have led to encouraging results as they have been proved (at an acceptable level of accuracy) capable of reproducing the concentrations observed at street level.

For the immediate needs of the State-of-the-Environment 2005 report (according to the IP2004) the urban scale air quality model OFIS will be applied to the ensemble of the cities considered in the MERLIN project. These cities have been chosen, as MERLIN will supply the detailed emission inventories required by the urban scale model. The boundary

concentrations and meteorological data required by OFIS for base year and scenarios will be obtained from EMEP model results. Emission reduction factors (per sector) derived from the emission reductions calculated by RAINS (see Technical report on Scenario test run results for Climate Change and Air Pollution SoEOR2005 Part 1) will be applied to the urban emission inventories leading to air quality projections at city level. These model results will then be used by the street scale model, in conjunction with reasonable assumptions to account for the street emissions and emission changes per scenario.

6.2 Future needs and possibilities: the ultra fine particles

Information on PM_{10} and to a lesser extent on $PM_{2.5}$ levels has greatly improved following implementation of the Council Decision on Exchange of Information 97/101/EC and the First Daughter Directive. Compared with the PM_{10} limit values of the First Daughter Directive to be met in 2005 (Stage 1), PM_{10} concentrations in parts of Europe are rather high. According to the CAFE Second Position Paper on Particulate Matter²:

- Exceedances in PM_{10} concentrations are more frequent at traffic exposed and industrial sites than in the urban background.
- Similar is the situation for $PM_{2.5}$; there are indications that the additional burden of $PM_{2.5}$ at traffic exposed sites is comparable to the additional PM_{10} burden at the same sites.
- For the less "conventional metrics", it seems that traffic sites tend to show somewhat higher levels of $PM_{1,0}$ than urban background sites and considerably higher number concentrations of ultrafine particles. There is evidence that the number concentration of ultrafine particles varies much stronger spatially, with a range of an order of magnitude going from rural to hotspot levels (compare also Figures 6.1-6.3 and the references given in the figure legends).

It becomes obvious that in the near future the ultrafine particles should be included in the assessment and their hotspot levels modeled. Indeed, this task may be urgently needed, as scientific evidence on the adverse health effects of ultrafine particles grows.

So far the SEC modeling exercise for the local scale has only focused on PM_{10} and $PM_{2.5}$ approximated at that scale as inert. The exercise has so far shown that there is an underestimation of the concentrations, due to missing sources or to low estimates of the emissions.

In a second step, SEC should also focus on the ultrafine particles emitted from vehicles. It should be recalled that these particles comprise two families: the larger ones from the formation of soot during combustion process and the smaller ones (nanoparticles) from gas-to-particle conversion processes during dilution of exhaust gases. Control of dilution can influence the relative proportions of the two families of particles. By control of the fuel sulphur content it appears possible to suppress the formation of nanoparticles and to manipulate particle number emitted through vehicle design and fuel composition. This potential should be taken into account in number based hotspot models and should be tested against available and future databases.

² Final Draft, CAFE Working Group on Particulate ₂Matter, April 6th, 2004

To this aim, a future SEC activity focused on ultrafine particles could be based on and benefit from:

- Existing methods and codes that are being modified to deal with nanoparticle aerosols. In particular in the nanoparticle size range, collision and coagulation processes should be accounted for to determine the particle size distribution and chemical composition as a function of particle size. Moreover, the microphysical processes, such as nucleation of gas-phase species or coagulation of primary exhaust particles, are also attempted to be modeled on spatial scales as small as a few meters.
- The new version of COPERT (4) which is currently under preparation. This emission database will also include emission factors on nanoparticle number counts, size distributions (number and mass based) specific area and size resolved chemical composition of particles emitted by all types of vehicles.

Evidently such a modelling exercise will need to be thoroughly evaluated against sets of comprehensive measurements. There is considerable evidence that suitable measurements are being conducted currently at European scale and can be used for this evaluation.



Figure 6.1. PM number concentration decrease with distance for various particle size ranges. (Zhu et al., Atmospheric Environment, 2002).



Figure 6.2. Effect of ambient temperature on particle number concentration and decay rates (Zhu et al., Aerosol Science and Technology, 2004).



Figure 6.3. Black carbon concentration decrease with distance for two cases with different vehicle fleet compositions (Zhu et al., Atmospheric Environment, 2002).

ANNEX A

Table A.1. Monthly vehicle distribution in Hornsgatan, Stockholm.

| Type | Class | Legislation | Jan | Feb | Mar | Apr | May | Jun | Jul | Ang | Sen | Oct | Nov | Dec |
|--|------------------------------------|-------------------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| rype | Gasoline $< 1.4.1$ | PREECE | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0000 | 0 | 0 |
| | Gusonne «I, II | ECE 15/00 01 | Ő | 0 | 0 | 0 | Ő | Ő | ő | 0 | ő | 0 | 0 | 0 |
| | | ECE 15/02 | 378 | 353 | 409 | 368 | 425 | 368 | 312 | 388 | 398 | 392 | 395 | 374 |
| | | ECE 15/02 | 11424 | 10690 | 12276 | 11140 | 12952 | 11126 | 0442 | 11726 | 12027 | 11942 | 11059 | 11202 |
| | | ECE 15/05 | 28002 | 25407 | 41125 | 27025 | 42718 | 27012 | 21201 | 20007 | 20074 | 20262 | 20746 | 27564 |
| | | Improved Conventional | 38002 | 55497 | 41155 | 37023 | 42/18 | 37013 | 51561 | 39007 | 39974 | 39303 | 39740 | 37304 |
| | | On an Laser | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | | Euro L 01/441/EEC | 44030 | 41120 | 47660 | 42000 | 40405 | 42004 | 26250 | 45105 | 46215 | 45607 | 46050 | 42522 |
| | | Euro I - 91/441/EEC | 44030 | 41128 | 4/660 | 42898 | 49495 | 42884 | 30339 | 45195 | 46315 | 45607 | 46050 | 43522 |
| | | Euro II - 94/12/EC | 51382 | 47995 | 55018 | 50061 | 57759 | 50045 | 42430 | 52/41 | 54049 | 53223 | 53740 | 50790 |
| | G | Euro III - 98/69/EC Stage2000 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | 0 |
| | Gasoline 1,4 - 2,01 | PRE ECE | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | | ECE 15/00-01 | 511 | 477 | 552 | 409 | 574 | 108 | 422 | 524 | 527 | 520 | 524 | 505 |
| | | ECE 15/02 | 511 | 4// | 353 | 498 | 574 | 498 | 422 | 524 | 337 | 529 | 554 | 1505 |
| | | ECE 15/03 | 15450 | 14431 | 16/23 | 15052 | 1/36/ | 15047 | 12/58 | 15858 | 16251 | 16003 | 16158 | 152/1 |
| | | ECE 15/04 | 51349 | 47964 | 55582 | 50029 | 57721 | 50012 | 42402 | 52707 | 54014 | 53188 | 53705 | 50757 |
| | | Improved Conventional | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | | Open Loop | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 20 | | Euro I - 91/441/EEC | 59494 | 55572 | 64399 | 57965 | 66877 | 57946 | 49128 | 61067 | 62581 | 61625 | 62224 | 58808 |
| 3 | | Euro II - 94/12/EC | 69428 | 64851 | 75152 | 67643 | 78044 | 67621 | 57331 | 71264 | 73031 | 71915 | 72613 | 68627 |
| E . | | Euro III - 98/69/EC Stage2000 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| a de la compañía de | Gasoline >2,01 | PREECE | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| ž | | ECE 15/00-01 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| A. | | ECE 15/02 | 125 | 116 | 135 | 121 | 140 | 121 | 103 | 128 | 131 | 129 | 130 | 123 |
| | | ECE 15/03 | 3770 | 3522 | 4081 | 3673 | 4238 | 3672 | 3113 | 3870 | 3966 | 3905 | 3943 | 3727 |
| | | ECE 15/04 | 12532 | 11705 | 13565 | 12209 | 14087 | 12205 | 10348 | 12863 | 13182 | 12980 | 13107 | 12387 |
| | | Euro I - 91/441/EEC | 14519 | 13562 | 15716 | 14146 | 16321 | 14141 | 11990 | 14903 | 15273 | 15039 | 15186 | 14352 |
| | | Euro II - 94/12/EC | 16944 | 15827 | 18341 | 16508 | 19047 | 16503 | 13992 | 17392 | 17823 | 17551 | 17721 | 16748 |
| | 21 1 2 2 1 | Euro III - 98/69/EC Stage2000 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | Diesel <2,01 | Conventional | 4007 | 3742 | 4337 | 3904 | 4504 | 3902 | 3309 | 4113 | 4215 | 4150 | 4190 | 3960 |
| | | Euro I - 91/441/EEC | 2224 | 2077 | 2407 | 2166 | 2500 | 2166 | 1836 | 2282 | 2339 | 2303 | 2326 | 2198 |
| | | Euro II - 94/12/EC | 4448 | 4155 | 4815 | 4334 | 5000 | 4333 | 3673 | 4566 | 4679 | 4608 | 4652 | 4397 |
| | | Euro III - 98/69/EC Stage2000 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | Diesel >2,01 | Conventional | 2671 | 2495 | 2891 | 2602 | 3003 | 2602 | 2206 | 2742 | 2810 | 2767 | 2794 | 2640 |
| | | Euro I - 91/441/EEC | 1482 | 1385 | 1605 | 1444 | 1666 | 1444 | 1224 | 1522 | 1559 | 1535 | 1550 | 1465 |
| | | Euro II - 94/12/EC | 2966 | 2770 | 3210 | 2889 | 3334 | 2888 | 2449 | 3044 | 3119 | 3072 | 3102 | 2931 |
| | | Euro III - 98/69/EC Stage2000 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | LPG | Conventional | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | | Euro I - 91/441/EEC | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | | Euro II - 94/12/EC | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | | Euro III - 98/69/EC Stage2000 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | 2-Stroke | Conventional | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 89 | Gasoline <3,5t | Conventional | 15762 | 14723 | 17062 | 15357 | 17719 | 15352 | 13016 | 16179 | 16580 | 16327 | 16486 | 15581 |
| ick | | Euro I - 93/59/EEC | 1178 | 1101 | 1276 | 1148 | 1325 | 1148 | 973 | 1210 | 1240 | 1221 | 1232 | 1165 |
| /eh | | Euro II - 96/69/EC | 41 | 39 | 45 | 40 | 46 | 40 | 34 | 42 | 43 | 43 | 43 | 41 |
| Å | | Euro III - 98/69/EC Stage2000 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8 | Diesel <3,5 t | Conventional | 2718 | 2539 | 2942 | 2648 | 3055 | 2647 | 2244 | 2790 | 2859 | 2815 | 2843 | 2687 |
| 1 | | Euro I - 93/59/EEC | 2020 | 1887 | 2187 | 1968 | 2271 | 1968 | 1668 | 2074 | 2125 | 2093 | 2113 | 1997 |
| 3 | | Euro II - 96/69/EC | 6415 | 5992 | 6944 | 6250 | 7211 | 6248 | 5297 | 6585 | 6748 | 6645 | 6709 | 6341 |
| | | Euro III - 98/69/EC Stage2000 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | Gasoline >3,5 t | Conventional | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | Diesel 3,5 - 7,5 t | Conventional | 6203 | 6195 | 6066 | 5296 | 6806 | 6172 | 5810 | 7717 | 6453 | 6062 | 6041 | 5576 |
| | | Euro I - 91/542/EEC Stage I | 1441 | 1439 | 1409 | 1230 | 1581 | 1434 | 1350 | 1793 | 1499 | 1408 | 1403 | 1295 |
| | | Euro II - 91/542/EEC Stage II | 2063 | 2060 | 2017 | 1761 | 2264 | 2053 | 1932 | 2566 | 2146 | 2016 | 2009 | 1854 |
| | | Euro III - 2000 Standards | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| de | Diesel 7,5 - 16 t | Conventional | 6815 | 6807 | 6664 | 5818 | 7478 | 6782 | 6383 | 8478 | 7090 | 6661 | 6637 | 6127 |
| i i i i i i i i i i i i i i i i i i i | | Euro I - 91/542/EEC Stage I | 1583 | 1581 | 1548 | 1352 | 1737 | 1575 | 1483 | 1970 | 1647 | 1547 | 1542 | 1423 |
| 2 | | Euro II - 91/542/EEC Stage II | 2266 | 2264 | 2216 | 1935 | 2487 | 2255 | 2123 | 2820 | 2358 | 2215 | 2207 | 2037 |
| Ĩ | | Euro III - 2000 Standards | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| y I | Diesel 16 - 32 t | Conventional | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| E. | | Euro I - 91/542/EEC Stage I | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ξ | | Euro II - 91/542/EEC Stage II | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | | Euro III - 2000 Standards | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | Diesel >32t | Conventional | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | | Euro I - 91/542/EEC Stage I | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | | Euro II - 91/542/EEC Stage II | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | | Euro III - 2000 Standards | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | Urban Buses | Conventional | 3231 | 3227 | 3159 | 2758 | 3545 | 3215 | 3026 | 4019 | 3361 | 3157 | 3146 | 2904 |
| 8 | | Euro I - 91/542/EEC Stage I | 315 | 315 | 308 | 269 | 346 | 314 | 295 | 392 | 328 | 308 | 307 | 283 |
| ac | | Euro II - 91/542/EEC Stage II | 409 | 409 | 400 | 350 | 449 | 407 | 384 | 509 | 426 | 400 | 399 | 368 |
| ğ | | Euro III - 2000 Standards | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| si Si | Coaches | Conventional | 808 | 807 | 790 | 690 | 886 | 804 | 756 | 1005 | 840 | 789 | 787 | 726 |
| S. | | Euro I - 91/542/EEC Stage I | 79 | 79 | 77 | 67 | 86 | 78 | 74 | 98 | 82 | 77 | 77 | 71 |
| - | | Euro II - 91/542/EEC Stage II | 102 | 102 | 100 | 87 | 112 | 102 | 96 | 127 | 107 | 100 | 100 | 92 |
| | 50 2 | Euro III - 2000 Standards | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| l de | <50 cm ³ | Conventional | 11631 | 10864 | 12589 | 11332 | 13074 | 11328 | 9604 | 11938 | 12234 | 12047 | 12164 | 11496 |
| đ | | 97/24/EC Stage I | 1866 | 1743 | 2019 | 1818 | 2097 | 1817 | 1541 | 1915 | 1962 | 1932 | 1951 | 1844 |
| ~ | | 97/24/EC Stage II | 1895 | 1770 | 2051 | 1846 | 2130 | 1845 | 1565 | 1945 | 1993 | 1962 | 1982 | 1873 |
| | 2-stroke >50 cm ³ | Conventional | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 90 | 4 . 4 | 97/24/EC | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| g | 4-stroke <250 cm ³ | Conventional | 3211 | 2999 | 3475 | 3128 | 3609 | 3127 | 2651 | 3296 | 3377 | 3326 | 3358 | 3174 |
| E E | 4 | 97/24/EC | 1038 | 970 | 1124 | 1011 | 1167 | 1011 | 857 | 1065 | 1092 | 1075 | 1086 | 1026 |
| Ę. | 4-stroke 250 - 750 cm ³ | Conventional | 3211 | 2999 | 3475 | 3128 | 3609 | 3127 | 2651 | 3296 | 3377 | 3326 | 3358 | 3174 |
| N N | 4 | 97/24/EC | 1038 | 970 | 1124 | 1011 | 1167 | 1011 | 857 | 1065 | 1092 | 1075 | 1086 | 1026 |
| | 4-stroke >/50 cm ³ | Conventional | 3211 | 2999 | 5475 | 3128 | 3609 | 5127 | 2651 | 3296 | 3377 | 3326 | 3358 | 3174 |
| I | 1 | 97724/EC | 1038 | 970 | 1124 | 1011 | 1167 | 1011 | 857 | 1065 | 1092 | 1075 | 1086 | 1026 |

| Туре | Class | Legislation | 01:00 | 02:00 | 03:00 | 04:00 | 05:00 | 06:00 | 07:00 | 08:00 | 09:00 | 10:00 | 11:00 | 12:00 |
|-------|------------------------------------|----------------------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Tjpe | Gasoline <1.4 l | PRE ECE | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| | | ECE 15/00-01 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| | | ECE 15/02 | 0.5 | 0.5 | 0.4 | 0.3 | 0.2 | 0.3 | 0.7 | 1.3 | 1.4 | 1.2 | 1.4 | 1.5 |
| | | ECE 15/03 | 16.5 | 14.6 | 11.5 | 10.2 | 7.1 | 8.1 | 22.6 | 38.3 | 41.2 | 37.2 | 41.4 | 45.9 |
| | | ECE 15/04 | 54.9 | 48.6 | 38.4 | 34.0 | 23.7 | 26.9 | 75.1 | 127.3 | 136.9 | 123.7 | 137.5 | 152.4 |
| | | Improved Conventional | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| | | Open Loop | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| | | Euro I - 91/441/EEC | 63.7 | 56.3 | 44.4 | 39.4 | 27.4 | 31.2 | 87.0 | 147.4 | 158.6 | 143.3 | 159.3 | 176.6 |
| | | Euro II - 94/12/EC | 74.3 | 65.7 | 51.9 | 46.0 | 32.0 | 36.4 | 101.5 | 172.1 | 185.1 | 167.3 | 185.9 | 206.1 |
| | G F 14 201 | Euro III - 98/69/EC Stage2000 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| | Gasoline 1,4 - 2,01 | PRE ECE | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| | | ECE 15/00-01 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 1.0 | 1.7 | 1.8 | 1.7 | 1.8 | 2.0 |
| | | ECE 15/02 ECE 15/03 | 22.3 | 19.8 | 15.6 | 13.8 | 9.6 | 10.4 | 30.5 | 51.7 | 55.6 | 50.3 | 55.9 | 62.0 |
| | | ECE 15/04 | 74.2 | 65.7 | 51.8 | 46.0 | 32.0 | 36.3 | 101.4 | 172.0 | 184.9 | 167.2 | 185.8 | 206.0 |
| | | Improved Conventional | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| | | Open Loop | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| | | Euro I - 91/441/EEC | 86.0 | 76.1 | 60.0 | 53.3 | 37.0 | 42.1 | 117.5 | 199.2 | 214.3 | 193.7 | 215.3 | 238.7 |
| , A | | Euro II - 94/12/EC | 100.4 | 88.8 | 70.1 | 62.2 | 43.2 | 49.1 | 137.1 | 232.5 | 250.0 | 226.0 | 251.2 | 278.5 |
| E. | | Euro III - 98/69/EC Stage2000 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Bu a | Gasoline >2,0 l | PRE ECE | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| SSR | | ECE 15/00-01 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| 4 | | ECE 15/02 ECE 15/03 | 5.5 | 4.8 | 3.8 | 3.4 | 2.3 | 2.7 | 7.4 | 12.6 | 13.6 | 12.3 | 13.6 | 15.1 |
| | | ECE 15/04 | 18.1 | 16.0 | 12.6 | 11.2 | 7.8 | 8.9 | 24.8 | 42.0 | 45.1 | 40.8 | 45.3 | 50.3 |
| | | Euro I - 91/441/EEC | 21.0 | 18.6 | 14.7 | 13.0 | 9.0 | 10.3 | 28.7 | 48.6 | 52.3 | 47.3 | 52.5 | 58.2 |
| | | Euro II - 94/12/EC | 24.5 | 21.7 | 17.1 | 15.2 | 10.5 | 12.0 | 33.5 | 56.7 | 61.0 | 55.2 | 61.3 | 68.0 |
| | | Euro III - 98/69/EC Stage2000 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| | Diesel <2,01 | Conventional | 5.8 | 5.1 | 4.0 | 3.6 | 2.5 | 2.8 | 7.9 | 13.4 | 14.4 | 13.0 | 14.5 | 16.1 |
| | | Euro I - 91/441/EEC | 3.2 | 2.8 | 2.2 | 2.0 | 1.4 | 1.6 | 4.4 | 7.4 | 8.0 | 7.2 | 8.0 | 8.9 |
| | | Euro III - 94/12/EC | 6.4 | 5.7 | 4.5 | 4.0 | 2.8 | 3.1 | 8.8 | 14.9 | 16.0 | 14.5 | 16.1 | 17.8 |
| | Diesel >2.0.1 | Conventional | 3.0 | 3.4 | 2.0 | 24 | 1.7 | 1.0 | 5.2 | 0.0 | 9.6 | 8.7 | 0.0 | 10.7 |
| | Dieser > 2,0 1 | Euro I - 91/441/EEC | 2.1 | 19 | 1.5 | 13 | 0.9 | 1.9 | 2.9 | 5.0 | 5.3 | 4.8 | 5.4 | 5.9 |
| | | Euro II - 94/12/EC | 4.3 | 3.8 | 3.0 | 2.7 | 1.8 | 2.1 | 5.9 | 9.9 | 10.7 | 9.7 | 10.7 | 11.9 |
| | | Euro III - 98/69/EC Stage2000 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| | LPG | Conventional | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| | | Euro I - 91/441/EEC | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| | | Euro II - 94/12/EC | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| | 2-Stroke | Conventional | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| | Gasoline <3,5t | Conventional | 22.8 | 20.2 | 15.9 | 14.1 | 9.8 | 11.2 | 31.1 | 52.8 | 56.8 | 51.3 | 57.0 | 63.2 |
| cle | | Euro I - 93/59/EEC | 1.7 | 1.5 | 1.2 | 1.1 | 0.7 | 0.8 | 2.3 | 3.9 | 4.2 | 3.8 | 4.3 | 4.7 |
| /ehi | | Euro II - 96/69/EC | 0.1 | 0.1 | 0.0 | 0.0 | 0.0 | 0.0 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.2 |
| Γ. | D: 1.25. | Euro III - 98/69/EC Stage2000 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Ā | Diesel <3,5 t | Conventional Euro L 93/59/EEC | 3.9 | 3.5 | 2.7 | 2.4 | 1./ | 1.9 | 5.4 | 9.1 | 9.8 | 8.8 | 9.8 | 10.9 |
| - Fai | | Euro II - 96/69/EC | 9.3 | 8.2 | 6.5 | 5.7 | 4.0 | 4.5 | 12.7 | 21.5 | 23.1 | 20.9 | 23.2 | 25.7 |
| 9 | | Euro III - 98/69/EC Stage2000 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| | Gasoline >3,5 t | Conventional | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| | Diesel 3,5 - 7,5 t | Conventional | 6.1 | 8.0 | 7.4 | 6.8 | 6.0 | 6.4 | 12.7 | 21.5 | 24.3 | 23.6 | 25.5 | 27.0 |
| | | Euro I - 91/542/EEC Stage I | 1.4 | 1.9 | 1.7 | 1.6 | 1.4 | 1.5 | 2.9 | 5.0 | 5.6 | 5.5 | 5.9 | 6.3 |
| | | Euro II - 91/542/EEC Stage II | 2.0 | 2.7 | 2.5 | 2.3 | 2.0 | 2.1 | 4.2 | 7.1 | 8.1 | 7.8 | 8.5 | 9.0 |
| 89 | Diesel 7.5 - 16 t | Conventional | 6.7 | 8.8 | 8.1 | 7.5 | 6.6 | 7.0 | 13.9 | 23.6 | 26.7 | 25.9 | 28.0 | 29.7 |
| lic] | 5105017,5 101 | Euro I - 91/542/EEC Stage I | 1.6 | 2.1 | 1.9 | 1.7 | 1.5 | 1.6 | 3.2 | 5.5 | 6.2 | 6.0 | 6.5 | 6.9 |
| Ρ٩ | | Euro II - 91/542/EEC Stage II | 2.2 | 2.9 | 2.7 | 2.5 | 2.2 | 2.3 | 4.6 | 7.9 | 8.9 | 8.6 | 9.3 | 9.9 |
| τî. | | Euro III - 2000 Standards | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Ū, | Diesel 16 - 32 t | Conventional | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| E. | | Euro I - 91/542/EEC Stage I | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| æ | | Euro II - 91/542/EEC Stage II | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| | Diesel >32t | Conventional | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| | 1010301 > 521 | Euro I - 91/542/EEC Stage I | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| | | Euro II - 91/542/EEC Stage II | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| | | Euro III - 2000 Standards | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| | Urban Buses | Conventional | 3.2 | 4.2 | 3.8 | 3.6 | 3.1 | 3.3 | 6.6 | 11.2 | 12.6 | 12.3 | 13.3 | 14.1 |
| Jes | | Euro I - 91/542/EEC Stage I | 0.3 | 0.4 | 0.4 | 0.3 | 0.3 | 0.3 | 0.6 | 1.1 | 1.2 | 1.2 | 1.3 | 1.4 |
| oad | | Euro II - 91/542/EEC Stage II | 0.4 | 0.5 | 0.5 | 0.5 | 0.4 | 0.4 | 0.8 | 1.4 | 1.6 | 1.6 | 1.7 | 1.8 |
| 0 | Coaches | Conventional | 0.0 | 1.0 | 1.0 | 0.0 | 0.0 | 0.0 | 1.7 | 2.8 | 3.2 | 3.1 | 3.3 | 3.5 |
| SS | Coaches | Euro I - 91/542/EEC Stage I | 0.0 | 0.1 | 0.1 | 0.9 | 0.3 | 0.3 | 0.2 | 0.3 | 0.3 | 0.3 | 0.3 | 0.3 |
| Bu | | Euro II - 91/542/EEC Stage II | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.2 | 0.4 | 0.4 | 0.4 | 0.4 | 0.4 |
| | | Euro III - 2000 Standards | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| spa | <50 cm ³ | Conventional | 16.8 | 14.9 | 11.7 | 10.4 | 7.2 | 8.2 | 23.0 | 38.9 | 41.9 | 37.9 | 42.1 | 46.7 |
| do | | 97/24/EC Stage I | 2.7 | 2.4 | 1.9 | 1.7 | 1.2 | 1.3 | 3.7 | 6.2 | 6.7 | 6.1 | 6.8 | 7.5 |
| 4 | 2 stroke > 50 am3 | 9 //24/EC Stage II | 2.7 | 2.4 | 1.9 | 1.7 | 1.2 | 1.3 | 3.7 | 6.3 | 6.8 | 6.2 | 6.9 | 7.6 |
| | 2-500Ke >30 CIIP | 97/24/EC | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| 8 | 4-stroke <250 cm ³ | Conventional | 4.6 | 4.1 | 3.2 | 2.9 | 2.0 | 2.3 | 6.3 | 10.8 | 11.6 | 10.5 | 11.6 | 12.9 |
| cyd | | 97/24/EC | 1.5 | 1.3 | 1.0 | 0.9 | 0.6 | 0.7 | 2.1 | 3.5 | 3.7 | 3.4 | 3.8 | 4.2 |
| otor | 4-stroke 250 - 750 cm ³ | Conventional | 4.6 | 4.1 | 3.2 | 2.9 | 2.0 | 2.3 | 6.3 | 10.8 | 11.6 | 10.5 | 11.6 | 12.9 |
| M | 4 + 1 + 770 - 0 | 97/24/EC | 1.5 | 1.3 | 1.0 | 0.9 | 0.6 | 0.7 | 2.1 | 3.5 | 3.7 | 3.4 | 3.8 | 4.2 |
| | 4-stroke >750 cm ³ | Conventional | 4.6 | 4.1 | 3.2 | 2.9 | 2.0 | 2.3 | 6.3 | 10.8 | 11.6 | 10.5 | 11.6 | 12.9 |
| | | 21/24/EC | 1.3 | 1.5 | 1.0 | 0.9 | 0.0 | 0.7 | 2.1 | 3.3 | 3.7 | ٥.4 | 3.8 | 4.2 |

Table A.2. Hourly vehicle distribution in Hornsgatan, Stockholm, 01:00 – 12:00.

| | Table A.3. Hourly | vehicle | distribution | in Hornsgatan | , Stockholm | 13:00-2 | 24:00. |
|--|-------------------|---------|--------------|---------------|-------------|---------|--------|
|--|-------------------|---------|--------------|---------------|-------------|---------|--------|

| Туре | Class | Legislation | 13:00 | 14:00 | 15:00 | 16:00 | 17:00 | 18:00 | 19:00 | 20:00 | 21:00 | 22:00 | 23:00 | 00:00 |
|-------|------------------------------------|-------------------------------|-------|-------|-------|-------|-------|------------|-------|-------|-------|-------|-------|-------|
| | Gasoline <1,4 l | PRE ECE | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| | | ECE 15/00-01 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| | | ECE 15/02 | 1.7 | 1.7 | 1.8 | 1.9 | 1.9 | 1.8 | 1.5 | 1.3 | 1.1 | 1.0 | 0.8 | 0.7 |
| | | ECE 15/03 | 50.3 | 51.4 | 53.6 | 57.7 | 58.7 | 53.3 | 46.0 | 37.9 | 33.5 | 31.5 | 25.1 | 21.3 |
| | | ECE 15/04 | 167.0 | 171.0 | 178.1 | 191.8 | 195.2 | 177.1 | 153.0 | 126.1 | 111.5 | 104.7 | 83.3 | 70.7 |
| | | Improved Conventional | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| | | Open Loop | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| | | Euro I - 91/441/EEC | 193.5 | 198.1 | 206.3 | 222.3 | 226.2 | 205.2 | 177.3 | 146.1 | 129.2 | 121.4 | 96.5 | 81.9 |
| | | Euro II - 94/12/EC | 225.8 | 231.2 | 240.7 | 259.4 | 263.9 | 239.4 | 206.9 | 170.5 | 150.8 | 141.6 | 112.6 | 95.6 |
| | | Euro III - 98/69/EC Stage2000 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| | Gasoline 1,4 - 2,01 | PRE ECE | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| | | ECE 15/00-01 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| | | ECE 15/02 | 2.2 | 2.3 | 2.4 | 2.6 | 2.6 | 2.4 | 2.1 | 1.7 | 1.5 | 1.4 | 1.1 | 1.0 |
| | | ECE 15/03 | 67.9 | 69.5 | 72.4 | 78.0 | 79.4 | 72.0 | 62.2 | 51.3 | 45.3 | 42.6 | 33.8 | 28.7 |
| | | ECE 15/04 | 225.7 | 231.0 | 240.6 | 259.2 | 263.8 | 239.3 | 206.7 | 170.4 | 150.7 | 141.5 | 112.5 | 95.5 |
| | | Improved Conventional | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| | | Open Loop | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| | | Euro I - 91/441/EEC | 261.5 | 267.7 | 278.8 | 300.3 | 305.6 | 277.2 | 239.5 | 197.4 | 174.6 | 164.0 | 130.3 | 110.7 |
| , E | | Euro II - 94/12/EC | 305.1 | 312.4 | 325.3 | 350.5 | 356.6 | 323.5 | 279.5 | 230.4 | 203.7 | 191.4 | 152.1 | 129.2 |
| - C | | Euro III - 98/69/EC Stage2000 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| | Gasoline >2,0 l | PRE ECE | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| SSC . | | ECE 15/00-01 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Pa | | ECE 15/02 | 0.5 | 0.6 | 0.6 | 0.6 | 0.6 | 0.6 | 0.5 | 0.4 | 0.4 | 0.3 | 0.3 | 0.2 |
| 1 | | ECE 15/03 | 16.6 | 17.0 | 17.7 | 19.0 | 19.4 | 17.6 | 15.2 | 12.5 | 11.1 | 10.4 | 8.3 | 7.0 |
| 1 | | ECE 15/04 | 55.1 | 56.4 | 58.7 | 63.3 | 64.4 | 58.4 | 50.5 | 41.6 | 36.8 | 34.5 | 27.5 | 23.3 |
| 1 | | Euro I - 91/441/EEC | 63.8 | 65.3 | 68.0 | 73.3 | 74.6 | 67.7 | 58.5 | 48.2 | 42.6 | 40.0 | 31.8 | 27.0 |
| 1 | | Euro II - 94/12/EC | 74.5 | 76.2 | 79.4 | 85.5 | 87.0 | 79.0 | 68.2 | 56.2 | 49.7 | 46.7 | 37.1 | 31.5 |
| 1 | D: 1.261 | Euro III - 98/69/EC Stage2000 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| 1 | Diesel <2,01 | Conventional | 17.6 | 18.0 | 18.8 | 20.2 | 20.6 | 18.7 | 16.1 | 13.3 | 11.8 | 11.0 | 8.8 | 7.5 |
| 1 | | Euro I - 91/441/EEC | 9.8 | 10.0 | 10.4 | 11.2 | 11.4 | 10.4 | 9.0 | /.4 | 6.5 | 0.1 | 4.9 | 4.1 |
| 1 | | Euro III - 94/12/EC | 19.6 | 20.0 | 20.8 | 22.5 | 22.9 | 20.7 | 17.9 | 14.8 | 13.1 | 12.3 | 9.7 | 8.3 |
| 1 | Diesel >2.0.1 | Conventional | 11.7 | 12.0 | 12.5 | 12.5 | 12.7 | 12.4 | 10.0 | 0.0 | 7.0 | 7.4 | 0.0 | 5.0 |
| | Diesei >2,0 i | Euro I 91/441/EEC | 6.5 | 67 | 6.9 | 15.5 | 7.6 | 6.9 | 10.8 | 0.9 | /.0 | /.4 | 3.9 | 2.0 |
| | | Euro II 94/12/EC | 13.0 | 13.3 | 13.0 | 15.0 | 15.2 | 13.8 | 11.0 | 4.9 | 4.3 | 4.1 | 5.2 | 2.0 |
| | | Euro III - 98/69/EC Stage2000 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| | LPG | Conventional | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| | 2.0 | Euro I - 91/441/EEC | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| | | Euro II - 94/12/EC | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| | | Euro III - 98/69/EC Stage2000 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| | 2-Stroke | Conventional | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| | Gasoline <3,5t | Conventional | 69.3 | 70.9 | 73.9 | 79.6 | 81.0 | 73.5 | 63.5 | 52.3 | 46.3 | 43.4 | 34.5 | 29.3 |
| ee | | Euro I - 93/59/EEC | 5.2 | 5.3 | 5.5 | 5.9 | 6.1 | 5.5 | 4.7 | 3.9 | 3.5 | 3.2 | 2.6 | 2.2 |
| Ē | | Euro II - 96/69/EC | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 |
| 5 | | Euro III - 98/69/EC Stage2000 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Ā | Diesel <3,5 t | Conventional | 11.9 | 12.2 | 12.7 | 13.7 | 14.0 | 12.7 | 10.9 | 9.0 | 8.0 | 7.5 | 6.0 | 5.1 |
| E | | Euro I - 93/59/EEC | 8.9 | 9.1 | 9.5 | 10.2 | 10.4 | 9.4 | 8.1 | 6.7 | 5.9 | 5.6 | 4.4 | 3.8 |
| 3 | | Euro II - 96/69/EC | 28.2 | 28.9 | 30.1 | 32.4 | 33.0 | 29.9 | 25.8 | 21.3 | 18.8 | 17.7 | 14.1 | 11.9 |
| | | Euro III - 98/69/EC Stage2000 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| | Gasoline >3,5 t | Conventional | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| | Diesel 3,5 - 7,5 t | Conventional | 27.9 | 28.6 | 29.2 | 31.1 | 29.1 | 23.5 | 18.1 | 14.7 | 10.8 | 10.2 | 8.4 | 7.0 |
| | | Euro I - 91/542/EEC Stage I | 6.5 | 6.6 | 6.8 | 7.2 | 6.8 | 5.5 | 4.2 | 3.4 | 2.5 | 2.4 | 1.9 | 1.6 |
| 1 | | Euro II - 91/542/EEC Stage II | 9.3 | 9.5 | 9.7 | 10.4 | 9.7 | 7.8 | 6.0 | 4.9 | 3.6 | 3.4 | 2.8 | 2.3 |
| s | D: 175 16 | Euro III - 2000 Standards | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| ide | Diesei 7,5 - 16 t | Euro I 01/542/EEC Stars I | 30.7 | 31.4 | 52.1 | 54.2 | 52.0 | 25.8 | 19.8 | 10.1 | 11.9 | 11.2 | 9.2 | 1.7 |
| /eh | | Euro II 91/542/EEC Stage I | /.1 | 10.4 | /.4 | 11.4 | 10.4 | 6.U 0 2 | 4.0 | 5.1 | 2.8 | 2.0 | 2.1 | 1.8 |
| 1 | | Euro III 2000 Standarda | 10.2 | 10.4 | 10.7 | 11.4 | 10.0 | 8.0 | 0.0 | 5.4 | 4.0 | 3./ | 3.1 | 2.6 |
| Ā | Diesel 16 - 32 + | Conventional | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Ś. | 5.0001 10 - 52 t | Euro I - 91/542/EEC Stage I | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Hea | | Euro II - 91/542/EEC Stage I | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| 1 | | Euro III - 2000 Standards | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| | Diesel >32t | Conventional | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| 1 | | Euro I - 91/542/EEC Stage I | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| | | Euro II - 91/542/EEC Stage II | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| 1 | | Euro III - 2000 Standards | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| | Urban Buses | Conventional | 14.5 | 14.9 | 15.2 | 16.2 | 15.1 | 12.2 | 9.4 | 7.6 | 5.6 | 5.3 | 4.4 | 3.6 |
| 8 | | Euro I - 91/542/EEC Stage I | 1.4 | 1.5 | 1.5 | 1.6 | 1.5 | 1.2 | 0.9 | 0.7 | 0.6 | 0.5 | 0.4 | 0.4 |
| L L | | Euro II - 91/542/EEC Stage II | 1.8 | 1.9 | 1.9 | 2.1 | 1.9 | 1.6 | 1.2 | 1.0 | 0.7 | 0.7 | 0.6 | 0.5 |
| Ö | | Euro III - 2000 Standards | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \$2 | Coaches | Conventional | 3.6 | 3.7 | 3.8 | 4.1 | 3.8 | 3.1 | 2.4 | 1.9 | 1.4 | 1.3 | 1.1 | 0.9 |
| , TIS | | Euro I - 91/542/EEC Stage I | 0.4 | 0.4 | 0.4 | 0.4 | 0.4 | 0.3 | 0.2 | 0.2 | 0.1 | 0.1 | 0.1 | 0.1 |
| m | | Euro II - 91/542/EEC Stage II | 0.5 | 0.5 | 0.5 | 0.5 | 0.5 | 0.4 | 0.3 | 0.2 | 0.2 | 0.2 | 0.1 | 0.1 |
| L | | Euro III - 2000 Standards | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| eds | <50 cm ³ | Conventional | 51.1 | 52.3 | 54.5 | 58.7 | 59.7 | 54.2 | 46.8 | 38.6 | 34.1 | 32.1 | 25.5 | 21.6 |
| dol (| | 97/24/EC Stage I | 8.2 | 8.4 | 8.7 | 9.4 | 9.6 | 8.7 | 7.5 | 6.2 | 5.5 | 5.1 | 4.1 | 3.5 |
| 4 | 2 staslas 50 2 | 9 //24/EC Stage II | 8.3 | 8.5 | 8.9 | 9.6 | 9.7 | 8.8 | 7.6 | 6.3 | 5.6 | 5.2 | 4.2 | 3.5 |
| 1 | 2-stroke >50 cm ³ | Conventional | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| 89 | 4 steples <2503 | 7//24/EC | 0.0 | 14.4 | 0.0 | 16.2 | 0.0 | 15.0 | 12.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| yde | 4-stroke <250 cm ³ | 07/24/EC | 14.1 | 14.4 | 15.0 | 10.2 | 10.5 | 15.0 | 12.9 | 10.7 | 9.4 | 8.8 | 7.0 | 0.0 |
| OLC. | 4-stroke 250 - 750 cm ³ | Conventional | 4.0 | 4.7 | 4.9 | 16.2 | 16.5 | 4.0 | 12.9 | 10.7 | 9.0 | 2.9 | 2.3 | 6.0 |
| VI0t. | . 54.540 250 - 750 CHP | 97/24/EC | 4.1 | 47 | 49 | 5.2 | 53 | 4.8 | 4.2 | 34 | 3.4 | 29 | 23 | 1 9 |
| ~ | 4-stroke >750 cm ³ | Conventional | 14.0 | 14.7 | 15.0 | 16.2 | 16.5 | 15.0 | 12.9 | 10.7 | 9.4 | 2.9 | 7.0 | 6.0 |
| 1 | | 97/24/EC | 4.6 | 4.7 | 4.9 | 5.2 | 5.3 | 4.8 | 4.2 | 3.4 | 3.0 | 2.9 | 2.3 | 1.9 |

| Fable B.1. Monthly | vehicle distribution in | Marylebone Rd., London. |
|---------------------------|-------------------------|-------------------------|
|---------------------------|-------------------------|-------------------------|

| Type | Class | Legislation | Jan | Feb | Mar | Anr | May | Jun | Jul | Ang | Sen | Oct | Nov | Dec |
|----------|------------------------------------|-------------------------------|--------|-----------|-----------|--------|--------|------------|-----------|--------|--------------|--------|--------|--------------|
| Type | Gasoline < 1.4.1 | PREFCE | 0 | 0 | 0 | | 0 | Jun | Ju | Aug | 0 | 000 | 0 | 0 |
| | Gusonne (1,11 | ECE 15/00 01 | 250 | 258 | 275 | 258 | 275 | 263 | 276 | 260 | 257 | 256 | 256 | 250 |
| | | ECE 15/00-01 | 2109 | 2103 | 2241 | 2101 | 275 | 2142 | 2250 | 2102 | 2001 | 2000 | 2082 | 2108 |
| | | ECE 15/02 | 19596 | 19526 | 10752 | 19515 | 10721 | 10074 | 10921 | 102192 | 19422 | 19410 | 19252 | 10590 |
| | | ECE 15/03 | 18380 | 240911 | 19752 | 16515 | 19721 | 100/4 | 19651 | 19516 | 249409 | 249110 | 247220 | 18580 |
| | | ECE 13/04 | 230489 | 249811 | 200197 | 249330 | 203783 | 234308 | 207208 | 200550 | 248408 | 248110 | 247329 | 230409 |
| | | Open Loon | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | | Euro L 01/441/EEC | 102002 | 102470 | 205105 | 102267 | 204786 | 105000 | 205020 | 200500 | 101200 | 101169 | 100566 | 102040 |
| | | Euro II - 91/441/EEC | 206780 | 205715 | 421671 | 205270 | 421016 | 402024 | 403930 | 412408 | 202402 | 202020 | 201792 | 206662 |
| | | Euro III - 94/12/EC | 390789 | 393713 | 4210/1 | 393219 | 421010 | 402934 | 425508 | 412408 | 393492 | 393020 | 391/83 | 390002 |
| | Gradier 1.4, 2.01 | Euro III - 98/69/EC Stage2000 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | Gasoline 1,4 - 2,01 | PRE ECE | 262 | 262 | 270 | 262 | 270 | 267 | 201 | 272 | 201 | 200 | 200 | 262 |
| | | ECE 15/00-01 | 203 | 202 | 279 | 202 | 279 | 207 | 281 | 273 | 201 | 260 | 260 | 203 |
| | | ECE 15/02 | 2141 | 2130 | 2276 | 2133 | 2272 | 21/5 | 2285 | 2220 | 2124 | 2121 | 2114 | 2141 |
| | | ECE 15/03 | 18875 | 18822 | 20056 | 18801 | 20025 | 19165 | 20137 | 19616 | 18/16 | 18693 | 18035 | 18807 |
| | | ECE 15/04 | 254351 | 253003 | 270301 | 253384 | 209881 | 258290 | 2/1389 | 264364 | 252238 | 251935 | 251142 | 254270 |
| | | Improved Conventional | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | | Euro L 01/441/EEC | 105077 | 105447 | 208267 | 105222 | 207042 | 100012 | 200105 | 202602 | 104240 | 104116 | 102505 | 105014 |
| 2 | | Euro II - 91/441/EEC | 402007 | 193447 | 428172 | 193232 | 407507 | 400146 | 4209105 | 419767 | 200550 | 200080 | 207822 | 193914 |
| Ö | | Euro III 98/69/EC Stage2000 | 402907 | 401810 | 420175 | 401374 | 427507 | 409140 | 429890 | 418707 | 399559 | 399080 | 397823 | 402778 |
| 5 | Casalina > 2.0.1 | PDE ECE | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| E. | Gasonne >2,01 | ECE 15/00-01 | 48 | 48 | 52 | 48 | 51 | 49 | 52 | 50 | 48 | 48 | 48 | 48 |
| 1 | | ECE 15/02 | 395 | 394 | 420 | 393 | 419 | 401 | 421 | 410 | 392 | 391 | 390 | 395 |
| 4 | | ECE 15/03 | 3480 | 3470 | 3698 | 3467 | 3692 | 3534 | 3713 | 3617 | 3451 | 3447 | 3436 | 3479 |
| | | ECE 15/04 | 20539 | 20484 | 21827 | 20461 | 21793 | 20857 | 21915 | 21348 | 20369 | 20344 | 20280 | 20533 |
| 1 | | Euro I - 91/441/EEC | 62493 | 62324 | 66412 | 62255 | 66309 | 63461 | 66679 | 64953 | 61974 | 61899 | 61705 | 62473 |
| | | Euro II - 94/12/EC | 74289 | 74088 | 78947 | 74006 | 78825 | 75439 | 79265 | 77213 | 73671 | 73583 | 73351 | 74265 |
| 1 | | Euro III - 98/69/EC Stage2000 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | Diesel <2,01 | Conventional | 29464 | 29385 | 31312 | 29352 | 31263 | 29921 | 31438 | 30624 | 29220 | 29184 | 29093 | 29455 |
| | | Euro I - 91/441/EEC | 20950 | 20893 | 22263 | 20870 | 22229 | 21274 | 22353 | 21774 | 20776 | 20751 | 20685 | 20943 |
| | | Euro II - 94/12/EC | 43070 | 42954 | 45771 | 42906 | 45700 | 43737 | 45955 | 44766 | 42712 | 42661 | 42527 | 43057 |
| | | Euro III - 98/69/EC Stage2000 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | Diesel >2,01 | Conventional | 19643 | 19590 | 20875 | 19568 | 20842 | 19947 | 20959 | 20416 | 19480 | 19456 | 19395 | 19637 |
| | | Euro I - 91/441/EEC | 13966 | 13929 | 14842 | 13913 | 14819 | 14183 | 14902 | 14516 | 13850 | 13834 | 13790 | 13962 |
| | | Euro II - 94/12/EC | 28714 | 28636 | 30514 | 28604 | 30467 | 29158 | 30637 | 29844 | 28475 | 28441 | 28351 | 28704 |
| | | Euro III - 98/69/EC Stage2000 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | LPG | Conventional | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | | Euro I - 91/441/EEC | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | | Euro II - 94/12/EC | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | | Euro III - 98/69/EC Stage2000 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | 2-Stroke | Conventional | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8 | Gasoline <3,5t | Conventional | 44927 | 44805 | 47744 | 44756 | 47670 | 45623 | 47937 | 46696 | 44554 | 44500 | 44360 | 44913 |
| Į. | | Euro I - 93/59/EEC | 16809 | 16763 | 17863 | 16745 | 17835 | 17069 | 17934 | 17470 | 16669 | 16649 | 16596 | 16803 |
| Vel | | Euro II - 96/69/EC | 35489 | 35393 | 37715 | 35354 | 37656 | 36039 | 37867 | 36886 | 35194 | 35152 | 35041 | 35478 |
| Δ. | D: 1.25. | Euro III - 98/69/EC Stage2000 | 0 | 105.11 | 12200 | 0 | 10100 | 41201 | 10074 | 10051 | 40212 | 102.65 | 10120 | 10,620 |
| ă | Diesel <3,5 t | Conventional | 40651 | 40541 | 43200 | 40496 | 43133 | 41281 | 43374 | 42251 | 40313 | 40265 | 40138 | 40638 |
| 톱 | | Euro I - 93/59/EEC | 15209 | 15168 | 24125 | 15151 | 16137 | 15444 | 16228 | 15807 | 15082 | 15064 | 15017 | 15204 |
| Ē | | Euro III - 90/09/EC | 52112 | 52025 | 54125 | 51969 | 34072 | 32009 | 34203 | 33370 | 51645 | 51807 | 51700 | 52101 |
| | Gasoline >3.5.t | Conventional | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | Diesel 35 - 75t | Conventional | 24181 | 25794 | 27376 | 23778 | 27428 | 26410 | 27182 | 26338 | 25947 | 26479 | 27228 | 23842 |
| | Dieser 5,5 - 7,5 t | Euro I - 91/542/EEC Stage I | 16201 | 17282 | 18342 | 15932 | 18377 | 17695 | 18212 | 17647 | 17385 | 17741 | 18243 | 15975 |
| | | Euro II - 91/542/EEC Stage II | 23214 | 24763 | 26281 | 22828 | 26331 | 25354 | 26096 | 25285 | 24909 | 25420 | 26140 | 22889 |
| 1 | | Euro III - 2000 Standards | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8 | Diesel 7.5 - 16 t | Conventional | 49944 | 53277 | 56544 | 49113 | 56651 | 54549 | 56144 | 54400 | 53592 | 54691 | 56239 | 49246 |
| bid | | Euro I - 91/542/EEC Stage I | 33463 | 35696 | 37885 | 32907 | 37957 | 36548 | 37617 | 36449 | 35907 | 36644 | 37681 | 32995 |
| PA | | Euro II - 91/542/EEC Stage II | 47947 | 51147 | 54283 | 47150 | 54386 | 52368 | 53899 | 52225 | 51449 | 52505 | 53991 | 47277 |
| πţ | | Euro III - 2000 Standards | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| đ | Diesel 16 - 32 t | Conventional | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Śve | | Euro I - 91/542/EEC Stage I | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ĥ | | Euro II - 91/542/EEC Stage II | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 1 | | Euro III - 2000 Standards | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | Diesel >32t | Conventional | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | | Euro I - 91/542/EEC Stage I | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | | Euro II - 91/542/EEC Stage II | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | | Euro III - 2000 Standards | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | Urban Buses | Conventional | 18072 | 19278 | 20460 | 17771 | 20499 | 19738 | 20315 | 19684 | 19392 | 19790 | 20350 | 17819 |
| pes pick | | Euro I - 91/542/EEC Stage I | 10709 | 11424 | 12124 | 10531 | 12148 | 11697 | 12039 | 11665 | 11492 | 11727 | 12059 | 10560 |
| Dec | | Euro II - 91/542/EEC Stage II | 13593 | 14500 | 15389 | 13367 | 15418 | 14846 | 15280 | 14806 | 14586 | 14885 | 15306 | 15403 |
| ġ | Caashaa | Euro III - 2000 Standards | 4510 | 4910 | 5117 | 0 | 5125 | 4025 | 5070 | 4022 | 4949 | 4047 | 5007 | 4455 |
| ŝ | Coacnes | Euro I 01/542/EEC Store I | 4518 | 4819 | 2021 | 4443 | 3027 | 4935 | 3019 | 4921 | 4848 | 494/ | 2015 | 4455 |
| Bu | | Euro II - 91/542/EEC Stage I | 20// | 2830 | 3031 | 2033 | 305/ | 2924 | 3820 | 2910 | 2813 3616 | 2932 | 3013 | ∠040 3251 |
| | | Euro III - 2000 Standarde | 0 | J025 0 | J047 0 | 0 | 0.000 | 5/12 | 3820 | 5701 | 0400 | 5721 | 5627 | 0 |
| * | <50 cm ³ | Conventional | 5450 | 5435 | 5792 | 5429 | 5783 | 5535 | 5815 | 5665 | 5405 | 5398 | 5381 | 5448 |
| bec | | 97/24/EC Stage I | 2383 | 2377 | 2533 | 2374 | 2529 | 2420 | 2543 | 2477 | 2363 | 2361 | 2353 | 2382 |
| 2 | | 97/24/EC Stage II | 2489 | 2482 | 2645 | 2480 | 2641 | 2528 | 2656 | 2587 | 2469 | 2466 | 2458 | 2488 |
| | 2-stroke >50 cm3 | Conventional | 2928 | 2920 | 3112 | 2917 | 3107 | 2973 | 3124 | 3043 | 2904 | 2900 | 2891 | 2927 |
| | | 97/24/EC | 2618 | 2611 | 2782 | 2608 | 2777 | 2658 | 2793 | 2721 | 2596 | 2593 | 2585 | 2617 |
| s | 4-stroke <250 cm ³ | Conventional | 6871 | 6852 | 7301 | 6844 | 7290 | 6977 | 7331 | 7141 | 6814 | 6805 | 6784 | 6868 |
| C.A.C | | 97/24/EC | 6142 | 6126 | 6527 | 6119 | 6517 | 6237 | 6554 | 6384 | 6091 | 6084 | 6065 | 6140 |
| tor | 4-stroke 250 - 750 cm ³ | Conventional | 6871 | 6852 | 7301 | 6844 | 7290 | 6977 | 7331 | 7141 | 6814 | 6805 | 6784 | 6868 |
| Ň | | 97/24/EC | 6142 | 6126 | 6527 | 6119 | 6517 | 6237 | 6554 | 6384 | 6091 | 6084 | 6065 | 6140 |
| | 4-stroke >750 cm ³ | Conventional | 6871 | 6852 | 7301 | 6844 | 7290 | 6977 | 7331 | 7141 | 6814 | 6805 | 6784 | 6868 |
| | 1 | 97/24/EC | 6142 | 6126 | 6527 | 6119 | 6517 | 6237 | 6554 | 6384 | 6091 | 6084 | 6065 | 6140 |

| Table B.2. Hourly vehicle distribution in Marylebone Rd., London, 01:00 -12 | :00 |
|---|-----|
|---|-----|

| Type | Class | Logislation | 01.00 | 02:00 | 03.00 | 04:00 | 05:00 | 06:00 | 07.00 | 08.00 | 00.00 | 10.00 | 11.00 | 12.00 |
|------------|------------------------------------|-------------------------------|-------|-------|------------|-------|-------|------------|------------|-------|-------|-------|-------|-------|
| турс | Class Cosoline <1.4.1 | DDE ECE | 0.0 | 02:00 | 0.0 | 04:00 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 12:00 |
| | Gasonne <1,41 | FCE 15/00-01 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| | | ECE 15/02 | 1.7 | 1.4 | 1.2 | 1.1 | 1.6 | 2.6 | 3.2 | 3.3 | 3.3 | 3.4 | 3.5 | 3.6 |
| | | ECE 15/02 | 15.1 | 11.9 | 10.3 | 10.0 | 13.8 | 23.1 | 28.5 | 29.0 | 29.3 | 30.1 | 30.7 | 31.5 |
| | | ECE 15/04 | 203.1 | 160.5 | 139.5 | 134.9 | 186.3 | 310.9 | 384.4 | 391.4 | 394.9 | 405.5 | 413.5 | 424.1 |
| | | Improved Conventional | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| | | Open Loop | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| | | Euro I - 91/441/EEC | 156.5 | 123.7 | 107.5 | 103.9 | 143.5 | 239.5 | 296.2 | 301.6 | 304.3 | 312.4 | 318.6 | 326.7 |
| | | Euro II - 94/12/EC | 321.8 | 254.3 | 220.9 | 213.7 | 295.1 | 492.4 | 608.9 | 620.0 | 625.6 | 642.3 | 655.0 | 671.7 |
| | | Euro III - 98/69/EC Stage2000 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| | Gasoline 1,4 - 2,0 1 | PRE ECE | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| | | ECE 15/00-01 | 0.2 | 0.2 | 0.1 | 0.1 | 0.2 | 0.3 | 0.4 | 0.4 | 0.4 | 0.4 | 0.4 | 0.4 |
| | | ECE 15/02 | 1.7 | 1.4 | 1.2 | 1.2 | 1.6 | 2.7 | 3.3 | 3.3 | 3.4 | 3.5 | 3.5 | 3.6 |
| | | ECE 15/03 | 15.5 | 12.1 | 10.5 | 10.2 | 14.0 | 25.4 | 29.0 | 29.5 | 29.8 | 30.6 | 31.2 | 32.0 |
| | | ECE 15/04 | 200.5 | 165.0 | 141.0 | 137.0 | 189.2 | 313.7 | 390.5 | 397.4 | 401.0 | 411.7 | 419.5 | 430.0 |
| | | Open Loop | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| | | Euro I - 91/441/EEC | 158.9 | 125.6 | 109.1 | 105.5 | 145.7 | 243.2 | 300.8 | 306.2 | 309.0 | 317.2 | 323.5 | 331.8 |
| SIR | | Euro II - 94/12/EC | 326.8 | 258.2 | 224.3 | 217.0 | 299.6 | 500.0 | 618.3 | 629.6 | 635.2 | 652.2 | 665.1 | 682.1 |
| ğ | | Euro III - 98/69/EC Stage2000 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| age age | Gasoline >2,01 | PRE ECE | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| SSCI | | ECE 15/00-01 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 |
| Pa | | ECE 15/02 | 0.3 | 0.3 | 0.2 | 0.2 | 0.3 | 0.5 | 0.6 | 0.6 | 0.6 | 0.6 | 0.7 | 0.7 |
| | | ECE 15/03 | 2.8 | 2.2 | 1.9 | 1.9 | 2.6 | 4.3 | 5.3 | 5.4 | 5.5 | 5.6 | 5.7 | 5.9 |
| | | ECE 15/04 | 16.7 | 13.2 | 11.4 | 11.1 | 15.3 | 25.5 | 31.5 | 32.1 | 32.4 | 33.2 | 33.9 | 34.8 |
| | | Euro I - 91/441/EEC | 50.7 | 40.0 | 34.8 | 33.7 | 46.5 | 77.6 | 95.9 | 97.6 | 98.5 | 101.2 | 103.2 | 105.8 |
| | | Euro II - 94/12/EC | 60.2 | 47.6 | 41.4 | 40.0 | 55.2 | 92.2 | 114.0 | 116.1 | 117.1 | 120.5 | 122.6 | 125.8 |
| | Discal <2.01 | Conventional | 23.9 | 18.9 | 16.4 | 15.9 | 21.9 | 36.6 | 45.2 | 46.0 | 46.5 | 47.7 | 48.6 | 49.9 |
| | Diesei <2,01 | Euro I - 91/441/EEC | 17.0 | 13.4 | 11.7 | 11.3 | 15.6 | 26.0 | 32.2 | 32.7 | 33.0 | 33.9 | 34.6 | 35.5 |
| | | Euro II - 94/12/EC | 34.9 | 27.6 | 24.0 | 23.2 | 32.0 | 53.5 | 66.1 | 67.3 | 67.9 | 69.7 | 71.1 | 72.9 |
| | | Euro III - 98/69/EC Stage2000 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| | Diesel >2,01 | Conventional | 15.9 | 12.6 | 10.9 | 10.6 | 14.6 | 24.4 | 30.1 | 30.7 | 31.0 | 31.8 | 32.4 | 33.3 |
| | | Euro I - 91/441/EEC | 11.3 | 9.0 | 7.8 | 7.5 | 10.4 | 17.3 | 21.4 | 21.8 | 22.0 | 22.6 | 23.1 | 23.6 |
| | | Euro II - 94/12/EC | 23.3 | 18.4 | 16.0 | 15.5 | 21.4 | 35.6 | 44.1 | 44.9 | 45.3 | 46.5 | 47.4 | 48.6 |
| | | Euro III - 98/69/EC Stage2000 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| | LPG | Conventional | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| | | Euro I - 91/441/EEC | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| | | Euro II - 94/12/EC | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| | 2 Stuales | Euro III - 98/69/EC Stage2000 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| | 2-Stroke Cosoline <3.5t | Conventional | 36.4 | 28.8 | 25.0 | 24.2 | 33.4 | 55.8 | 68.9 | 70.2 | 70.8 | 72.7 | 74.2 | 76.1 |
| Sec | Gasonne <5,51 | Euro I - 93/59/EEC | 13.6 | 10.8 | 9.4 | 9.1 | 12.5 | 20.9 | 25.8 | 26.3 | 26.5 | 27.2 | 27.7 | 28.5 |
| ehic | | Euro II - 96/69/EC | 28.8 | 22.7 | 19.8 | 19.1 | 26.4 | 44.0 | 54.5 | 55.5 | 56.0 | 57.5 | 58.6 | 60.1 |
| y v | | Euro III - 98/69/EC Stage2000 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| 2 | Diesel <3,5 t | Conventional | 33.0 | 26.1 | 22.6 | 21.9 | 30.2 | 50.5 | 62.4 | 63.5 | 64.1 | 65.8 | 67.1 | 68.8 |
| Ę. | | Euro I - 93/59/EEC | 12.3 | 9.7 | 8.5 | 8.2 | 11.3 | 18.9 | 23.3 | 23.8 | 24.0 | 24.6 | 25.1 | 25.7 |
| цi | | Euro II - 96/69/EC | 26.0 | 20.6 | 17.9 | 17.3 | 23.9 | 39.9 | 49.3 | 50.2 | 50.6 | 52.0 | 53.0 | 54.4 |
| | C | Euro III - 98/69/EC Stage2000 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| | Gasonne $>3,5$ t | Conventional | 10.0 | 10.7 | 11.9 | 15.3 | 26.1 | 44.6 | 55.0 | 56.7 | 57.2 | 60.4 | 60.9 | 59.3 |
| | Dieser 5,5 - 7,5 t | Euro I - 91/542/EEC Stage I | 7.3 | 7.2 | 8.0 | 10.2 | 17.5 | 29.9 | 36.8 | 38.0 | 38.4 | 40.4 | 40.8 | 39.5 |
| | | Euro II - 91/542/EEC Stage II | 10.4 | 10.3 | 11.4 | 14.7 | 25.1 | 42.8 | 52.8 | 54.4 | 55.0 | 58.0 | 58.4 | 56.9 |
| | | Euro III - 2000 Standards | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| 8 | Diesel 7,5 - 16 t | Conventional | 22.4 | 22.1 | 24.5 | 31.6 | 54.0 | 92.2 | 113.6 | 117.1 | 118.2 | 124.7 | 125.7 | 122.5 |
| hic | | Euro I - 91/542/EEC Stage I | 15.0 | 14.8 | 16.4 | 21.1 | 36.2 | 61.8 | 76.1 | 78.4 | 79.2 | 83.5 | 84.2 | 82.1 |
| 3V. | | Euro II - 91/542/EEC Stage II | 21.5 | 21.2 | 23.5 | 30.3 | 51.8 | 88.5 | 109.1 | 112.4 | 113.5 | 119.7 | 120.7 | 117.6 |
| fi a | | Euro III - 2000 Standards | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| уĽ | Diesel 16 - 32 t | Conventional | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| C. | | Euro I - 91/542/EEC Stage I | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| н | | Euro II - 91/542/EEC Stage II | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| | Discal >22t | Euro III - 2000 Standards | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| | Diesei >52t | Euro I - 91/542/EEC Stage I | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| | | Euro II - 91/542/EEC Stage II | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| | | Euro III - 2000 Standards | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| | Urban Buses | Conventional | 8.1 | 8.0 | 8.9 | 11.4 | 19.5 | 33.4 | 41.1 | 42.4 | 42.8 | 45.1 | 45.5 | 44.3 |
| 8 | | Euro I - 91/542/EEC Stage I | 4.8 | 4.7 | 5.3 | 6.8 | 11.6 | 19.8 | 24.4 | 25.1 | 25.4 | 26.7 | 27.0 | 26.3 |
| ach | | Euro II - 91/542/EEC Stage II | 6.1 | 6.0 | 6.7 | 8.6 | 14.7 | 25.1 | 30.9 | 31.9 | 32.2 | 33.9 | 34.2 | 33.3 |
| පී | | Euro III - 2000 Standards | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| ģ | Coaches | Conventional | 2.0 | 2.0 | 2.2 | 2.9 | 4.9 | 8.3 | 10.3 | 10.6 | 10.7 | 11.3 | 11.4 | 11.1 |
| Bus | | Euro I - 91/542/EEC Stage I | 1.2 | 1.2 | 1.3 | 1.7 | 2.9 | 4.9 | 6.1 | 6.3 | 6.3 | 6.7 | 6.7 | 6.6 |
| - | | Euro II - 91/542/EEC Stage II | 1.5 | 1.5 | 1.7 | 2.1 | 3.7 | 6.3 | 7.7 | 8.0 | 8.0 | 8.5 | 8.6 | 8.3 |
| s | <50 cm ³ | Euro III - 2000 Standards | 0.0 | 3.5 | 0.0 | 2.0 | 0.0 | 6.8 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| ped | <50 cm* | 97/24/EC Stage I | 4.4 | 1.5 | 1.3 | 2.9 | 4.1 | 3.0 | 0.4 3.7 | 3.7 | 3.0 | 3.0 | 3.0 | 9.2 |
| P. | | 97/24/EC Stage II | 2.0 | 1.6 | 1.4 | 1.3 | 1.9 | 3.1 | 3.8 | 3.9 | 3.9 | 4.0 | 4.1 | 4.2 |
| | 2-stroke >50 cm ³ | Conventional | 2.4 | 1.9 | 1.6 | 1.6 | 2.2 | 3.6 | 4.5 | 4.6 | 4.6 | 4.7 | 4.8 | 5.0 |
| | | 97/24/EC | 2.1 | 1.7 | 1.5 | 1.4 | 1.9 | 3.2 | 4.0 | 4.1 | 4.1 | 4.2 | 4.3 | 4.4 |
| S | 4-stroke <250 cm ³ | Conventional | 5.6 | 4.4 | 3.8 | 3.7 | 5.1 | 8.5 | 10.5 | 10.7 | 10.8 | 11.1 | 11.3 | 11.6 |
| 5 | | 97/24/EC | 5.0 | 3.9 | 3.4 | 3.3 | 4.6 | 7.6 | 9.4 | 9.6 | 9.7 | 9.9 | 10.1 | 10.4 |
| oto | 4-stroke 250 - 750 cm ³ | Conventional | 5.6 | 4.4 | 3.8 | 3.7 | 5.1 | 8.5 | 10.5 | 10.7 | 10.8 | 11.1 | 11.3 | 11.6 |
| Z | | 97/24/EC | 5.0 | 3.9 | 3.4 | 3.3 | 4.6 | 7.6 | 9.4 | 9.6 | 9.7 | 9.9 | 10.1 | 10.4 |
| | 4-stroke >750 cm ² | 97/24/EC | 5.0 | 4.4 | 5.8 3.4 | 3.7 | 5.1 | 8.5 7.6 | 9.4 | 9.6 | 9.7 | 9.9 | 10.1 | 11.6 |

| Туре | Class | Legislation | 13:00 | 14:00 | 15:00 | 16:00 | 17:00 | 18:00 | 19:00 | 20:00 | 21:00 | 22:00 | 23:00 | 00:00 |
|------|-------------------------------|--------------------------------|-------------|-------|------------|------------|--------|-------|------------|-------|-------|-------------|-------|------------|
| | Gasoline <1.4 l | PRE ECE | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| | | ECE 15/00-01 | 0.4 | 0.4 | 0.5 | 0.5 | 0.5 | 0.5 | 0.5 | 0.4 | 0.4 | 0.4 | 0.3 | 0.3 |
| | | ECE 15/02 | 3.6 | 3.7 | 3.7 | 3.8 | 3.9 | 4.0 | 3.7 | 3.3 | 3.1 | 3.0 | 2.8 | 2.3 |
| | | ECE 15/02 | 32.0 | 32.2 | 32.6 | 33.4 | 34.4 | 35.0 | 32.5 | 28.0 | 27.0 | 26.2 | 25.0 | 10.0 |
| | | ECE 15/04 | 431.3 | 434.1 | 439.4 | 449.9 | 463.2 | 472.2 | 438.3 | 390.1 | 363.3 | 353.3 | 336.4 | 268.8 |
| | | Improved Conventional | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 200.0 |
| | | Open Loop | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| | | Euro L - 91/4/1/EEC | 332.3 | 334.4 | 338.6 | 346.6 | 356.9 | 363.8 | 337.7 | 300.5 | 270.0 | 272.2 | 259.2 | 207.1 |
| | | Euro II 04/12/EC | 692.2 | 697.6 | 606.1 | 712.6 | 722.9 | 748.0 | 604.4 | 617.0 | 575.5 | 550.6 | 532.8 | 425.8 |
| | | Euro III 08/60/EC Stage2000 | 085.5 | 087.0 | 090.1 | /12.0 | / 33.8 | 748.0 | 094.4 | 017.9 | 0.0 | 0.0 | 0.0 | 425.8 |
| | Gasolino 1.4 2.01 | PPE ECE | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| | Gasolille 1,4 - 2,0 I | FRE ECE | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| | | ECE 15/00-01 | 0.3 | 2.7 | 2.0 | 0.5 | 0.5 | 0.5 | 0.5 | 2.2 | 2.1 | 2.0 | 2.0 | 0.5 |
| | | ECE 15/02 | 22.5 | 20.7 | 22.1 | 22.0 | 4.0 | 4.0 | 22.0 | 3.5 | 27.4 | 3.0 | 2.9 | 2.5 |
| | | ECE 15/03 | 32.5 | 32.7 | 33.1 | 33.9 | 34.9 | 35.0 | 33.0 | 29.4 | 27.4 | 20.0 | 25.5 | 20.3 |
| | | ECE 15/04 | 438.0 | 440.8 | 446.2 | 456.8 | 470.4 | 479.5 | 445.1 | 396.1 | 368.9 | 358.7 | 341.0 | 273.0 |
| | | Improved Conventional | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| | | Open Loop | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| 2 | | Euro I - 91/441/EEC | 337.5 | 339.6 | 343.8 | 352.0 | 362.4 | 369.5 | 343.0 | 305.2 | 284.2 | 276.4 | 263.2 | 210.3 |
| 3 | | Euro II - 94/12/EC | 693.8 | 698.2 | 706.8 | 723.6 | /45.1 | /59.6 | 705.1 | 627.4 | 584.3 | 568.3 | 541.1 | 432.4 |
| 5 | | Euro III - 98/69/EC Stage2000 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| gu | Gasoline >2,0 I | PRE ECE | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| S | | ECE 15/00-01 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 |
| 4 | | ECE 15/02 | 0.7 | 0.7 | 0.7 | 0.7 | 0.7 | 0.7 | 0.7 | 0.0 | 0.0 | 0.0 | 0.5 | 0.4 |
| | | ECE 15/03 | 6.0 | 6.0 | 0.1 | 6.2 | 0.4 | 0.0 | 0.1 | 5.4 | 5.0 | 4.9 | 4.7 | 3.7 |
| | | ECE 15/04 | 35.4 | 35.6 | 36.0 | 36.9 | 38.0 | 38.7 | 55.9 | 32.0 | 29.8 | 29.0 | 27.6 | 22.0 |
| | | Euro I - 91/441/EEC | 107.6 | 108.5 | 109.6 | 112.2 | 115.6 | 117.8 | 109.4 | 97.5 | 90.6 | 88.1 | 83.9 | 67.1 |
| | | Euro II - 94/12/EC | 127.9 | 128.7 | 130.3 | 155.4 | 157.4 | 140.0 | 150.0 | 115.7 | 107.7 | 104.8 | 99.8 | /9.7 |
| | D:1 -2.01 | Euro III - 98/09/EC Stage2000 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| | Diesel <2,01 | Conventional | 50.7 | 51.1 | 51.7 | 52.9 | 54.5 | 55.5 | 51.6 | 45.9 | 42.7 | 41.6 | 39.6 | 31.6 |
| | | Euro I - 91/441/EEC | 36.1 | 36.3 | 36.8 | 37.6 | 38.7 | 39.5 | 36.7 | 32.6 | 30.4 | 29.5 | 28.1 | 22.5 |
| | | Euro II - 94/12/EC | /4.2 | /4.6 | /5.6 | //.4 | /9./ | 81.2 | /5.4 | 07.1 | 62.5 | 60.7 | 57.8 | 46.2 |
| | D: 1 2 0 1 | Euro III - 98/69/EC Stage2000 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| | Diesel >2,01 | Conventional | 33.8 | 34.0 | 34.5 | 35.3 | 36.3 | 37.0 | 34.4 | 30.6 | 28.5 | 27.7 | 26.4 | 21.1 |
| | | Euro I - 91/441/EEC | 24.0 | 24.2 | 24.5 | 25.1 | 25.8 | 26.3 | 24.4 | 21.7 | 20.3 | 19.7 | 18.8 | 15.0 |
| | | Euro II - 94/12/EC | 49.4 | 49.8 | 50.4 | 51.6 | 53.1 | 54.1 | 50.2 | 44.7 | 41.6 | 40.5 | 38.6 | 30.8 |
| | | Euro III - 98/69/EC Stage2000 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| | LPG | Conventional | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| | | Euro I - 91/441/EEC | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| | | Euro II - 94/12/EC | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| | | Euro III - 98/69/EC Stage2000 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| | 2-Stroke | Conventional | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| 8 | Gasoline <3,5t | Conventional | 77.4 | 77.9 | 78.8 | 80.7 | 83.1 | 84.7 | 78.6 | 70.0 | 65.2 | 63.4 | 60.3 | 48.2 |
| ide | | Euro I - 93/59/EEC | 28.9 | 29.1 | 29.5 | 30.2 | 31.1 | 31.7 | 29.4 | 26.2 | 24.4 | 23.7 | 22.6 | 18.0 |
| Veh | | Euro II - 96/69/EC | 61.1 | 61.5 | 62.3 | 63.7 | 65.6 | 66.9 | 62.1 | 55.3 | 51.5 | 50.1 | 47.7 | 38.1 |
| È. | | Euro III - 98/69/EC Stage2000 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| ā | Diesel <3,5 t | Conventional | 70.0 | 70.4 | 71.3 | 73.0 | 75.2 | 76.6 | 71.1 | 63.3 | 59.0 | 57.3 | 54.6 | 43.6 |
| 퇷 | | Euro I - 93/59/EEC | 26.2 | 26.4 | 26.7 | 27.3 | 28.1 | 28.7 | 26.6 | 23.7 | 22.1 | 21.5 | 20.4 | 16.3 |
| Ť | | Euro II - 96/69/EC | 55.3 | 55.6 | 56.3 | 57.7 | 59.4 | 60.5 | 56.2 | 50.0 | 46.6 | 45.3 | 43.1 | 34.5 |
| | G 11 2 5 . | Euro III - 98/69/EC Stage2000 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| | Gasoline >3,5 t | Conventional | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| | Diesel 3,5 - 7,5 t | Conventional | 56.2 | 52.1 | 47.4 | 41.2 | 36.1 | 30.6 | 27.1 | 24.4 | 21.3 | 19.7 | 17.7 | 13.2 |
| | | Euro I - 91/542/EEC Stage I | 37.7 | 34.9 | 31.8 | 27.6 | 24.2 | 20.5 | 18.1 | 16.3 | 14.3 | 13.2 | 11.8 | 8.8 |
| | | Euro II - 91/542/EEC Stage II | 54.0 | 50.0 | 45.5 | 39.6 | 34.6 | 29.4 | 26.0 | 23.4 | 20.5 | 18.9 | 17.0 | 12.6 |
| × | D: | Euro III - 2000 Standards | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| icle | Diesel 7,5 - 16 t | Conventional | 116.1 | 107.6 | 97.9 | 85.2 | /4.5 | 63.2 | 55.9 | 50.4 | 44.1 | 40.7 | 36.5 | 27.2 |
| (ehi | | Euro I - 91/542/EEC Stage I | 77.8 | /2.1 | 65.6 | 57.1 | 49.9 | 42.3 | 57.4 | 33.8 | 29.5 | 27.3 | 24.5 | 18.2 |
| 5 | | Euro II - 91/542/EEC Stage II | 111.5 | 103.3 | 94.0 | 81.8 | /1.5 | 60.7 | 53.7 | 48.4 | 42.3 | 39.1 | 35.0 | 26.1 |
| P | Discal 16 22 : | Euro III - 2000 Standards | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Ń | Diesei 10 - 32 t | Error L 01/542/EEC Store L | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| G | | Euro I - 91/542/EEC Stage I | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Ĥ | | Euro III - 91/542/EEC Stage II | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| | D: | Euro III - 2000 Standards | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| | Diesel >32t | Conventional | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| | | Euro I - 91/342/EEC Stage I | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| | | Euro II - 91/542/EEC Stage II | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| - | Urban Busas | Conventional | 42.0 | 28.0 | 25.4 | 20.8 | 27.0 | 22.0 | 20.2 | 18.2 | 15.0 | 14.7 | 13.2 | 0.0 |
| | Orban Buses | Euro I 01/542/EEC Store I | 24.0 | 22.1 | 21.0 | 19.3 | 16.0 | 12.5 | 12.0 | 10.2 | 13.9 | 97 | 7.9 | 5.0 |
| he | | Euro II - 91/542/EEC Stage I | 31.6 | 20.3 | 21.0 | 23.2 | 20.3 | 17.2 | 15.2 | 13.7 | 12.0 | 11.1 | 0.0 | 5.8 7.4 |
| ğ | | Euro III - 2000 Standards | 0.0 | 29.5 | 20.0 | 0.0 | 20.5 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Ŷ | Conchas | Conventional | 10.5 | 0.0 | 8.0 | 77 | 6.7 | 5.7 | 5.1 | 4.6 | 4.0 | 2.7 | 2.2 | 2.5 |
| ŝ | coaches | Euro I - 91/5/2/EEC Stage I | 6.2 | 5.8 | 5.2 | 4.6 | 4.0 | 3.4 | 3.0 | 2.0 | 2.4 | 2.7 | 2.0 | 1.5 |
| ã | | Euro II - 91/542/EEC Stage II | 7.9 | 73 | 67 | 5.8 | 5.1 | 43 | 3.8 | 3.4 | 3.0 | 2.2 | 2.0 | 1.0 |
| | | Euro III - 2000 Standards | 0.0 | 7.5 | 0.7 | 0.0 | 0.0 | 4.5 | 0.0 | 0.0 | 0.0 | 2.8 | 2.5 | 0.0 |
| s | <50 cm ³ | Conventional | Q./ | 0.0 | 0.0 | 0.0 | 10.1 | 10.3 | 0.0 | 8.5 | 7.0 | 77 | 73 | 5 9 |
| bed | ~ | 97/24/EC Stage I | 7.4 // 1 | 2.4 | 2.0 4.2 | 7.0 | 10.1 | 10.5 | 7.J 1 7 | 37 | 2.5 | 3.1 | 2.5 | 2.0 |
| ٩ų. | | 97/24/FC Stage II | 4.1 | 4.1 | 4.2 | 4.5 | 4.4 | 4.5 | 4.2 | 30 | 3.5 | 3.4 | 3.2 | 2.0 |
| PH . | 2-stroke ≥50 cm ³ | Conventional | 4.5 | 4.5 | 5.1 | 4.3 | 5.4 | 5.5 | 5.1 | 1.5 | 4.2 | 3.J // 1 | 3.0 | 2.7 |
| | 2 500KC > 50 CHI | 97/24/EC | 4.5 | 45 | 2.1 | 2.3 4.7 | 4 8 | 49 | 4.6 | 4.0 | 3.8 | 37 | 3.9 | 2.1 |
| 8 | 4-stroke <250 cm ³ | Conventional | 11.9 | 11.0 | 12.1 | 12.2 | 12.7 | 13.0 | 12.0 | 10.7 | 10.0 | 0.7 | 0.2 | 2.8 |
| Ad | | 97/24/EC | 10.6 | 10.6 | 10.8 | 11.0 | 11.4 | 11.6 | 10.7 | 9.6 | 8.9 | 8.7 | 8.2 | 6.6 |
| ju j | 4-stroke 250 - 750 cm3 | Conventional | 11.8 | 11.9 | 12.1 | 12.3 | 12.7 | 13.0 | 12.0 | 10.7 | 10.0 | 9.7 | 9.2 | 7.4 |
| VIO | | 97/24/EC | 10.6 | 10.6 | 10.8 | 11.0 | 11.4 | 11.6 | 10.7 | 9.6 | 8.9 | 8.7 | 8.2 | 6.6 |
| 4 | 4-stroke >750 cm ³ | Conventional | 11.8 | 11.9 | 12.1 | 12.3 | 12.7 | 13.0 | 12.0 | 10.7 | 10.0 | 9.7 | 9.2 | 7.4 |
| | | 97/24/EC | 10.6 | 10.6 | 10.8 | 11.0 | 11.4 | 11.6 | 10.7 | 9.6 | 8.9 | 8.7 | 8.2 | 6.6 |

ANNEX C

Table C.1. Monthly vehicle distribution in Frankfurter Allee, Berlin.

| Туре | Class | Legislation | Jan | Feb | Mar | Apr | May | Jun | Jul | Aug | Sep | Oct | Nov | Dec |
|----------------|------------------------------------|-------------------------------|--------|--------|----------------|--------|--------|--------|----------------|---------------|--------|--------|--------|--------|
| | Gasoline <1,41 | PRE ECE | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | | ECE 15/00-01 | 2241 | 1934 | 1825 | 1917 | 2181 | 1934 | 1769 | 1834 | 2197 | 2257 | 2274 | 2136 |
| | | ECE 15/02 | 5529 | 4772 | 4502 | 4731 | 5381 | 4771 | 4366 | 4524 | 5420 | 5568 | 5611 | 5271 |
| | | ECE 15/03 | 19471 | 16808 | 15857 | 16662 | 18950 | 16802 | 15376 | 15933 | 19087 | 19610 | 19761 | 18564 |
| | | ECE 15/04 | 19917 | 17192 | 16220 | 17043 | 19384 | 17187 | 15728 | 16298 | 19524 | 20058 | 20214 | 18989 |
| | | Improved Conventional | 31936 | 27567 | 26008 | 27328 | 31082 | 27559 | 25219 | 26133 | 31307 | 32163 | 32412 | 30448 |
| | | Open Loop | 12306 | 10622 | 10021 | 10530 | 11977 | 10619 | 9718 | 10070 | 12063 | 12393 | 12489 | 11732 |
| | | Euro L - 91/441/EEC | 153999 | 132931 | 125411 | 131778 | 149879 | 132891 | 121610 | 126014 | 150963 | 155093 | 156293 | 146825 |
| | | Euro I = 91/441/EEC | 174090 | 151050 | 142505 | 140720 | 170200 | 151005 | 120105 | 142100 | 171520 | 135093 | 177506 | 140825 |
| | | Euro II - 94/12/EC | 1/4989 | 151050 | 142505 | 149/39 | 74719 | 151005 | 138185 | 143190 | 75259 | 176232 | 77016 | 72105 |
| | | Euro III - 98/69/EC Stage2000 | /6//2 | 66269 | 62520 | 65694 | /4/18 | 66249 | 60625 | 62821 | /5258 | //31/ | //916 | /3195 |
| | Gasoline 1,4 - 2,0 I | PRE ECE | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | | ECE 15/00-01 | 3028 | 2614 | 2466 | 2591 | 2947 | 2613 | 2391 | 2478 | 2968 | 3049 | 3073 | 2887 |
| | | ECE 15/02 | 7470 | 6448 | 6083 | 6392 | 7270 | 6446 | 5899 | 6113 | 7323 | 7523 | 7582 | 7122 |
| | | ECE 15/03 | 26310 | 22710 | 21426 | 22513 | 25606 | 22704 | 20776 | 21529 | 25791 | 26497 | 26702 | 25084 |
| | | ECE 15/04 | 30053 | 25942 | 24474 | 25717 | 29249 | 25934 | 23733 | 24592 | 29461 | 30267 | 30501 | 28653 |
| | | Improved Conventional | 13081 | 11291 | 10653 | 11193 | 12731 | 11288 | 10330 | 10704 | 12823 | 13174 | 13276 | 12472 |
| | | Open Loop | 5057 | 4365 | 4118 | 4327 | 4921 | 4364 | 3993 | 4138 | 4957 | 5093 | 5132 | 4821 |
| | | Euro I - 91/441/EEC | 246586 | 212852 | 200811 | 211004 | 239989 | 212788 | 194724 | 201776 | 241724 | 248337 | 250260 | 235098 |
| ars | | Euro II - 94/12/EC | 236447 | 204100 | 192554 | 202328 | 230121 | 204038 | 186717 | 193479 | 231785 | 238125 | 239969 | 225431 |
| Ö | | Euro III - 98/69/EC Stage2000 | 103735 | 89543 | 84478 | 88766 | 100959 | 89516 | 81917 | 84884 | 101689 | 104471 | 105280 | 98902 |
| 8 | Gasoline >2.01 | PREECE | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| sen | | ECE 15/00-01 | 739 | 638 | 602 | 632 | 719 | 638 | 584 | 605 | 724 | 744 | 750 | 704 |
| Se Se | | ECE 15/02 | 1823 | 1574 | 1485 | 1560 | 1774 | 1573 | 1440 | 1492 | 1787 | 1836 | 1850 | 1738 |
| - | | ECE 15/03 | 6421 | 5542 | 5229 | 5494 | 6249 | 5541 | 5070 | 5254 | 6294 | 6466 | 6516 | 6122 |
| 1 | | ECE 15/04 | 7155 | 6177 | 5827 | 6123 | 6964 | 6175 | 5651 | 5855 | 7014 | 7206 | 7262 | 6822 |
| | | Euro I - 91/441/EEC | 64784 | 55921 | 52758 | 55436 | 63051 | 55905 | 51159 | 53012 | 63507 | 65244 | 65749 | 61766 |
| 1 | | Euro II - 94/12/EC | 57704 | 49910 | 46002 | 49279 | 56161 | 49705 | 45569 | 47219 | 56567 | 58114 | 58564 | 55016 |
| 1 | | Euro III - 98/60/EC Stage2000 | 25216 | 21252 | 20617 | 21662 | 24620 | 21846 | 10002 | 20716 | 24917 | 25/06 | 25602 | 24127 |
| 1 | Diacal <2.0.1 | Conventional | 40456 | 24021 | 20017 | 2/4/10 | 20274 | 24011 | 31047 | 23104 | 20450 | 40742 | 41050 | 29571 |
| | LACSEI <2,0 I | Euro L 01/441/EEC | 40450 | 204921 | 32940 10427 | 20422 | 22220 | 20507 | 3194/ 18047 | 10520 | 22207 | 40743 | 41059 | 20755 |
| | | Euro II - 91/441/EEC | 2380/ | 42757 | 1943/ | 42277 | 40225 | 42744 | 1084/ | 41490 | 40500 | 2403/ | 24225 | 48220 |
| 1 | | Euro II - 94/12/EC | 50692 | 43/5/ | 41281 | 435// | 49335 | 43/44 | 40030 | 41480 | 49692 | 51051 | 5144/ | 48550 |
| | D: 1.00: | Euro III - 98/69/EC Stage2000 | 22939 | 19801 | 18680 | 19629 | 22325 | 19/95 | 18114 | 18770 | 22486 | 23102 | 23280 | 21870 |
| | Diesel >2,0 I | Conventional | 26971 | 23281 | 21964 | 23079 | 26249 | 23274 | 21298 | 22069 | 26439 | 27162 | 27372 | 25714 |
| | | Euro I - 91/441/EEC | 15912 | 13735 | 12958 | 13616 | 15486 | 13731 | 12565 | 13020 | 15598 | 16024 | 16149 | 15170 |
| | | Euro II - 94/12/EC | 33794 | 29171 | 27521 | 28918 | 32890 | 29162 | 26687 | 27653 | 33128 | 34034 | 34298 | 32220 |
| | | Euro III - 98/69/EC Stage2000 | 15293 | 13200 | 12454 | 13086 | 14883 | 13196 | 12076 | 12514 | 14991 | 15401 | 15520 | 14580 |
| | LPG | Conventional | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | | Euro I - 91/441/EEC | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | | Euro II - 94/12/EC | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | | Euro III - 98/69/EC Stage2000 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | 2-Stroke | Conventional | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | Gasoline <3,5t | Conventional | 7519 | 6490 | 6123 | 6434 | 7318 | 6488 | 5937 | 6152 | 7370 | 7572 | 7631 | 7168 |
| cle. | | Euro I - 93/59/EEC | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| ē | | Euro II - 96/69/EC | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ň | | Euro III - 98/69/EC Stage2000 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| ÷. | Diesel <3,5 t | Conventional | 28042 | 24205 | 22836 | 23995 | 27292 | 24198 | 22144 | 22946 | 27489 | 28241 | 28459 | 26735 |
| 1 | | Euro I - 93/59/EEC | 6205 | 5356 | 5053 | 5309 | 6039 | 5354 | 4900 | 5077 | 6082 | 6249 | 6297 | 5916 |
| -gi | | Euro II - 96/69/EC | 17428 | 15044 | 14193 | 14913 | 16962 | 15039 | 13762 | 14261 | 17084 | 17551 | 17687 | 16616 |
| Г | | Euro III - 98/69/EC Stage2000 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | Gasoline >3.5.t | Conventional | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | Diesel 3 5 - 7 5 t | Conventional | 24070 | 20777 | 19601 | 20596 | 23426 | 20771 | 19007 | 19696 | 23595 | 24241 | 24428 | 22948 |
| | 510501 5,5 7,5 0 | Euro L - 91/542/EEC Stage I | 5638 | 4867 | 4591 | 4825 | 5487 | 4865 | 4452 | 4614 | 5527 | 5678 | 5722 | 5375 |
| | | Euro II - 91/542/EEC Stage II | 9005 | 7773 | 7334 | 7706 | 8764 | 7771 | 7111 | 7369 | 8828 | 9069 | 0130 | 8586 |
| | | Euro III 2000 Stondordo | 1012 | 1650 | 1550 | 1627 | 1962 | 1651 | 1511 | 1566 | 1976 | 1027 | 1042 | 1924 |
| ŝ | Disc.175 164 | Euro III - 2000 Standards | 14270 | 1032 | 11/200 | 1037 | 12002 | 1031 | 11076 | 11604 | 12007 | 14200 | 1942 | 1024 |
| icle | Diesei 7,5 - 10 t | Euro L 01/542/EEC Store J | 142/9 | 12320 | 2724 | 2022 | 1389/ | 12322 | 2641 | 2727 | 1399/ | 14380 | 3205 | 13014 |
| /ehu | | Euro I - 91/542/EEC Stage I | 5345 | 288/ | 4251 | 2802 | 5255 | 2880 | 2041 | 4271 | 5219 | 5308 | 5395 | 5189 |
| 5 | | Euro II - 91/542/EEC Stage II | 5542 | 4611 | 4351 | 45/1 | 5199 | 4610 | 4219 | 45/1 | 5257 | 5380 | 5422 | 5093 |
| Į Ž | D: 116 DD | Euro III - 2000 Standards | 1135 | 980 | 924 | 971 | 1105 | 979 | 896 | 929 | 1113 | 1143 | 1152 | 1082 |
| y. | Diesel 16 - 32 t | Conventional | 10891 | 9401 | 8869 | 9319 | 10600 | 9398 | 8600 | 8912 | 10676 | 10968 | 11053 | 10384 |
| (Ga) | | Euro I - 91/542/EEC Stage I | 2551 | 2202 | 2078 | 2183 | 2483 | 2201 | 2015 | 2088 | 2501 | 2569 | 2589 | 2452 |
| Ħ | | Euro II - 91/542/EEC Stage II | 4075 | 3517 | 3318 | 3487 | 3966 | 3516 | 3218 | 3334 | 3994 | 4104 | 4135 | 3885 |
| | D: 1 00. | Euro III - 2000 Standards | 866 | 747 | 705 | 741 | 843 | 747 | 684 | 708 | 849 | 872 | 879 | 825 |
| | Diesel >32t | Conventional | 596 | 514 | 485 | 510 | 580 | 514 | 471 | 488 | 584 | 600 | 605 | 568 |
| | | Euro I - 91/542/EEC Stage I | 140 | 120 | 114 | 119 | 136 | 120 | 110 | 114 | 137 | 141 | 142 | 133 |
| | | Euro II - 91/542/EEC Stage II | 223 | 192 | 182 | 191 | 217 | 192 | 176 | 182 | 219 | 225 | 226 | 213 |
| | | Euro III - 2000 Standards | 47 | 41 | 39 | 41 | 46 | 41 | 37 | 39 | 46 | 48 | 48 | 45 |
| | Urban Buses | Conventional | 3190 | 2754 | 2598 | 2730 | 3105 | 2753 | 2519 | 2611 | 3128 | 3213 | 3238 | 3042 |
| 8 | | Euro I - 91/542/EEC Stage I | 584 | 504 | 475 | 499 | 568 | 504 | 461 | 478 | 572 | 588 | 592 | 556 |
| sch | | Euro II - 91/542/EEC Stage II | 580 | 500 | 472 | 496 | 564 | 500 | 458 | 474 | 568 | 584 | 588 | 553 |
| ð | | Euro III - 2000 Standards | 113 | 97 | 92 | 97 | 110 | 97 | 89 | 92 | 111 | 114 | 115 | 108 |
| s | Coaches | Conventional | 798 | 688 | 650 | 683 | 776 | 688 | 630 | 653 | 782 | 803 | 809 | 760 |
| ISC | | Euro I - 91/542/EEC Stage I | 146 | 126 | 119 | 125 | 142 | 126 | 115 | 119 | 143 | 147 | 148 | 139 |
| ā | | Euro II - 91/542/EEC Stage II | 145 | 125 | 118 | 124 | 141 | 125 | 114 | 119 | 142 | 146 | 147 | 138 |
| 1 | | Euro III - 2000 Standards | 28 | 24 | 23 | 24 | 27 | 24 | 22 | 23 | 28 | 28 | 29 | 27 |
| sb | <50 cm ³ | Conventional | 61714 | 53271 | 50258 | 52809 | 60063 | 53255 | 48734 | 50499 | 60497 | 62152 | 62633 | 58839 |
| ped | | 97/24/EC Stage I | 4618 | 3986 | 3761 | 3952 | 4495 | 3985 | 3647 | 3779 | 4527 | 4651 | 4687 | 4403 |
| ۲ ⁰ | | 97/24/EC Stage II | 253 | 219 | 206 | 217 | 247 | 219 | 200 | 207 | 248 | 255 | 257 | 241 |
| <u> </u> | 2-stroke >50 cm ³ | Conventional | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 1 | | 97/24/EC | 0 | 0 | 0 | õ | 0 | 0 | 0 | õ | 0 | 0 | 0 | 0 |
| S | 4-stroke <250 cm ³ | Conventional | 27946 | 24122 | 22758 | 23912 | 27198 | 24116 | 22068 | 22868 | 27395 | 28144 | 28362 | 26644 |
| yc | . 500kc <250 cm | 97/24/EC | 27940 | 1904 | 1796 | 1889 | 2147 | 1904 | 1742 | 1805 | 21595 | 20144 | 20302 | 2103 |
| orc | 4-stroke 250 - 750 cm ³ | Conventional | 27946 | 24122 | 22758 | 23012 | 27198 | 24116 | 22068 | 22868 | 27305 | 28144 | 28362 | 26644 |
| Ę. | . saoke 250 = 750 cm ^e | 97/24/EC | 27940 | 1004 | 1706 | 1999 | 21170 | 1004 | 1742 | 1905 | 21595 | 20144 | 20502 | 2102 |
| 4 | 4 stroke >750 am3 | Conventional | 2200 | 24122 | 22750 | 22012 | 214/ | 24116 | 22040 | 22020 | 2102 | 28144 | 24239 | 2103 |
| | 4-50 OKC > / 50 CM ² | 07/24/EC | 2/940 | 24125 | 22/38 | 23913 | 21198 | 24110 | 22008 | 22808 1905 | 21393 | 20144 | 20302 | 20044 |
| 1 | 1 | 71/24/EC | 2206 | 1904 | 1/90 | 1999 | 214/ | 1904 | 1/42 | 1803 | 2102 | 2222 | 2239 | 2103 |

| Туре | Class | Legislation | 1:00 | 2:00 | 3:00 | 4:00 | 5:00 | 6:00 | 7:00 | 8:00 | 9:00 | 10:00 | 11:00 | 12:00 |
|-------|------------------------------------|-------------------------------|-------|-------|-------|-------|-------|--------|--------|--------|--------|--------|--------|----------|
| | Gasoline <1,4 l | PRE ECE | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | | ECE 15/00-01 | 330 | 235 | 176 | 176 | 310 | 1009 | 1172 | 1266 | 1238 | 1300 | 1349 | 1369 |
| | | ECE 15/02 | 814 | 579 | 434 | 434 | 765 | 2490 | 2892 | 3125 | 3055 | 3208 | 3328 | 3377 |
| | | ECE 15/02 | 2866 | 2038 | 1527 | 1527 | 2694 | 8771 | 10184 | 11005 | 10760 | 11298 | 11723 | 11894 |
| | | ECE 15/04 | 2000 | 2085 | 1562 | 1562 | 2755 | 8972 | 10418 | 11257 | 11007 | 11557 | 11991 | 12166 |
| | | Improved Conventional | 4700 | 3343 | 2505 | 2505 | 4418 | 1/386 | 16704 | 18050 | 17640 | 18531 | 10227 | 10508 |
| | | Open Loop | 1811 | 1288 | 965 | 965 | 1702 | 5543 | 6437 | 6955 | 6800 | 7141 | 7409 | 7517 |
| | | Euro L 01/441/EEC | 22664 | 16122 | 12070 | 12070 | 21202 | 60272 | 80540 | 87040 | 95102 | 20250 | 02714 | 04069 |
| | | Euro II - 91/441/EEC | 22004 | 19210 | 12079 | 12079 | 21303 | 709372 | 01529 | 02002 | 06702 | 101520 | 92714 | 106990 |
| | | Euro III - 94/12/EC | 11208 | 2027 | 6022 | 6022 | 10620 | 24592 | 40155 | 42201 | 42426 | 101559 | 46220 | 100889 |
| | Casalina 1.4 2.0.1 | DRE ECE | 11298 | 8037 | 0022 | 0022 | 10020 | 34383 | 40133 | 45591 | 42420 | 44,546 | 40220 | 40895 |
| | Gasonne 1,4 - 2,0 1 | FRE ECE ECE 15/00.01 | 116 | 217 | 227 | 227 | 410 | 1264 | 1594 | 1711 | 1672 | 1757 | 1822 | 1840 |
| | | ECE 15/00-01 | 1000 | 782 | 596 | 596 | 1022 | 2265 | 2007 | 4222 | 4128 | 1737 | 1023 | 1649 |
| | | ECE 15/02 | 2072 | 2754 | 2064 | 2064 | 2640 | 11952 | 127(1 | 4222 | 4120 | 4555 | 15940 | 4505 |
| | | ECE 15/03 | 5872 | 2754 | 2064 | 2064 | 3640 | 11852 | 15701 | 14870 | 14539 | 15200 | 15840 | 100/1 |
| | | ECE 15/04 | 4425 | 3140 | 2557 | 2557 | 4157 | 13538 | 15/19 | 10980 | 10008 | 17439 | 18095 | 18558 |
| | | Improved Conventional | 1925 | 520 | 207 | 207 | 1810 | 2079 | 0842 | 1393 | 7229 | 7590 | 2014 | 2080 |
| | | | 744 | 329 | 10241 | 10242 | 24111 | 2278 | 2045 | 2858 | 2794 | 2954 | 5044 | 5089 |
| 2 | | Euro I - 91/441/EEC | 36289 | 25815 | 19341 | 19342 | 34111 | 1110/9 | 128977 | 139369 | 136268 | 143084 | 148455 | 150623 |
| E. | | Euro II - 94/12/EC | 34797 | 24753 | 18546 | 18546 | 32708 | 106511 | 123673 | 133639 | 130665 | 13/200 | 142350 | 144429 |
| er | G | Euro III - 98/69/EC Stage2000 | 15266 | 10860 | 8136 | 8137 | 14350 | 46729 | 54258 | 58630 | 57326 | 60193 | 62452 | 63364 |
| gu | Gasoline >2,01 | PRE ECE | 100 | 0 | 50 | 0 | 102 | 222 | 296 | 419 | 108 | 420 | 0 | 0 451 |
| SS | | ECE 15/00-01 | 109 | 101 | 142 | 142 | 102 | 333 | 380 | 410 | 408 | 429 | 1000 | 451 |
| Å. | | ECE 15/02 | 208 | 191 | 145 | 145 | 252 | 821 | 954 | 1050 | 2540 | 1058 | 1098 | 1114 |
| | | ECE 15/03 | 945 | 672 | 504 | 504 | 888 | 2892 | 5358 | 3629 | 5548 | 5726 | 3866 | 5922 |
| | | EUE 15/04 | 1053 | /49 | 561 | 561 | 990 | 3223 | 5/43 | 4044 | 3954 | 4152 | 4308 | 4371 |
| | | Euro I - 91/441/EEC | 9534 | 6/82 | 5081 | 5082 | 8962 | 29183 | 33885 | 30616 | 35801 | 37592 | 39003 | 39572 |
| | | Euro II - 94/12/EC | 8492 | 6041 | 4526 | 4526 | 7982 | 25994 | 50182 | 52614 | 51888 | 35485 | 54740 | 35248 |
| | Disculu (2.0.1 | Euro III - 98/69/EC Stage2000 | 5/26 | 2650 | 1986 | 1986 | 5502 | 11404 | 15242 | 14309 | 13990 | 14690 | 15241 | 15464 |
| | Diesei <2,01 | Conventional | 5954 | 4235 | 5173 | 5173 | 5596 | 18224 | 21160 | 22865 | 22357 | 25475 | 24356 | 24712 |
| | | Euro I - 91/441/EEC | 5512 | 2499 | 1872 | 1872 | 3302 | 10751 | 12484 | 15490 | 15189 | 15849 | 14369 | 14579 |
| | | Euro II - 94/12/EC | /460 | 5307 | 3976 | 3976 | 7012 | 22835 | 26514 | 28651 | 28013 | 29414 | 30518 | 50964 |
| | D: 1.001 | Euro III - 98/69/EC Stage2000 | 55/6 | 2401 | 1/99 | 1/99 | 5173 | 10333 | 11998 | 12965 | 12676 | 15310 | 15810 | 14012 |
| | Diesel >2,01 | Conventional | 3969 | 2824 | 2115 | 2116 | 3731 | 12149 | 14107 | 15244 | 14904 | 15650 | 16237 | 16475 |
| | | Euro I - 91/441/EEC | 2342 | 1666 | 1248 | 1248 | 2201 | 7168 | 8322 | 8993 | 8793 | 9233 | 9579 | 9719 |
| | | Euro II - 94/12/EC | 4973 | 3538 | 2651 | 2651 | 4675 | 15223 | 17676 | 19100 | 18675 | 19609 | 20346 | 20643 |
| | 1.00 | Euro III - 98/69/EC Stage2000 | 2251 | 1601 | 1199 | 1200 | 2115 | 6889 | 7999 | 8643 | 8451 | 8874 | 9207 | 9341 |
| | LPG | | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | | Euro I - 91/441/EEC | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | | Euro II - 94/12/EC | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | 2.6. 1 | Euro III - 98/69/EC Stage2000 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | 2-Stroke | Conventional | 1107 | 0 | 500 | 500 | 10.40 | 2207 | 2022 | 1250 | 1155 | 1262 | 1507 | 4502 |
| es | Gasonne < 5,5t | Error L 02/50/EEC | 1107 | /8/ | 590 | 590 | 1040 | 3387 | 3933 | 4250 | 4155 | 4365 | 4527 | 4595 |
| hic | | Euro II - 95/59/EEC | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ve | | Euro III - 90/09/EC | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| ЦĄ | Diacal <3.5 t | Conventional | 4127 | 2036 | 2100 | 2200 | 3870 | 12632 | 14667 | 158/0 | 15496 | 16271 | 16882 | 17120 |
| Ā | Diesei <5,5 t | Euro L 93/59/EEC | 4127 | 2930 | 487 | 487 | 2019 | 2705 | 3245 | 3507 | 3420 | 3600 | 3736 | 3790 |
| ght | | Euro II 06/60/EC | 2565 | 1824 | 1267 | 1267 | 2411 | 7951 | 0116 | 0850 | 0621 | 10112 | 10402 | 10645 |
| E | | Euro III 98/69/EC Stage2000 | 2303 | 1824 | 1307 | 1307 | 2411 | /851 | 9110 | 9650 | 9031 | 10113 | 10492 | 10045 |
| - | Gasoline >3.5 t | Conventional | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | Diesel 35 - 75 t | Conventional | 3542 | 2520 | 1888 | 1888 | 3330 | 10843 | 12590 | 13604 | 13301 | 13967 | 14491 | 14703 |
| | B10501 5,5 7,5 1 | Euro I - 91/542/EEC Stage I | 830 | 590 | 442 | 442 | 780 | 2540 | 2949 | 3187 | 3116 | 3272 | 3394 | 3444 |
| | | Euro II - 91/542/EEC Stage II | 1325 | 943 | 706 | 706 | 1246 | 4057 | 4710 | 5090 | 4976 | 5225 | 5422 | 5501 |
| | | Euro III - 2000 Standards | 282 | 200 | 150 | 150 | 265 | 862 | 1001 | 1081 | 1057 | 1110 | 1152 | 1169 |
| 8 | Diesel 7.5 - 16 t | Conventional | 2101 | 1495 | 1120 | 1120 | 1975 | 6432 | 7469 | 8070 | 7891 | 8285 | 8597 | 8722 |
| nicle | | Euro I - 91/542/EEC Stage I | 492 | 350 | 262 | 262 | 463 | 1507 | 1749 | 1890 | 1848 | 1941 | 2014 | 2043 |
| Vet | | Euro II - 91/542/EEC Stage II | 786 | 559 | 419 | 419 | 739 | 2406 | 2794 | 3019 | 2952 | 3100 | 3216 | 3263 |
| ty | | Euro III - 2000 Standards | 167 | 119 | 89 | 89 | 157 | 511 | 594 | 642 | 627 | 659 | 683 | 693 |
| ā | Diesel 16 - 32 t | Conventional | 1603 | 1140 | 854 | 854 | 1507 | 4906 | 5697 | 6156 | 6019 | 6320 | 6557 | 6653 |
| łvy | | Euro I - 91/542/EEC Stage I | 375 | 267 | 200 | 200 | 353 | 1149 | 1334 | 1442 | 1410 | 1480 | 1536 | 1558 |
| He | | Euro II - 91/542/EEC Stage II | 600 | 427 | 320 | 320 | 564 | 1836 | 2131 | 2303 | 2252 | 2364 | 2453 | 2489 |
| | | Euro III - 2000 Standards | 127 | 91 | 68 | 68 | 120 | 390 | 453 | 489 | 478 | 502 | 521 | 529 |
| | Diesel >32t | Conventional | 88 | 62 | 47 | 47 | 82 | 268 | 312 | 337 | 329 | 346 | 359 | 364 |
| | | Euro I - 91/542/EEC Stage I | 21 | 15 | 11 | 11 | 19 | 63 | 73 | 79 | 77 | 81 | 84 | 85 |
| | | Euro II - 91/542/EEC Stage II | 33 | 23 | 17 | 17 | 31 | 100 | 117 | 126 | 123 | 129 | 134 | 136 |
| | | Euro III - 2000 Standards | 7 | 5 | 4 | 4 | 7 | 21 | 25 | 27 | 26 | 27 | 29 | 29 |
| | Urban Buses | Conventional | 470 | 334 | 250 | 250 | 441 | 1437 | 1669 | 1803 | 1763 | 1851 | 1921 | 1949 |
| 8 | | Euro I - 91/542/EEC Stage I | 86 | 61 | 46 | 46 | 81 | 263 | 305 | 330 | 323 | 339 | 351 | 356 |
| ch | | Euro II - 91/542/EEC Stage II | 85 | 61 | 45 | 45 | 80 | 261 | 303 | 328 | 320 | 336 | 349 | 354 |
| ů | | Euro III - 2000 Standards | 17 | 12 | 9 | 9 | 16 | 51 | 59 | 64 | 62 | 66 | 68 | 69 |
| | Coaches | Conventional | 117 | 84 | 63 | 63 | 110 | 359 | 417 | 451 | 441 | 463 | 480 | 487 |
| ISC | | Euro I - 91/542/EEC Stage I | 21 | 15 | 11 | 11 | 20 | 66 | 76 | 82 | 81 | 85 | 88 | 89 |
| B | | Euro II - 91/542/EEC Stage II | 21 | 15 | 11 | 11 | 20 | 65 | 76 | 82 | 80 | 84 | 87 | 88 |
| | | Euro III - 2000 Standards | 4 | 3 | 2 | 2 | 4 | 13 | 15 | 16 | 16 | 16 | 17 | 17 |
| sb | <50 cm ³ | Conventional | 9082 | 6461 | 4841 | 4841 | 8537 | 27800 | 32280 | 34881 | 34104 | 35810 | 37154 | 37697 |
| ope | | 97/24/EC Stage I | 680 | 483 | 362 | 362 | 639 | 2080 | 2416 | 2610 | 2552 | 2680 | 2780 | 2821 |
| Ň | | 97/24/EC Stage II | 37 | 27 | 20 | 20 | 35 | 114 | 132 | 143 | 140 | 147 | 152 | 155 |
| | 2-stroke >50 cm ³ | Conventional | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | | 97/24/EC | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| cles | 4-stroke <250 cm ³ | Conventional | 4113 | 2926 | 2192 | 2192 | 3866 | 12589 | 14617 | 15795 | 15444 | 16216 | 16825 | 17070 |
| rcy | | 97/24/EC | 325 | 231 | 173 | 173 | 305 | 994 | 1154 | 1247 | 1219 | 1280 | 1328 | 1347 |
| oto | 4-stroke 250 - 750 cm ³ | Conventional | 4113 | 2926 | 2192 | 2192 | 3866 | 12589 | 14617 | 15795 | 15444 | 16216 | 16825 | 17070 |
| M | | 97/24/EC | 325 | 231 | 173 | 173 | 305 | 994 | 1154 | 1247 | 1219 | 1280 | 1328 | 1347 |
| | 4-stroke >750 cm ³ | Conventional | 4113 | 2926 | 2192 | 2192 | 3866 | 12589 | 14617 | 15795 | 15444 | 16216 | 16825 | 17070 |
| | 1 | 97/24/EC | 325 | 231 | 173 | 173 | 305 | 994 | 1154 | 1247 | 1219 | 1280 | 1328 | 1347 |

Table C.2. Hourly vehicle distribution in Frankfurter Allee, Berlin, 01:00 – 12:00.

Conventional

Conventional

Conventional

Conventional

97/24/EC

97/24/EC

97/24/EC

97/24/EC

Motorcycles

-stroke >50 cm³

-stroke <250 cm³

750 c 250 -

>750 cm

| Type | Class | Legislation | 13:00 | 14:00 | 15:00 | 16:00 | 17:00 | 18:00 | 19:00 | 20:00 | 21:00 | 22:00 | 23:00 | 0:00 |
|--|---------------------|--|--------|---------------|--------|--------|--------|----------|----------|--------|--------|-------|---------|---------|
| Type | Gasoline <1.41 | PREECE | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0.00 |
| | | ECE 15/00-01 | 1414 | 1449 | 1602 | 1658 | 1612 | 1510 | 1415 | 1138 | 939 | 725 | 639 | 467 |
| | | ECE 15/00 01 | 3489 | 3575 | 3953 | 4090 | 3977 | 3727 | 3491 | 2809 | 2316 | 1790 | 1576 | 1152 |
| | | ECE 15/02 | 12287 | 12502 | 13021 | 14405 | 14008 | 13126 | 12204 | 0803 | 2159 | 6303 | 5552 | 4057 |
| | | ECE 15/05 | 12267 | 12090 | 14220 | 14405 | 14008 | 12426 | 12294 | 10110 | 0150 | 6119 | 5670 | 4057 |
| | | Improved Conventional | 20152 | 20652 | 14239 | 14/33 | 22075 | 21528 | 20164 | 16226 | 12280 | 10220 | 0107 | 4150 |
| | | Open Loop | 20152 | 20032 | 22032 | 23027 | 22913 | 21326 | 20104 | 6252 | 5156 | 2084 | 2500 | 2564 |
| | | Euro L 01/441/EEC | 07175 | 00597 | 110008 | 112022 | 110797 | 102911 | 07222 | 78241 | 64521 | 10952 | 42014 | 22095 |
| | | Euro II 04/12/EC | 110420 | 112161 | 125105 | 120461 | 125000 | 117060 | 110495 | 2241 | 72215 | 56649 | 40200 | 26459 |
| | | Euro III - 94/12/EC | 110420 | 10646 | 51005 | 56708 | 55220 | 51752 | 110465 | 20005 | 22165 | 24952 | 21802 | 15005 |
| | Gasolina 1.4 2.01 | DRE ECE | 40444 | 49040 | 34880 | 30798 | 55250 | 51752 | 46472 | 39003 | 32103 | 24855 | 21092 | 13993 |
| | Gasonne 1,4 - 2,01 | FRE ECE ECE 15/00 01 | 1011 | 1059 | 2165 | 2240 | 2179 | 2041 | 1012 | 1529 | 1260 | 080 | 863 | 621 |
| | | ECE 15/00-01 | 4714 | 4921 | 5241 | 5527 | 5274 | 5026 | 1912 | 2705 | 21209 | 2419 | 2120 | 1556 |
| | | ECE 15/02 ECE 15/02 | 4/14 | 17014 | 19910 | 10465 | 19027 | 17725 | 4/1/ | 12267 | 11022 | 2410 | 2150 | 5491 |
| | | ECE 15/03 | 18064 | 10425 | 21496 | 22224 | 21/21 | 20250 | 10012 | 15307 | 12502 | 0720 | 9570 | (261 |
| | | Improved Conventional | 2254 | 19455 8450 | 21460 | 0679 | 0410 | 20239 | 8250 | 6646 | 5491 | 4025 | 2720 | 2725 |
| | | | 2101 | 2270 | 9552 | 2741 | 2629 | 2400 | 2102 | 25.00 | 2110 | 4233 | 1442 | 1054 |
| | | Error L 01/441/EEC | 155500 | 3270 | 17(201 | 3/41 | 177205 | 166224 | 3193 | 2509 | 102212 | 70826 | 70215 | 51275 |
| 2 | | Euro I - 91/441/EEC | 135598 | 159461 | 1/0291 | 182450 | 170100 | 150224 | 133090 | 125281 | 105512 | 79820 | 70315 | 31373 |
| ð | | Euro II - 94/12/EC | 149199 | 152904 | 74162 | 174929 | 74627 | 159589 | 149288 | 52702 | 42462 | 76545 | 0/424 | 49262 |
| d. | Coordina y 2.0.1 | Euro III - 98/69/EC Stage2000 | 65457 | 67083 | /4165 | /6/45 | /462/ | 69927 | 65496 | 52703 | 43462 | 33381 | 29580 | 21013 |
| <u>G</u> | Gasonne >2,01 | ECE 15/00-01 | 466 | 478 | 528 | 547 | 532 | 498 | 467 | 375 | 310 | 239 | 211 | 154 |
| an a | | ECE 15/02 | 1150 | 1179 | 1303 | 1349 | 1312 | 1229 | 1151 | 926 | 764 | 590 | 520 | 380 |
| - | | ECE 15/03 | 4052 | 4152 | 4590 | 4750 | 4619 | 4328 | 4054 | 3262 | 2690 | 2079 | 1831 | 1338 |
| | | ECE 15/04 | 4515 | 4627 | 5116 | 5294 | 5148 | 4824 | 4518 | 3635 | 2998 | 2316 | 2040 | 1491 |
| | | Euro I - 91/441/EEC | 40879 | 41894 | 46316 | 47929 | 46606 | 43671 | 40904 | 32914 | 27143 | 20972 | 18473 | 13497 |
| | | Euro II - 94/12/EC | 36412 | 37316 | 41254 | 42691 | 41513 | 38898 | 36433 | 29317 | 24176 | 18680 | 16455 | 12022 |
| | | Euro III - 98/69/EC Stage2000 | 15975 | 16371 | 18099 | 18729 | 18213 | 17066 | 15984 | 12862 | 10607 | 8195 | 7219 | 5274 |
| | Diesel <2,01 | Conventional | 25528 | 26162 | 28923 | 29930 | 29104 | 27271 | 25543 | 20554 | 16950 | 13097 | 11536 | 8429 |
| | | Euro I - 91/441/EEC | 15060 | 15434 | 17063 | 17658 | 17170 | 16089 | 15069 | 12126 | 10000 | 7726 | 6806 | 4973 |
| | | Euro II - 94/12/EC | 31987 | 32781 | 36241 | 37503 | 36468 | 34171 | 32006 | 25754 | 21238 | 16410 | 14455 | 10561 |
| | | Euro III - 98/69/EC Stage2000 | 14475 | 14834 | 16400 | 16971 | 16502 | 15463 | 14483 | 11654 | 9611 | 7426 | 6541 | 4779 |
| | Diesel >2,0 1 | Conventional | 17019 | 17441 | 19282 | 19953 | 19403 | 18181 | 17029 | 13703 | 11300 | 8731 | 7691 | 5619 |
| | | Euro I - 91/441/EEC | 10040 | 10290 | 11376 | 11772 | 11447 | 10726 | 10046 | 8084 | 6666 | 5151 | 4537 | 3315 |
| | | Euro II - 94/12/EC | 21324 | 21854 | 24161 | 25002 | 24312 | 22781 | 21337 | 17170 | 14159 | 10940 | 9637 | 7041 |
| | LDC | Euro III - 98/69/EC Stage2000 | 9650 | 9889 | 10933 | 11314 | 11001 | 10309 | 9655 | ///0 | 6407 | 4951 | 4361 | 3186 |
| | LPG | Euro I 91/441/EEC | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | | Euro II 94/12/EC | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | | Euro III - 98/69/EC Stage2000 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | 2-Stroke | Conventional | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | Gasoline <3,5t | Conventional | 4744 | 4862 | 5375 | 5562 | 5409 | 5068 | 4747 | 3820 | 3150 | 2434 | 2144 | 1566 |
| des | | Euro I - 93/59/EEC | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| iĝ. | | Euro II - 96/69/EC | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| ~ | | Euro III - 98/69/EC Stage2000 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 1 E | Diesel <3,5 t | Conventional | 17695 | 18134 | 20048 | 20746 | 20173 | 18903 | 17705 | 14247 | 11749 | 9078 | 7996 | 5842 |
| Ē | | Euro I - 93/59/EEC | 3915 | 4012 | 4436 | 4590 | 4464 | 4183 | 3918 | 3152 | 2600 | 2009 | 1769 | 1293 |
| [ji | | Euro II - 96/69/EC | 10997 | 11270 | 12460 | 12893 | 12538 | 11748 | 11004 | 8854 | 7302 | 5642 | 4970 | 3631 |
| _ | | Euro III - 98/69/EC Stage2000 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | Gasoline >3,5 t | Conventional | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | Diesel 3,5 - 7,5 t | Conventional | 15188 | 15565 | 17208 | 17807 | 17316 | 16225 | 15197 | 12229 | 10084 | 1025 | 6864 | 5015 |
| | | Euro I - 91/542/EEC Stage I | 3558 | 5822 | 4031 | 41/1 | 4056 | 3801 | 3560 | 2865 | 2362 | 1825 | 1608 | 11/5 |
| | | Euro II - 91/342/EEC Stage II Euro III - 2000 Standarda | 1207 | 1227 | 1268 | 1416 | 1276 | 1200 | 1208 | 4575 | 2//3 | 2915 | 2308 | 18/0 |
| 8 | Diesel 7.5 16 t | Conventional | 9010 | 0234 | 10208 | 10564 | 10272 | 9625 | 0015 | 7255 | 5082 | 4622 | 4072 | 2075 |
| icle | Diesei 7,5 - 10 t | Euro I 91/542/EEC Stage I | 2111 | 9254 | 2301 | 2475 | 2406 | 2255 | 2112 | 1600 | 1401 | 1083 | 4072 | 2973 |
| /ep | | Euro II 91/542/EEC Stage I | 3371 | 2105 | 2591 | 2473 | 2400 | 3601 | 2112 | 2714 | 2228 | 1720 | 1523 | 1113 |
| E. | | Euro III - 2000 Standards | 716 | 734 | 811 | 840 | 817 | 765 | 717 | 577 | 476 | 367 | 324 | 236 |
| ā | Diesel 16 - 32 t | Conventional | 6872 | 7043 | 7786 | 8057 | 7835 | 7342 | 6876 | 5533 | 4563 | 3526 | 3106 | 2269 |
| ŵ | | Euro I - 91/542/EEC Stage I | 1610 | 1650 | 1824 | 1887 | 1835 | 1720 | 1611 | 1296 | 1069 | 826 | 727 | 532 |
| He | | Euro II - 91/542/EEC Stage II | 2571 | 2635 | 2913 | 3015 | 2931 | 2747 | 2573 | 2070 | 1707 | 1319 | 1162 | 849 |
| _ | | Euro III - 2000 Standards | 546 | 560 | 619 | 640 | 623 | 584 | 547 | 440 | 363 | 280 | 247 | 180 |
| | Diesel >32t | Conventional | 376 | 385 | 426 | 441 | 429 | 402 | 376 | 303 | 250 | 193 | 170 | 124 |
| | | Euro I - 91/542/EEC Stage I | 88 | 90 | 100 | 103 | 100 | 94 | 88 | 71 | 58 | 45 | 40 | 29 |
| | | Euro II - 91/542/EEC Stage II | 141 | 144 | 159 | 165 | 160 | 150 | 141 | 113 | 93 | 72 | 64 | 46 |
| | | Euro III - 2000 Standards | 30 | 31 | 34 | 35 | 34 | 32 | 30 | 24 | 20 | 15 | 14 | 10 |
| | Urban Buses | Conventional | 2013 | 2063 | 2281 | 2360 | 2295 | 2151 | 2014 | 1621 | 1337 | 1033 | 910 | 665 |
| pes | | Euro I - 91/542/EEC Stage I | 368 | 377 | 417 | 432 | 420 | 393 | 368 | 297 | 245 | 189 | 166 | 122 |
| ad | | Euro II - 91/542/EEC Stage II | 366 | 375 | 414 | 429 | 417 | 391 | 366 | 294 | 243 | 188 | 165 | 121 |
| Ŭ | G 1 | Euro III - 2000 Standards | 7/1 | -73 | 81 | 84 | 81 | 76 | 71 | 57 | 47 | 37 | 32 | 24 |
| 8 | Coacnes | Conventional Euro L 91/542/EEC Store J | 503 | 516 | 570 | 590 | 574 | 538 | 504 | 405 | 334 | 258 | 227 | 166 |
| Bus | | Euro II - 91/542/EEC Stage I | 92 | 94 | 104 | 108 | 103 | 98 | 92 | 74 | 61 | 47 | 42 | 30 |
| | | Euro III - 2000 Standards | 191 | 94 19 | 20 | 21 | 20 | 98 10 | 91 19 | 14 | 12 | 4/ | 41 Q | 50 2 |
| ş | <50 cm ³ | Conventional | 38942 | 39909 | 44121 | 45657 | 44397 | 41601 | 38965 | 31355 | 25856 | 19978 | 17598 | 12858 |
| bec | | 97/24/EC Stage I | 2914 | 2986 | 3302 | 3417 | 3322 | 3113 | 2916 | 2346 | 1935 | 1495 | 1317 | 962 |
| M | | 97/24/EC Stage II | 160 | 164 | 181 | 187 | 182 | 171 | 160 | 129 | 106 | 82 | 72 | 53 |

1577

20675

20104

11709

18838

Table C.3. Hourly vehicle distribution in Frankfurter Allee, Berlin, 13:00 – 24:00.

714

7969

5822

ANNEX D

Hornsgatan case



Figure D.1. Model intercomparison results for NO_x average daily variation at street level in Hornsgatan in 2000 compared to hotspot measurements.



Figure D.2. Model intercomparison results for NO_2 average daily variation at street level in Hornsgatan in 2000 compared to hotspot measurements.



Figure D.3. Model intercomparison results for $PM_{2.5}$ average daily variation at street level in Hornsgatan in 2000 compared to hotspot measurements.



Figure D.4. OSPM model, user intercomparison results for NO_x average daily variation at street level in Hornsgatan in 2000 compared to measurements.



Figure D.5. OSPM model, user intercomparison results for NO_2 average daily variation at street level in Hornsgatan in 2000 compared to measurements.



Figure D.6. OSPM model, user intercomparison results for $PM_{2.5}$ average daily variation at street level in Hornsgatan in 2000 compared with measurements.

Frankfurter Allee case



Figure D.7. Model intercomparison results for CO average daily variation at street level in Frankfurter Allee in 2002 compared to hotspot measurements.



Figure D.8. Model intercomparison results for NO_x average daily variation at street level in Frankfurter Allee in 2002 compared to hotspot measurements.



Figure D.9. Model intercomparison results for NO_2 average daily variation at street level in Frankfurter Allee in 2002 compared to hotspot measurements.



Figure D.10. Model intercomparison results for PM_{10} average daily variation at street level in Frankfurter Allee in 2002 compared to hotspot measurements.



Figure D.11. OSPM model, user intercomparison results for CO average daily variation at street level in Frankfurter Allee in 2002 compared to measurements.



Figure D.12. OSPM model, user intercomparison results for NO_x average daily variation at street level in Frankfurter Allee in 2002 compared to measurements.



Figure D.13. OSPM model, user intercomparison results for NO_2 average daily variation at street level in Frankfurter Allee in 2002 compared to measurements



Figure D.14. OSPM model, user intercomparison results for PM_{10} average daily variation at street level in Frankfurter Allee in 2002 compared to measurements.

Marylebone Rd. case



Figure D.15. Model intercomparison results for CO average daily variation at street level in Marylebone Rd. in 2000 compared to hotspot measurements.



Figure D.16. Model intercomparison results for NO_x average daily variation at street level in Marylebone Rd. in 2000 compared with hotspot.



Figure D.17. Model intercomparison results for NO_2 average daily variation at street level in Marylebone Rd. in 2000 compared with hotspot measurements.



Figure D.18. Model intercomparison results for the $PM_{2.5}$ average daily variation at street level Marylebone Rd. in 2000 compared to hotspot measurements.



Figure D.19. SEP-SCAM model results, average daily variation for all four pollutants at street level in Marylebone Rd. in 2000 is compared to street measurement and indicative SEP-SCAM results using half the hourly wind speed intensity.

ANNEX E

| Tabl | e E.1. | DeltaCs | statistical | interco | mparison | for | NO_x | average | daily | variation | at |
|--------|---------|----------|-------------|---------|-----------|------|--------|---------|-------|-----------|----|
| street | level i | n Hornsg | atan in 200 | 0 comp | ared to D | elta | C obse | erved. | | | |

| | BOXSTREET | OSPM | SEP-SCAM | ADMS | LASAT | GRAL | MISKAM | MIMO |
|---------|-----------|--------|----------|--------|--------|--------|--------|--------|
| AVERAGE | 152.96 | 98.90 | 129.52 | 96.01 | 113.85 | 154.08 | 159.91 | 139.99 |
| BIAS | 4.67 | -49.38 | -18.77 | -52.28 | -34.43 | 5.80 | 11.62 | -8.29 |
| NMSE | 0.013 | 0.236 | 0.048 | 0.340 | 0.159 | 0.013 | 0.022 | 0.021 |
| CC | 0.970 | 0.989 | 0.983 | 0.844 | 0.890 | 0.980 | 0.980 | 0.983 |

Table E.2. DeltaCs statistical intercomparison for NO₂ average daily variation at street level in Hornsgatan in 2000 compared to DeltaC observed.

| | Č. | | | | |
|---------|-----------|-------|----------|-------|--------|
| | BOXSTREET | OSPM | SEP-SCAM | ADMS | LASAT |
| AVERAGE | 24.96 | 23.69 | 32.80 | 52.02 | 21.92 |
| BIAS | -6.87 | -8.13 | 0.98 | 20.20 | -9.90 |
| NMSE | 0.227 | 0.130 | 0.020 | 0.271 | 0.346 |
| CC | 0.360 | 0.941 | 0.966 | 0.759 | -0.235 |

Table E.3. DeltaCs statistical intercomparison for $PM_{2.5}$ average daily variation at street level in Hornsgatan in 2000 compared to DeltaC observed.

| | BOXSTREET | OSPM | SEP-SCAM | ADMS | LASAT | GRAL | MISKAM | МІМО |
|---------|-----------|-------|----------|-------|-------|-------|--------|-------|
| AVERAGE | 5.36 | 3.70 | 4.64 | 4.51 | 3.77 | 5.39 | 5.76 | 4.87 |
| BIAS | 0.24 | -1.43 | -0.49 | -0.61 | -1.36 | 0.27 | 0.64 | -0.25 |
| NMSE | 0.016 | 0.149 | 0.033 | 0.073 | 0.183 | 0.022 | 0.023 | 0.014 |
| СС | 0.979 | 0.967 | 0.940 | 0.901 | 0.939 | 0.950 | 0.976 | 0.979 |

Table E.4. OSPM user DeltaCs statistical intercomparison for NO_x average daily variation at street level in Hornsgatan in 2000 compared to DeltaC observed.

| | NERI | LHTEE | ESMG | NERI* |
|---------|--------|--------|--------|--------|
| AVERAGE | 98.90 | 96.97 | 100.50 | 174.82 |
| BIAS | -49.38 | -51.32 | -47.79 | 26.54 |
| NMSE | 0.236 | 0.250 | 0.244 | 0.050 |
| СС | 0.989 | 0.991 | 0.989 | 0.965 |

Table E.5. OSPM user DeltaCs statistical intercomparison for NO₂ average daily variation at street level in Hornsgatan in 2000 compared to DeltaC observed.

| | NERI | LHTEE | ESMG | NERI* |
|---------|-------|-------|-------|-------|
| AVERAGE | 23.69 | 29.25 | 29.33 | 34.81 |
| BIAS | -8.13 | -2.57 | -2.50 | 2.98 |
| NMSE | 0.130 | 0.029 | 0.042 | 0.020 |
| СС | 0.941 | 0.960 | 0.924 | 0.928 |

Table E.6. OSPM user DeltaCs statistical intercomparison for $PM_{2.5}$ average daily variation at street level in Hornsgatan in 2000 compared to DeltaC observed.

| | NERI | LHTEE | NERI* |
|---------|-------|-------|-------|
| AVERAGE | 3.70 | 3.69 | 6.34 |
| BIAS | -1.43 | -1.44 | 1.21 |
| NMSE | 0.149 | 0.154 | 0.072 |
| сс | 0.967 | 0.970 | 0.966 |
| | OSPM | SEP-SCAM | ADMS | LASAT | GRAL | CPB3 |
|---------|-------|----------|-------|-------|-------|-------|
| AVERAGE | 0.36 | 0.33 | 0.20 | 0.26 | 0.35 | 0.10 |
| BIAS | -0.04 | -0.07 | -0.20 | -0.14 | -0.05 | -0.30 |
| NMSE | 0.023 | 0.045 | 0.529 | 0.248 | 0.040 | 2.712 |
| СС | 0.956 | 0.966 | 0.965 | 0.910 | 0.944 | 0.810 |

Table E.7. DeltaCs statistical intercomparison for CO average daily variation at street level in Frankfurter Allee for 2002 compared to DeltaC observed.

Table E.8. DeltaCs statistical intercomparison for NO_x average daily variation at street level in Frankfurter Allee for 2002 compared to DeltaC observed.

| | BOXSTREET | OSPM | SEP-SCAM | ADMS | LASAT | GRAL | MIMO | CPB3 |
|---------|-----------|-------|----------|--------|--------|-------|-------|--------|
| AVERAGE | 71.42 | 66.54 | 60.59 | 35.25 | 44.66 | 63.47 | 81.44 | 15.10 |
| BIAS | 11.75 | 6.87 | 0.92 | -24.42 | -15.01 | 3.80 | 21.77 | -44.57 |
| NMSE | 0.079 | 0.043 | 0.047 | 0.424 | 0.184 | 0.070 | 0.156 | 2.860 |
| CC | 0.922 | 0.922 | 0.892 | 0.883 | 0.848 | 0.841 | 0.877 | 0.812 |

Table E.9. DeltaCs statistical intercomparison for NO_2 average daily variation at street level in Frankfurter Allee for 2002 compared to DeltaC observed.

| | BOXSTREET | OSPM | SEP-SCAM | ADMS | LASAT |
|---------|-----------|-------|----------|-------|-------|
| AVERAGE | 46.03 | 16.19 | 18.51 | 25.08 | 25.57 |
| BIAS | 29.56 | -0.28 | 2.03 | 8.60 | 9.10 |
| NMSE | 1.628 | 0.070 | 0.057 | 0.269 | 0.301 |
| CC | 0.543 | 0.848 | 0.886 | 0.785 | 0.711 |

Table E.10. DeltaCs statistical intercomparison for PM_{10} average daily variation at street level in Frankfurter Allee for 2002 compared to DeltaC observed.

| | BOXSTREET | OSPM | SEP-SCAM | ADMS | LASAT | GRAL | МІМО |
|---------|-----------|-------|----------|-------|-------|-------|-------|
| AVERAGE | 2.46 | 3.38 | 3.43 | 2.09 | 2.17 | 3.27 | 14.87 |
| BIAS | -7.53 | -6.60 | -6.56 | -7.90 | -7.81 | -6.72 | 4.89 |
| NMSE | 2.646 | 1.615 | 1.571 | 3.580 | 3.397 | 1.713 | 0.261 |
| СС | 0.843 | 0.681 | 0.798 | 0.774 | 0.747 | 0.744 | 0.811 |

Table E.11. OSPM user DeltaCs statistical intercomparison for CO average daily variation at street level in Frankfurter Allee for 2002 compared to DeltaC observed.

| | NERI | LHTEE | ESMG | NERI* |
|---------|-------|-------|-------|-------|
| AVERAGE | 0.36 | 0.28 | 0.18 | 0.34 |
| BIAS | -0.04 | -0.12 | -0.22 | -0.06 |
| NMSE | 0.023 | 0.154 | 0.820 | 0.042 |
| СС | 0.956 | 0.961 | 0.952 | 0.967 |

| Table E.12.OSPM user | DeltaCs statistical | intercomparison | for NO _x | average | daily |
|--------------------------------|-----------------------|------------------|---------------------|-----------|-------|
| variation at street level in 1 | Frankfurter Allee for | or 2002 compared | l to Delta | C observe | ed. |

| | NERI | LHTEE | ESMG | NERI* |
|---------|-------|-------|--------|-------|
| AVERAGE | 66.54 | 50.99 | 32.88 | 61.37 |
| BIAS | 6.87 | -8.69 | -26.79 | 1.70 |
| NMSE | 0.043 | 0.093 | 0.586 | 0.046 |
| CC | 0.922 | 0.885 | 0.872 | 0.897 |

| Tunktutter Thee for 2002 compared to Denue observed | | | | |
|---|-------|-------|-------|-------|
| | NERI | LHTEE | ESMG | NERI* |
| AVERAGE | 16.19 | 17.26 | 11.30 | 15.26 |
| BIAS | -0.28 | 0.79 | -5.17 | -1.22 |
| NMSE | 0.070 | 0.050 | 0.322 | 0.077 |
| cc | 0.848 | 0.885 | 0.850 | 0.853 |

Table E.13. OSPM user DeltaCs intercomparison for NO₂ average daily variation at street level in Frankfurter Allee for 2002 compared to DeltaC observed.

| Table E.14. | OSPM user | DeltaCs s | statistical | intercomparis | on for | $PM_{10} \\$ | average | daily |
|-----------------|----------------|-----------|-------------|---------------|---------|--------------|----------|-------|
| variation at st | treet level in | Frankfurt | er Allee fe | or 2002 compa | ared to | measu | rements. | |

| | NERI | LHTEE | ESMG | NERI* |
|---------|-------|-------|-------|-------|
| AVERAGE | 3.38 | 2.71 | 1.63 | 8.08 |
| BIAS | -6.60 | -7.28 | -8.36 | -1.90 |
| NMSE | 1.615 | 2.397 | 5.240 | 0.114 |
| cc | 0.681 | 0.788 | 0.539 | 0.831 |

Table E.15. DeltaCs statistical intercomparison for CO average daily variation at street level in Marylebone Rd. for 2000 compared to DeltaC observed.

| | SEP-SCAM | GRAL | ADMS | LASAT | CPB3 |
|---------|----------|-------|-------|-------|-------|
| AVERAGE | 0.60 | 0.69 | 0.34 | 0.43 | 0.18 |
| BIAS | -1.05 | -0.96 | -1.31 | -1.22 | -1.47 |
| NMSE | 1.334 | 0.992 | 3.573 | 2.511 | 8.384 |
| cc | 0.862 | 0.813 | 0.826 | 0.793 | 0.886 |

Table E.16. DeltaCs statistical intercomparison for NO_x average daily variation at street level in Marylebone Rd. for 2000 compared to DeltaC observed.

| | BOXSTREET | SEP-SCAM | GRAL | ADMS | LASAT | ΜΙΜΟ | CPB3 |
|---------|-----------|----------|---------|---------|---------|--------|---------|
| AVERAGE | 135.11 | 166.98 | 195.29 | 90.52 | 117.20 | 230.07 | 47.18 |
| BIAS | -167.67 | -135.79 | -107.48 | -212.25 | -185.58 | -72.70 | -255.59 |
| NMSE | 0.743 | 0.390 | 0.225 | 1.762 | 1.041 | 0.102 | 4.864 |
| cc | 0.807 | 0.928 | 0.852 | 0.900 | 0.855 | 0.864 | 0.945 |

Table E.17. DeltaCs statistical intercomparison results for NO₂ average daily variation at street level in <u>Marylebone Rd. for 2000 compared to DeltaC</u> observed.

| | BOXSTREET | SEP-SCAM | ADMS | LASAT |
|---------|-----------|----------|-------|-------|
| AVERAGE | 8.63 | 23.07 | 49.66 | 47.82 |
| BIAS | -24.96 | -10.52 | 16.07 | 14.23 |
| NMSE | 4.681 | 0.199 | 0.183 | 0.158 |
| cc | -0.442 | 0.971 | 0.831 | 0.813 |

Table E.18. DeltaCs statistical intercomparison results for $PM_{2.5}$ average daily variation at street level in Marylebone Rd. for 2000 compared to DeltaC observed.

| | BOXSTREET | SEP-SCAM | ADMS | LASAT | МІМО | GRAL |
|---------|-----------|----------|-------|-------|-------|-------|
| AVERAGE | 3.94 | 7.49 | 5.32 | 5.34 | 10.58 | 8.65 |
| BIAS | -7.57 | -4.03 | -6.19 | -6.17 | -0.93 | -2.86 |
| NMSE | 1.334 | 0.202 | 0.671 | 0.669 | 0.034 | 0.098 |
| CC | 0.905 | 0.967 | 0.957 | 0.952 | 0.951 | 0.950 |